# ELEGTRONG D.A.ABOOK 

Packed with vital, up-to-date facts on every aspect of electronics practice . . . for hobbyists and professionals!


BY RUDOLF F. GRAF

## To My Mother and Father

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## THIRD EDITION

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The entire electromagnetic spectrum is presented. Then portions of this spectrum that are of particular interest to the electrical and electronic engineer are described in greater detail.

## 2. COMMUNICATION <br> 18

Information useful in all segments of communication, starting with propagation characteristics, modes, standards, and transmission data is given. Antenna, transmission line, and waveguide characteristics and performance data are presented. Modulation and intemational telecommunications standards, signals, signal reporting codes, radio amateur data, and emission information are also given, as is information on microphones.
3. PASSIVE COMPONENTS ANO CIRCUITS 70
Resistors, amplifiers, attenualors, filters, inductors, transformers, and capacitors are covered and their characteristics and applications are treated in depth. Computer-calculated tabulations of modern filter designs based on network synthesis are given.

Vacuum tubes, semiconductors, and integrated circuits are covered. Circuit configurations are given in which these components are employed together with definitions of integrated circuit, logic, and microelectronic terms. A tabulation that shows the characteristics of integrated circuit logic families currentiy in use is given. Solid-state sensor characleristics and semiconductor memories are covered.
5. MATHEMATICAL DATA, FORMULAS, SYMBOLS 220

This section covers reliability; mathematical signs. symbols, operations, and tables; charts and formulas; prefixes; geometric curves; solids; spherical as well as plane geometry; and trigonometry. Frequency, phase angle, and time relationships for recurrent wave forms are given. Power and voltage level determinations in signals circuits are explained. Letter symbols for all quantities encountered in the electronics, electrical field are defined. This section concludes with a comprehensive selection of conversion factors.
6. PHYSICAL DATA 300

This section covers the most often needed physical data and includes, among other items, laser radiation, motors, radioactivity, optical data, sound, incandescent lamps, cathode ray tubes, crystals, color codes, relay contacl code, military nomenclature, atmospheric and space data, chemical data, plastics, temperature and humidity tables, energy conversion factors and equivalents, wire data, hardware, shock and vibration, cooling data, and characteristics of materials.

INOEX 400

## Preface

This revised and expanded edition includes a great deal of new material that has come to light since the second edition was published.

The filter section has been thoroughly updated and now includes computer-generated tabulations of modern filter design based on network synthesis. This major entry was especially prepared for this book by Mr. Ed Wetherhold, whose contribution I most gratefully acknowledge.

I also wish to thank my friends and colleagues Rich Myers and F. Raymond Dewey for giving so unselfishly of their time to review and comment on the previous edition of this work and for generously sharing with me much of their private source material.

The word knowledge brings to mind the staggering body of facts and data accumulated by mankind since his descent from the trees. Once, thousands of years ago, it was possible for a man to know all that his kind had discovered. But, lime has added so greatly to our reservoir of wisdom, that knowledge, today, has assumed another meaning: knowing where to find the information needed.

This book humbly admits to being my attempt at simplifying the task of the busy engineer, technician, amateur, and sludent in locating the data he needs in the shortest possible time.

Gathered here, in one single volume, is a wealth of information in the form of timely and practical nomograms, tables, charts, and formulas.

Some of the material was available elsewhere, at some time or other, but never has all of it been gathered together under one cover. New and heretofore unpublished charts and nomograms are added because of what seemed to me an obvious need for such material.

The book is arranged in a most readily usable format. It contains only clear-cut, theory-free data and examples that are concise, accurate, and to the point. The user of this book will be looking for answers and he will find them, without having to fight his way through lengthy derivations and proofs.

In order to assist you in tinding the data you seek, the book has been divided into six functional sections. That organization, together with a comprehensive index, quickly leads to the specific information needed. The
book maintains uniform terminology and format which assures that data found in one section can be easily and accurately related to those in the rest of the book.

Much new and up-dated material has been added to this current edition of the book. It has been my intention (and centainly my hope) that this new material makes the book still more useful and comprehensive.

The preparation of a reference book such as this is not possible without the cooperation and assistance of numerous industry sources who have so generously made their material available. I gratefully acknowledge, with special thanks, the conlributions and critical efforts of Messrs. George J. Whalen, Arthur E. Fury, Rene Colen, and B. William Dudley, Jr.

If this book saves you many hours of tedious computations and search for information, it will indeed have served its intended purpose.

The author and publisher invite your comments and suggestions regarding any such other material as might have been included here, so that it may be considered for any subsequent edition or revision.

## Acknowledgments

Acknowledgment is made to the following organizations and publications who have permitted use of material originally published by them. I appreciate their cooperation during the preparation of this book.

Alpha Metals, Inc.: page 390.
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Automatic Electric Company: pages 236-237, 238, 267 (all from Tables and Formsiae).
Centralab Division of Globe-Union, Inc.: page 99.
Clairex Electronics, Inc. (and J. R. Rabinowilz): page 307.
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Conrad, Inc.: page 358.
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Clifford, (% 1980 BY TAB BOOKS Inc.).
Testing Machines Inc,: pages 287-299.
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TRW, Capacitor Division, page 242.
Vibrac Corporation: page 379.
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# ELECTRONIC DATABOOK 3RD EDITION 

## Section 1

## Frequency Data

The Electromagnelic Spectrum ..... 14
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This chart presents an overview of the complete electromagnetic radiation spectrum, extending from infrasonics to cosmic rays. The wavelength, the amount of energy required to radiale one photon, a general description, the band designation, and the normal occurrence or use are given. Some specific bands are described in more detall on the following pages.

$$
\begin{aligned}
& \lambda_{\mathrm{m}}=\frac{300,000}{f_{\mathrm{kHz}}}=\frac{300}{f_{\mathrm{MHz}}} \quad \lambda_{\mathrm{cm}}=\frac{30}{f_{G H Z}} \\
& \lambda_{\mathrm{ft}}=\frac{984,000}{f_{\mathrm{kHz}}}=\frac{984}{f_{\mathrm{MHz}}} \quad \lambda_{\mathrm{lm}}=\frac{11.8}{f_{G H z}}
\end{aligned}
$$



WAVELENGTH BANDS AND FREQUENCY USED IN RADIOCOMMUNICATION
Nomenclature of the frequency and wavelength bands used in radiocommunication in accordance with Article 2 , No. 12 of the "Radio Regulations," Geneva, 1959.

| Band Number | Frequency Range (lower fimit exclusive, upper limit inclusive) |  |  | Corresponding Metric Subdivision | Adjectival Band Designation |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\dagger$ |  | $30 \mathrm{c} / \mathrm{s}$ | ( Hz ) | Petametric waves | ELF Extremely-Low Frequency |
| 2 | $30-$ | $300 \mathrm{c} / \mathrm{s}$ | $(\mathrm{Hz})$ | Terametric waves | SLF Super-LOW Frequency |
| 3 | 300- | $3000 \mathrm{c} / \mathrm{s}$ | ( Hz ) | Gigametric waves | ULF Ultra-Low Frequency |
| 4 |  | $30 \mathrm{kc} / \mathrm{s}$ | (kHz) | Myriamelric waves | VLF Very-Low Frequency |
| 5 | $30-$ | $300 \mathrm{ke} / \mathrm{s}$ | (kHz) | Kilometric Waves | LF Low Frequency |
| 6 | $300-$ | $3000 \mathrm{kc} / \mathrm{s}$ | ( kHz ) | Hectometric waves | MF Medium Frequency |
|  |  | $30 \mathrm{Mc} / \mathrm{s}$ | (MHz) | Decametric waves | HF High Frequency |
| 8 | $30-$ | $300 \mathrm{Mc} / \mathrm{s}$ | (MHz) | Matric waves | VHF Very High Frequency |
| 9 | 300- | $3000 \mathrm{Mc} / \mathrm{s}$ | ( MHz ) | Decimetric waves | UHF Ultra-High Frequency |
| 10 |  | $30 \mathrm{Gc} / \mathrm{s}$ | (GHz) | Centimetric waves | SHF Super-High Frequency |
| 11 |  | $300 \mathrm{Ge} / \mathrm{s}$ | (GHz) | Millimetric waves | EHF Extremely-High Frequency |
| 12 | $300-$ | $\begin{aligned} & 3000 \mathrm{Gc} / \mathrm{s} \\ & \text { or } 3 \mathrm{Te} / \mathrm{s} \end{aligned}$ | $\begin{aligned} & (\mathrm{GHz}) \\ & (\mathrm{THz}) \end{aligned}$ | Decimilimetric waves | --- -- |

## BROADCASTING FREQUENCY ASSIGNMENTS

This table shows the frequency range, number of available channels, and channel width for AM, FM, and TV service in the United States.

| Type of Service | Frequency Range | Number of Available Channels | Width of Each Channel |
| :---: | :---: | :---: | :---: |
| AM radio FM radio | $\begin{gathered} 535-1605 \mathrm{kHz} \\ 88-108 \mathrm{MHz} \\ 54-72 \mathrm{MHz} \end{gathered}$ | $\begin{aligned} & 107 \\ & 100 \end{aligned}$ | $\begin{array}{r} 10 \mathrm{kHz} \\ 200 \mathrm{kHz} \end{array}$ |
| VHF television | $\left\{\begin{array}{r}\text { 76- } 88 \mathrm{MHz} \\ 174-216 \mathrm{MHz}\end{array}\right.$ | 12 | 6 MHz |
| UHF television | 470-890 M Hz | 70 | 6 MHz |




| Channel Number | Frequency Limits ( MHz ) | Video Carrier ( MHz ) Sound Carrier (MHz) |
| :---: | :---: | :---: |
| 69 |  | 801.25 |
|  |  | 805.75 |
| 70 (*) |  | 807.25 |
|  |  | 811.75 |
| 71 |  | 813.25 |
|  |  | 817.75 |
| 72 |  | 819.25 |
|  |  | 823.75 |
| 73 |  | 825.25 |
|  |  | 829.75 |
| 74 |  | 831.25 |
|  |  | 835.75 |
| 75 |  | 837.25 |
|  |  | 841.75 |
| 76 |  | 843.25 |
|  |  | 847.75 |
| 77 |  |  |
|  |  | $849.25$ |
|  | 854 | 853.75 |
| 78 |  | 855.25 |
|  |  | 859.75 |
| 79 |  |  |
|  |  | $\begin{aligned} & 861.25 \\ & 865.75 \end{aligned}$ |
| ...... | .-..-866 | ......- |
| 80 |  | 867.25 |
|  |  | 871.75 |
| 81 | -.872 |  |
|  |  | $\begin{aligned} & 873.25 \\ & 87775 \end{aligned}$ |
|  | ...-..-878. | 87.75 |
| 82 |  | 979.25 |
|  |  | 883.75 |
| 83 |  | 885.25 |
|  |  | 889.75 |

(*) Channels 70 to 83 were withdrawn and reassigned to TV translator station until licenses expire. License renewals will be granted only a secondary basis for land mobile radio operation.

FREQUENCIES IN USE AROUND THE WORLD IN THE AERONAUTICAL MOBILE BANDS

| WORLD AIR ROUTE AREA | FREQUENCY ALLOCATION (kHz) |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Alakk | 2945 | 3411.5 | 4668.5 | 5611.5 | 6567 |  | 11,328 |  |
| Hawall |  | 3453.5 |  | 5559 | 6649.5 |  |  |  |
| West Indies | 2861 |  | 4689.5 |  |  |  |  |  |
| Central East Pacific |  | $\begin{aligned} & 3432.5 \\ & 3446.5 \\ & 3467.5 \\ & 3481.5 \end{aligned}$ |  | $\begin{aligned} & 5551.5 \\ & 5604 \end{aligned}$ | $\begin{aligned} & 6612 \\ & 6679.5 \end{aligned}$ | $\begin{aligned} & 8879.5 \\ & 8930.5 \end{aligned}$ | $\begin{aligned} & 10,048 \\ & 10,084 \\ & 11,299.5 \\ & 11,318.5 \end{aligned}$ | $\begin{aligned} & 13,304.5 \\ & 13,334.5 \\ & 17,526.5 \end{aligned}$ |
| Central West Pacific | 2966 |  |  | $\begin{aligned} & 5506.5 \\ & 5536.5 \end{aligned}$ |  | 8862.5 |  | $\begin{aligned} & 13,354.5 \\ & 17,906.5 \end{aligned}$ |
| North Pecific | 2987 |  |  | 5521.5 |  | 8939 |  | $\begin{aligned} & 13,274.5 \\ & 17,906.5 \end{aligned}$ |
| South Pacific | 2945 |  |  | 5641.5 |  | 8845.5 |  | $\begin{aligned} & 13,344.5 \\ & 17,946.5 \end{aligned}$ |
| North Atlantic | $\begin{aligned} & 2868 \\ & 2931 \\ & 2945 \\ & 2987 \end{aligned}$ |  |  | $\begin{aligned} & 5611.5 \\ & 5626.5 \\ & 5641.5 \\ & 5671.5 \end{aligned}$ |  | $\begin{aligned} & 8862.5 \\ & 8888 \\ & 8913.5 \\ & 8947.5 \end{aligned}$ |  | $\begin{aligned} & 13,264.5 \\ & 13,284.5 \\ & 13,324.5 \\ & 13,354.5 \\ & 17,966.5 \end{aligned}$ |
| Eutope | $\begin{aligned} & 2889 \\ & 2910 \end{aligned}$ | $\begin{aligned} & 3467.5 \\ & 3481.5 \end{aligned}$ | $\begin{aligned} & 4654.5 \\ & 4689.5 \end{aligned}$ | 5551.5 | $\begin{aligned} & 6552 \\ & 6582 \end{aligned}$ | $\begin{aligned} & 8871 \\ & 8930.5 \end{aligned}$ | 11,299.5 | 17,906.5 |
| North-South America | $\begin{aligned} & 2889 \\ & 2910 \\ & 2966 \end{aligned}$ | 3404,5 | 4696.5 | $\begin{aligned} & 5566.5 \\ & 5581.5 \end{aligned}$ | 6567 <br> 6664.5 | $\begin{aligned} & 8820 \\ & 8845.5 \end{aligned}$ $8871$ | $\begin{aligned} & 11,290 \\ & 11,337.5 \end{aligned}$ | $\begin{aligned} & 13,314.5 \\ & 13,344.5 \\ & 17,916.5 \end{aligned}$ |
| Far East | $\begin{aligned} & 2868 \\ & 2987 \end{aligned}$ |  |  | $\begin{aligned} & 5611.5 \\ & 5671.5 \end{aligned}$ |  | 8871 <br> 8879.5 <br> 8930.5 |  | $\begin{aligned} & 13,284.5 \\ & 13,324.5 \\ & 17.966 .5 \end{aligned}$ |
| South Atlantic | 2875 | 3432.5 |  |  | 6597 <br> 6612 <br> 5679.5 | $\begin{aligned} & 8879.5 \\ & 8939 \end{aligned}$ | 10,048 | $\begin{aligned} & 13.274 .5 \\ & 17.946 .5 \end{aligned}$ |
| Middle East |  | $\begin{aligned} & 3404.5 \\ & 3446.5 \end{aligned}$ |  | 5604 | 6627 | 8845.5 | 10.021 | $\begin{aligned} & 13,334.5 \\ & 17,926.5 \end{aligned}$ |
| North-South Africa | 2966 | 3411.5 |  | $\begin{aligned} & 5506.5 \\ & 5521.5 \end{aligned}$ |  | $\begin{aligned} & 8820 \\ & 8956 \end{aligned}$ |  | $\begin{aligned} & 13,304.5 \\ & 13,334.5 \\ & 17,926.5 \\ & 17,946.5 \end{aligned}$ |
| Carlbbean | $\begin{aligned} & 2875 \\ & 2952 \\ & 2966 \end{aligned}$ |  |  | 5499 <br> 5566.5 <br> 5619 | 6537 | $\begin{aligned} & 8837 \\ & 8877 \end{aligned}$ | 10.021 | $\begin{aligned} & 13,294.5 \\ & 13,344.5 \\ & 17,936.5 \end{aligned}$ |
| Canada | 2973 |  |  | 5499 |  | 8871 | 11,356.5 |  |

FREQUENCIES USED BY SHIP AND SHORE STATIONS

| $\begin{aligned} & \text { Band } \\ & (\mathrm{MHz}) \end{aligned}$ | SHIP STATIONS |  | SHORE STATIONS |
| :---: | :---: | :---: | :---: |
|  | Calling Frequencies (kHz) | Working Frequencies (kHz) | (Approximate Limits) |
| 2 | 2065-2107 | Same as calling | 2000-2065 |
| 4 | 4178-4186 | $\begin{aligned} & 4161-4176 \\ & 4188-4236 \end{aligned}$ | 4240-4400 |
| 6 | 6267-6279 | $\begin{aligned} & 6241-6264 \\ & 5282-6355 \end{aligned}$ | 6352-6523 |
| 8 | 8356-8372 | $\begin{aligned} & 8322=8352 \\ & 8376-8473 \end{aligned}$ | 8478-8742 |
| 12 | 12,534-12,558 | $\begin{aligned} & 12,474-12,528 \\ & 12,564-12,709 \end{aligned}$ | 12,714-13,128 |
| 16 | 16,712-16,744 | $\begin{aligned} & 16,626=16,704 \\ & 16,752=16,946 \end{aligned}$ | 16,950-17,285 |
| 22 | 22,225-22,265 | $\begin{aligned} & 22,151-22,217 \\ & 22,272-22,395 \end{aligned}$ | 22,400-22,670 |

INTERNATIONAL AMPLITUDE-MODULATION BROADCASTING FREQUENCIES

| AMATEUR RADIO FREQUENCIES |  |  | $\begin{aligned} & 6.200 \mathrm{MHz} \\ & 9.775 \\ & 11.975 \\ & 15.45 \\ & 17.90 \\ & 21.75 \\ & 26.10 \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: |
| 1800 |  | $-2000 \mathrm{kHz}$ | $\begin{array}{ll} 3.300- & 3.500 \mathrm{GHz} \\ 5.650- & 5.925 \end{array}$ |  |
| $\begin{aligned} & 3.500 \\ & 7.000 \end{aligned}$ |  | - $\quad 4.000 \mathrm{MHz}$ |  |  |
|  |  | - 7.300 | $10.00-$ | 10.50 |
| 14.00 |  | - 14.35 | 24.00 - | 24.25 |
| 21.00 |  | - 21.45 | $48.00-$ | 50.00 |
| 28.00 |  | - 29.70 | $71.00-$ | 84.00 |
| 50.00 |  | - 54.00 | 152.0 - | 170.0 |
| 144.0 |  | - 148.0 | 200.0 - | 220.0 |
| 220.0 |  | - 225.0 | 240.0 - | 250.0 |
| 420.0 |  | - 450.0 | Above 275.0 |  |
| $1215$ |  | -1300 |  |  |
| 2300 |  | -2450 |  |  |

## CITIIINS RAOIO (PERSONAL RADIO) FREQUENCIES

$$
\begin{gathered}
26.96 \quad 27.23 \mathrm{MHz} \\
462.5375-462.7375 \\
467.5375-467.7375
\end{gathered}
$$

| Band | Frequency | Wavelength | Typical Use |
| :---: | :---: | :---: | :---: |
| P | $225-390 \mathrm{MHz}$ | $133.3-76.9 \mathrm{~cm}$ | Long range (over 200 miles) to very long range (beyond 1,000 miles) surface-10-air search. |
| L | $390-1550 \mathrm{MHz}$ | $76.9-19.3 \mathrm{~cm}$ | Very long through medium range surface-to-air missile and aircratt detection, tracking and air tratfic control, IFF transponders, beacon systems. |
| S | $1.55-5.2 \mathrm{GHz}$ | $19.3-5.77 \mathrm{~cm}$ | Medium and long range surface-to-air surveiliance, surfacebased weather radar, altimetry, missile-borne guidance, airborne bomb-navigation systems. |
| C | $3.9-6.2 \mathrm{MHz}$ | 7.69-4.84 cm | Airborne fire control, missile-borne beacons, recon, airborne weather avoidance, aircraft and missile target tracking. |
| $x$ | $5.2-10.9 \mathrm{MHz}$ | $5.77-2.75 \mathrm{~cm}$ | Doppler navigation, airborne fire control, airborne and sur-lace-based weather delection, bomb-navigation systems, missile-borne guidance, precision landing approach. |
| $K$ | 10.9- 36 GHz | $2.75-0.834 \mathrm{~cm}$ | Doppler navigation, automatic landing systems, airborne fire control, radar fuzing, recon, missile-borne guidance. |
| $Q$ | 36- 46 GHz | $0.834-0.652 \mathrm{~cm}$ | Recon, airport surlace detection. |
| V | $46-56 \mathrm{GHz}$ | $0.652-0.536 \mathrm{~cm}$ | High-resolution experimental shortrange systems. |

## CTCS (CONTINUOUS TONE CODED SQUELCH) ANO REMDTE CONTROL STANDARD FREQUENCY TABLE

The EIA Standard Tone Frequencies for remote (i.e., radio paging) and control applications have been established to allow adequate separation and minimum harmonic relationship for use in multiple frequency systems.

For optimum system performance it is best to choose the widest frequency spacing possible within the recommended range.

| Frequency | EIA | Frequency | EIA | Frequency | EIA |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Hz | Code | Hz | Code | Hz | Code |
| 67.0 | L. 1 | 258.8 | 136 | 651.9 | 153 |
| 71.9 | L 2 | 266.0 | 106 | 669.9 | 123 |
| 77.0 | L 3 | 273.3 | 137 | 688.3 | 154 |
| 82.5 | $\llcorner 4$ | 280.8 | 107 | 707.3 | 124 |
| 88.5 | L 4A | 288.5 | 138 | 726.8 | 155 |
| 94.8 | L 5 | 296.5 | 108 | 746.8 | 125 |
| 100.0 | 1 | 304.7 | 139 | 767.4 | 156 |
| 103.5 | 1 A | 313.0 | 109 | 788.5 | 126 |
| 107.2 | 18 | 321.7 | 140 | 810.2 | 157 |
| 110.9 | 2 | 330.5 | 110 | 832.5 | 127 |
| 114.8 | 2 A | 339.6 | 141 | 655.2 | 158 |
| 118.8 | 2 B | 349.0 | 111 | 879.0 | 128 |
| 123.0 | 3 | 358.6 | 142 | 903.0 | 159 |
| 127.3 | 3A | 368.5 | 112 | 926.1 | 129 |
| 131.8 | 3B | 378.6 | 143 | 953.7 | 160 |
| 136.5 | 4 | 389.0 | 113 | 979.9 | 130 |
| 141.3 | 4A | 399.8 | 144 | 1006.9 | 161 |
| 146.2 | 4B | 410.8 | 114 | 1049.6 | 131 |
| 151.4 | 5 | 422.1 | 145 | 1084.0 | P |
| 156.7 | 5A | 433.7 | 115 | 1120.0 | S11 |
| 162.2 | 5 B | 445.7 | 146 | 1190.0 | S12 |
| 167.9 | 6 | 457.9 | 116 | 1220.0 | S2 |
| 173.8 | 6A | 470.5 | 147 | 1265.0 | S14 |
| 179.9 | 6 B | 483.5 | 117 | 1291.4 | S3 |
| 186.2 | 7 | 496.8 | 148 | 1320.0 | S15 |
| 192.8 | 7A | 510.5 | 118 | 1355.0 | S16 |
| 203.5 | M1 | 524.6 | 149 | 1400.0 | S17 |
| 210.7 | M2 | 539.0 | 119 | 1430.5 | S7 |
| 218.1 | M3 | 553.9 | 150 | 1450.0 | S18 |
| 225.7 | M4 | 569.1 | 120 | 1500.0 | S20 |
| 233.6 | M5 | 582.1 | H | 1520.0 | S9 |
| 241.8 | M6 | 600.9 | 121 | 1550.0 | S21 |
| 250.3 | M7 | 617.4 | 152 | 1600.0 | S22 |
|  |  | 634.5 | 122 |  |  |

## ULTRASONIC TRANSDUCER MATERIALS

The table lists the ultrasonic transducer materials used in instrumentation, sensing and power applications.

| Piezoelectric Transducers |  |  |  |
| :---: | :---: | :---: | :---: |
| Material | Frequency Aange | Maximum Sare Operating Temperature | Typical Applications |
| Quartz | $100 \mathrm{kHz}-35+\mathrm{MHz}$ | $550^{\circ} \mathrm{C}$ | Medical and non-destructive testing |
| Barium Titanate | $100 \mathrm{kHz}-10 \mathrm{MHz}$ | $100^{\circ} \mathrm{C}$ | Most cleaning and processing applications |
| Lead Zirconale Lead Titanate | $5 \mathrm{kHz}-10 \mathrm{MHz}$ | $320^{\circ} \mathrm{C}$ | Mosl cleaning and processing applications, (high temperature uses) |
| Rochelle Salt | $20 \mathrm{~Hz}-1 \mathrm{MHz}$ | $45^{\circ} \mathrm{C}$ | Sonar and depth linding |
| Magnetostrictive Transducers |  |  |  |
| Nickel | $10 \mathrm{kHz}-100 \mathrm{kHz}$ | - | Cleaning, drilling, machining, soldering, melt treatment, and applications where transducer has pressure applied |
| Venadium Permendur | $10 \mathrm{kHz}-100 \mathrm{kHz}$ | - | Same as nickel |

## ULTRASONIC FREQUENCY SPECTRUM

Ultrasonic Frequency Spectrum


## NBS STANDARD FREQUENCY AND TIME bROADCAST SCHEDULES

The diagrams presented here, with explanalory notes, summarize the technical services provided by the National Bureau of Standards (NBS) radio stations WWV, WWVH, WWVB, and WWVL.

## WWV and WWVH Broadcast Services

Standard Radio Frequencies. WWV and WWVH transmit frequencies and time coordinated through the Bureau International de l'Heure (BIH), Paris, France. Transmissions are based upon the International time scale, Universal Coordinated Time (UTC).

WWV broadcasts continuously on radio carrier frequencies of $\mathbf{2 . 5}, 5,10,15,20$, and 25 MHz . WWVH broadcasts continuously on radio carrier frequencies of $2.5,5,10$, 15 and 20 MHz .

The broadcasts of WWV may also be heard via telephone by dialing (303) 499-7111, Boulder, Colorado.
Standard Audio Frequencies. Standard audio frequencies of $440 \mathrm{~Hz}, 500 \mathrm{~Hz}$, and 600 Hz are broadcast on each radio carrier frequency by the two stations. Duration of each Iransmitted standard tone is approximately 45 seconds. A $600 \cdot \mathrm{~Hz}$ tone is broadcast during odd minutes by WWW and during even minutes by WWVH. A $500 \cdot \mathrm{~Hz}$ tone is broadcast during alternate minutes unless voice announcements or silent periods are scheduled. The $440-\mathrm{Hz}$ tone is broadcast beginning one minute after the hour at WWVH and two minutes after the hour at WW. The $440-\mathrm{Hz}$ tone period is omitted during the first hour of the UTC day.

Standard Musical Pitch. The $440-\mathrm{Hz}$ tone is broadcast for approximately 45 seconds beginning 1 minute after the hour at WWVH and 2 minutes atter the hour at WWV. The tone is omitted during the zero hour of each UTC day.

Standard Time Intervals. Seconds pulses at precise intervais are derived from the same frequency standard that controls the radio carrier frequencies. Every minute, except the first of the hour, begins with a 800 -millisecond tone of $1,000 \mathrm{~Hz}$ at WWV and $1,200 \mathrm{~Hz}$ at WWVH. The first minute of every hour begins with an 800 -millisecond tone of $1,500 \mathrm{~Hz}$ at both stations.

The 1-second markers are transmitted throughout all programs of WWW and WWVH except that the 29th of the 59th markers of each minute are omitted.

Time Signals. The time announcements of WWV and WWVH reference the Coordinated Universal Time Scale maintained by the National Bureau of Siandards, UTC(NBS).

The 0 to $\mathbf{2 4}$ hour system is used starting with 0000 for midnight at the Greenwich Meridian (longitude zero). The first two figures give the hour, and the last two figures give the number of minutes past the hour when the tore returns.

At WWV a voice announcement of Greenwich Mean Time is given during the 7.5 seconds immediately preceding the minute.

At WWVH a voice announcement of Greenwich Mean Time occurs during the period 15 seconds to 7.5 seconds preceding the minute. The voice announcement for WWVH precedes that of WWV by 7.5 seconds. However, the tone markers referred to in both announcements occur simultaneously.

Propagation Forecasts. A forecast of radio propagation conditions is broadcast in voice from WWV at 14 minutes after every hour. The announcements are short-term forecasts and refer to propagation along paths in the North Atlantic area, such as Washington, D.C. to London or New York to Berlin.

The propagation forecast announcements are repeated in synoptic form comprised of a phonetic and a numeral. The phonetic (Whiskey, Uniform, or November) identifies the radio quality at the time the forecast is made. The numeral indicates on ascale of 1 to 9 the radio propagation quality expected during the six-hour period after the forecast is issued. The meaning of the phonetics and numerals are:

| Phonetic | Meaning |
| :--- | :--- |
| Whiskey | disturbed |
| Uniform | unsetlled |
| November | normal |


| Numeral | Meaning |
| :--- | :--- |
| One | useless |
| Two | very poor |
| Three | poor |
| Four | poor-to-fair |
| Five | fair |
| Six | fair-to-good |
| Seven | good |
| Eight | very good |
| Nine | excellent |

If, for example, propagation conditions are normal and expected to be good during the next six hours, the coded forecast announcement would be "November Seven."

Geophysical Alerts. Current geophysical alerts (Geoalerts) as declared by the World Warning Agency of the International Ursigram and World Days Service (IUWDS) are broadcast in voice from WWV at 18 minutes after each hour and from WWVH at 45 minutes after each hour.

Weather Information. Weather information about major storms in the Atlantic and Pacific areas is broadcast from WWV and WWVH respectively.

Time Code. The time code is Iransmitted continuously by both WWV and WWVH on a $100-\mathrm{Hz}$ subcarrier. The code format is a modified IRIG.H time code produced at a 1 -pps rate and carried on $100-\mathrm{Hz}$ modulation. The $100-\mathrm{Hz}$ subcarrier is synchronous with the code pulses so that 10 -millisecond resolution is readily obtained.

The code contains UTC time-of-year information in minutes, hours, and day of year. Seconds information may be obtained by counting puises.

The binary coded decimal (BCD) system is used. Each minute contains seven BCD groups in this order: two groups for minutes, two groups for hours, and three groups for day of year. The code digit weighting is $1-2-4-8$ for each BCD group multiplied by 1,10 , or 100 as the case may be. A complete time frame is 1 minute. The binary groups follow the 1 -minute reference marker.

Modulation. At WWV and WWVH, double sideband amplitude modulation is employed with 50 percent modulation on the steady tones, 25 percent for the IRIG-H code, 100 percent for seconds pulses, and 75 percent for voice.

## WWVB Broadcast Services

WWVB transmits a standard radio frequency, standard time signals, time intervals, and UT1 corrections. The station is located near WWV on the same site.

Program. WWVB broadcasts a standard radio carrier frequency of 60 kHz with no offset. It also broadcasts a time code consistent with the internationally coordinated time scale UTC(NBS).

## WWVL Experimental Broadcasts

WWVL broadcasts experimental programs, usually involving multiple frequencies. The station is located in the same building with WWVB and on the same site with WWV.

Effective On UTC, 1 July 1972, regularly scheduled transmissions from WWVL were discontinued. Contingent upon need and availability of funds this staton broadcasts experimental programs on an intermittent basis only.

WWVL transmits only carrier frequencies wilh no modulation. The format and trequencies used by WWVL are subject to change to meet the requirements of the particular experiment being conducted.


## WAVELENGTH-FREQUENCY CONYERSION SCALE

This scale is based on the formula

$$
\lambda_{m}=\frac{300}{f_{M H Z}}
$$

It shows the relationship between free space wavelength $\lambda$ and frequency $f$ and covers a frequency range extending from 300 Hz to 300 GHz , corresponding to wavelengths of $1000 \mathrm{~m}(1 \mathrm{~km})$ to 1 mm .

FOR EXAMPLE: A $60-\mathrm{MHz}$ signal has a wavelength of 5 m . A signal whose wavelength is 3 mm has a frequency of 100 GHz .

Frequency Wovelength
GHz - millimeter (mm)
MHz - meter(m)
kHz - kilometer $\{\mathrm{km}$ )


## Section 2

## Communication

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| Band | Frequency (Wavelength) | Characteristics | Applications |
| :---: | :---: | :---: | :---: |
| Very-low frequency (VLF) | $\begin{aligned} & 20-30 \mathrm{kHz} \\ & (20,000-10,000 \mathrm{~m}) \end{aligned}$ | Very stable; low attenuation at all times. Influenced by magnetic storms. Ground wave exdends over long distances. (No fading out long-time variations occur.) | Continuously operating longdistance station-to-station communication service. |
| Low <br> frequency (L.F) | $\begin{aligned} & 30-300 \mathrm{kHz} \\ & (10,000-1,000 \mathrm{~m}) \end{aligned}$ | Seasonal and daily variations greater than that of VLF; daytime absorption also greater, increasing with frequency. At night similar to VLF although slightly less reliable. | Long-distance station-to-station service (marine, navigational aids). |
| Medium frequency (MF) | $\begin{aligned} & 300-3,000 \mathrm{kHz} \\ & (1,000-100 \mathrm{~m}) \end{aligned}$ | Less reliable over long distances than lower frequencies. Attenuation: low at night, high in daytime; greater in summer than in winter. Low attenuation at night is due to sky-wave reflection. Ground-wave attenuation is relatively high over land and low over salt water. | Commercial broadcasting police, marine and airplane navigation. |
| High frequency (HF) | $\begin{aligned} & 3-30 \mathrm{MHz} \\ & (100-10 \mathrm{~m}) \end{aligned}$ | Dependent on ionospheric conditions, leading to considerable variation from day to night and from season to season. Attenuation low under favorable conditions, and high under unfavorable conditions. at medium to very long distances. | Medium and long-distance communication service of all types. |
| Very-high frequency (VHF) | $\begin{aligned} & 30-300 \mathrm{MHz} \\ & (10-1 \mathrm{~m}) \end{aligned}$ | $30-60 \mathrm{MHz}$ sometimes affected by ionosphere. Quasi-optical transmission (similar to light, but subject to diffraction by surface of the earth). | Tolevision, FM commercial broadcasting, radar aimplane navigation, shor-distance cormmnications. |
| Uiltra-high frequency (UHF) | $\begin{aligned} & 300-3.000 \mathrm{MHz} \\ & (100 \cdot 10 \mathrm{~cm}) \end{aligned}$ | Substantially same as above; slightly less diffraction. Under abnormal conditions, can be refracled by troposphere similar to sky-wave refraction. This ohen results temporarily in abnormally long ranges of Itansmission. | Television, radar, microwave relay, short-distance communications. |
| Super-high frequency (SHF) | $\begin{aligned} & 3,000 \cdot 30,000 \\ & \mathrm{MHz}(10.1 \mathrm{~cm}) \end{aligned}$ | Same as above. <br> $1-\mathrm{cm}$ range has broad water-vepor absorption band (slight $\mathrm{O}_{2}$ absorplion). | Radar, microwave relay, short distance communications. |

Principal ground-to-ground communication modes, utilizing the microwave ( 70 MHz to 20 GHz ) region of the spectrum. Characteristically wide-band ( 100 kHz to 20 MHz ) service.

| LIME OF SIGHT (LOS) | 0 to 35 miles, depending on ( h ). | $\begin{aligned} & 0.1 \text { to } 10 \mathrm{~W}, \\ & \text { two to } 10 \mathrm{ft} \\ & \text { antennas } \end{aligned}$ | Low-cost, high-performance wide-band system; replaces costly right-of-way maintenance of coaxial or multiple cable or over head wiring. |
| :---: | :---: | :---: | :---: |
|  | upto $1 / 2$ circumference of earth depending on satellite orbit and ( $\theta$ ) | 1 to 15 kW , 30 to $85-\mathrm{ft}$ antennas | Only practical system of global coverage using three active synchronous satellites ( 22,000 miles from earth) or a number of orbiting satellittes (dependent on distance covered and alttude) in conjunction with multiple earth earth stations. |
| DIFFRACTIOM (Plane Surface) | 30 to 70 miles, depending on (h) and $\mathrm{N}_{5}$ ) | 0.1 to 100 w , six to $28-\mathrm{ft}$ anternas | Diffraction mode is very specialized form of UHF used only rarely where rugged terrain prevents use |
|  | 30 to 120 miles, depending on ( h ), $\left(\mathrm{N}_{\mathrm{s}}\right)$ and $\left(\mathrm{G}_{0}\right)$ | $\begin{aligned} & 0.1 \text { to } 100 \mathrm{~W}, \\ & \text { six to } 28-\mathrm{ft} \\ & \text { antennaas } \end{aligned}$ | Great attention is belng given |
| oiffraction (Rough Surface) | 30 to 120 miles, depending on (b), $\left(N_{5}\right),\left(G_{0}\right)$, and ( $\mathrm{A}_{0}$ ) | 0.1 to 100 W , six to $28-\mathrm{ft}$ antennas | for utilization in trope path predictions. |
|  | 70 to 600 milles, depending on many factors | $\begin{aligned} & 1 \text { to } 100 \mathrm{~kW}, \\ & 10 \text { to } 120-\mathrm{ft} \\ & \text { antennas, } \\ & \text { refined modula, } \\ & \text { tion and recelver } \\ & \text { technigues } \end{aligned}$ | Only practical wide-band, reliable ground-based method of achieving 70 to 600 mile hop where unsuitable inter vening territory prevents use of LOS or diffraction modes. |

## INTERNATIONAL TELEVISION STANDARDS

This table outlines pertinent characteristics of the current TV standards used throughout the world. The video frequency-channel arrangements are also shown. The systems have been designated by letter and are in use or proposed for use in the countries listed.

| Country | Standard Usad ${ }^{\text {a }}$ | country | Standard Usad ${ }^{\circ}$ |
| :---: | :---: | :---: | :---: |
| Argontina | N | Meroico | M |
| Ausirala | 8 | Monaco | E, G |
| Ausinis | E. G | Morocco |  |
| Belgium | C, H | Nelherlands | B. G |
| Brazil | ${ }^{M}$ | Netheriands Antilitas | M |
| Bulgaria | D, K | New Zealand | 8 |
| Caneda | M | Nigeria | 8 |
| Chile | M | Norway | 8 |
| China | D | Paklistan | 8 |
| Cohumbia | M | Panama | H |
| Cuba | M | Pers | M |
| Czechoshovekia | D | Philipines | H |
| Denmank | B | Potend |  |
| Egypt | 8 | Portugal | B, 6 |
| Finland | B, G | Procdesia | B |
| Franca | E, L | Pomania | $K$ |
| Germany (Easl) | 8 | Saudi Arabla | B |
| Germany (West) | B, G | Singapore | 8 |
| Greece | ${ }_{8}$ | South Arica | 1 |
| Hong Kong | B. 1 D. | Spain | B, G |
| Hungary | D. K | Sweden | B, G |
| India | 8 | Swilzerfand | B. $G$ |
| Iran | 8 | Turkey | B |
| lreland | A | United Kingdom | A. 1 |
| 1srael italy | - ${ }^{\text {B }}$ | United States of America | M |
| Japen | M | Ropublics | D |
| Korra | C. L |  |  |
| Luxambourg | F | Yugaslavia | $\text { 8. } 6$ |
| ${ }^{\text {C }}$ Letter designations correspond to those in the following table. |  |  |  |


|  | $A$ | M | $N$ | $B$ | $c$ | $G$ | $H$ | $I$ | $D, K$ | $L$ | $F$ | $E$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lines/frame | 405 | 525 | 625 | 625 | 625 | 625 | 625 | 625 | 625 | 625 | 819 | 819 |
| Fields/sec | 50 | 60 | 50 | 50 | 50 | 50 | 50 | 50 | 50 | 50 | 50 | 50 |
| Interlace | 2/1 | 2/1 | 2/1 | $2 / 1$ | 2/1 | $2 / 1$ | 2/1 | $2 / 1$ | 2/1 | 2/1 | 2/1 | 2/1 |
| Frames/bec | 25 | 30 | - | 25 | 25 | 25 | 25 | 25 | 25 | 25 | 25 | 25 |
| Lines/sec | 10125 | 15750 | - | 15625 | 15625 | 15625 | 15625 | 15625 | 15625 | $15625^{\circ}$ | 20475 | 20475 |
| Aspect ratio ${ }^{\text {a }}$ | 4/3 | 4/3 | - | 4/3 | 4/3 | $4 / 3$ | 4/3 | $4 / 3$ | 4/3 | 4/3 | 4/3 | 4/3 |
| Video band (MHz) | 3 | 4.2 | 4.2 | 5 | 5 | 5 | 5 | 5.5 | 6 | 6 | 5 | 10 |
| RF band ( MHz ) | 5 | 6 | 6 | 7 | 7 | 8 | 8 | 8 | 8 | 8 | 7 | 14 |
| Visual polerity ${ }^{2}$ | + | - | - | - | $+$ | - | - | - | - | $+$ | $+$ | + |
| Sound medulation | A3 | F3 | - | F3 | A3 | F3 | F3 | F3 | F3 | F3 | A3 | A3 |
| Pre-ernphagis in microseconds | - | 75 | - | 50 | 50 | 50 | 50 | 50 | 50 | - | 50 | - |
| Deviation ( $\mathrm{kHz}_{2}$ ) | - | 25 | - | 50 | - | 50 | 50 | 50 | 50 | - | - | - |
| Gamma of picture signal | 0.45 | 0.45 | - | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.6 |

Notes:
${ }^{1}$ In all systems the sonnuing sequence is from left to right and top to bottom,
${ }^{2}$ All visual carriers are amplitude modulated. Positive polarity indicates that an increase in light intensity causes an increase in radiated power. Negative polarity (as used in the US-Standard M) means that a decrease in light inteasity causes an increase in radiated power.


This nomogram relates receiver-transmitter distance, wavelength and free space attenuation. It can also be used to convert between nautical and statute miles and between frequency and wavelength.

FOR EXAMPLE: A signal from a $200-\mathrm{MHz}$ transmitter will be attenuated 125 dB before it reaches a receiver located 100 nautical miles away.

At a distance of 200 nautical miles, and a system gain of 130 dB , the highest usable frequency is 180 MHz .
The maximum distance between a transmitter-recelver-antenna system with a total gain of 125 dB operating at 500 MHz is 45 statute miles.


## SIGNAL-STRENGTH NOMOGRAM

This nomogram is used to compute signal-strength input at the receiver based on a formula that converts field intensity at the receiving antenna to receiver input voltage.

If field intensity $\epsilon$, in microvolts per meter, of a given signal $f$, in MHz , is known, the signal strength $\mathbf{E}$, in microvolts, is determined for an input impedance of 50 ohms ( E , in $\mu \vee$ for $R=50$ ) and may be adjusted for any value of input impedance between 30 and 5000 ohms ( $E_{r}$ in $\mu \vee$ for $30 \leqslant R \leqslant 5,000$ ). An isotropic antenna, no-loss transmission line is assumed.

Signal strength for receiving antennas of gain > $1(0 \mathrm{~dB})$ are solved first by finding from the chart the voitage input for a system with an isotropic antenna and then adjusting the answer using the relation: $\mathrm{G}=20 \log \left(\mathrm{E}_{r}^{\prime} / \mathrm{E}_{r}\right)$ where G is the gain of the antenna referred to isotropic; $\mathrm{E}_{r}^{\prime}$ is the voltage input to be found; and $\mathrm{E}_{r}$ is the voltage input.

(Reprinted from Electronics, June 6. 1958, copyright McGraw-Hill, Inc., 1958)

## NOMOGRAM RELATING TRANSMITTER OUTPUT, TRANSMISSION LOSS, AND RECEIVER INPUT

This nomogram shows the available input voltage (microvolts into 50 ohms), if transmitter output in watts and transmission loss in decibels are known. It can also show the maximum permissible transmission loss if transmitter power and receiver requirements are given, or it can be used to determine the required transmitter output for a given transmission loss and receiver input voltage. Microvolts (into 50 ohms) may be directly converted to dBm on the left scale and watts may be converted to dBm on the center scale.

FOR EXAMPLE: (1) For a transmitter output of 5 W and a transmission loss of 90 dB , the receiver input will be $500 \mu \mathrm{~V}$. (2) For a minimum of $50 \mu \mathrm{~V}$ at the receiver, and a transmitter output of 5 W , the transmission loss may not exceed 110 dB .
dBm and dB scales are arithmetic Watts and microvolts scales are logarithmic

TOTAL LOSS BETWEEN TRANSMITTER OUTPUT AND RECEIVER INPUT-dB

RECEIVER INPUT MICROVOLTS INTO 50 OHMS dBm 10,000 ${ }^{20,000} T^{-20}$ TRANSMITTER OUTPUT $5.000+-30$ $4.0000-$ $3,000-00$ ,

## TRATTS dBm

 WATTS0,000
+70

(2)

This nomogram is based on the noise figure of a receiver as given by the equation:

$$
N F=\frac{\left(m E_{0} \sqrt{P_{n} / P_{5}}\right)^{2}}{2 R(4 K T \Delta f)}
$$

where $N F=$ noise figure; $m=$ modulation index; $P_{n}=$ noise power, $P_{s}=$ signal power; $K=$ Boltzmann's constant or $1.38 \times 10^{-23}$ joules $/{ }^{\circ} \mathrm{K} ; R=$ antenna resistance; $T=$ degrees Kelvin; $\Delta f=6-\mathrm{dB}$ audio bandwidth, and $E_{0}=$ signal generator output in $\mu \mathrm{V}$.

Nominal antenna impedance is 520 hms and the temperature can be approximated at $300^{\circ} \mathrm{K}$.
To find the noise figure of a receiver, it is only necessary to place a straightedge across the sensitivity and audio bandwidth points, extending it to intersect the noise figure line.

FOR EXAMPLE: Sensitivily of $10 \mu \mathrm{~V}$ and bandwidth of 6 kHz gives a noise figure of 100 , or 20 dB .


## LINE-OF-SIGHT TRANSMISSION RANGE NOMOGRAM SHOWING THE APPROXIMATE TRANSMISSION RANGE OF SIGNALS IN THE VHF BAND

The theoretical maximum distance that can be covered is equal to the geometrical or "optical" horizon distance of each antenna, and is defined by the formula $D=1.23 \sqrt{H_{t}}+1.23 \sqrt{H_{t}}$, where $D$ is in miles and $H_{t}$ and $H_{t}$ are the height in feet, above effective ground level, of the receiving and transmitting antennas. Atmospheric diffraction increases the distance by a factor of $2 / \sqrt{3}$ which defines the "radio" path undernormal or standard diffraction, by the formula $\mathrm{D}=1.41 \sqrt{H_{r}}+1.41 \sqrt{H_{r}}$.

FOR EXAMPLE: With a receiving antenna height of 30 ft and a transmitting antenna height of 100 ft , the "optical" horizon is 19 miles and the "radio" horizon is 21.5 miles.


The energy available from a radar transmitter is often the limiting factor in determining the maximum free space range. This nomogram relates the four interdependent radar equations involving peak power, average power, energy, duty cycle, pulse width, pulse repetition rate and pulse interval based on the following equations:

$$
\frac{P_{A V}}{P_{P}}=d=\tau f_{r} \text { and } P_{p} \tau=E=P_{A V} t
$$

where

$$
\begin{aligned}
P_{p} & =\text { peak power in watts } \\
P_{A V} & =\text { average power } \\
E & =\text { energy in joules } \\
d & =\text { duty cycle } \\
\tau & =\text { pulse width in microseconds } \\
t_{f} & =\text { pulse repetition rate in pulses } / \mathrm{sec} \\
t & =\text { pulse interval in microseconds }
\end{aligned}
$$

FOR EXAMPLE: A pulse repetition rate of 1,000 pulses $/ \mathrm{sec}$ with a pulse width of $5 \mu \mathrm{sec}$ will give a duty cycle of 0.005 . For a peak power of 100 kW . join this value on the $P_{P}$ scale with 0.005 on the duty-cycle scale and read an average power of 500 W . Joining the 100 kW point with the pulse width of $5 \mu \mathrm{sec}$ shows the energy as 0.5 J. (To crosscheck, connect the average power of 500 W with $1,000 \mathrm{pps}$ rep rate, which also yields 0.5 J .)



Coarse range information is provided by position of signal in broad azimuthal trace.


Single signal only. Signal nppears as "wingspot," position giving azimuth and elevation errors. Length of wings inversely proportional to range.


Signal appears as tro dots. Left dot gives range and azimuth of target. Relative position of right dot gives rough indication of elevation.


Antenna scen is conical. Sigual is a circle, the radius proportional to range. Brightest part indicates direction from axis of cone to target.


Same as type A, except time base is citcular, and signals appear as radisl pips.


Type A with lobe-switching antenna. Spread voltage splits signals from two lobes. When pips are of equal size, antenna is on target.


RANGE
Same as type $K$, but signals from two lobes are placed back to back.


Type $A$ with range step or range notch. When pip is aligned with step or notch, range can be read from a dial or counter.


A combination of type $K$ and type M.


Range is measured radially from the center.
(From Radar System Engineering by Louis Ridenour. Copyright © 1947 by McGraw-HIII Book Company. Used with pertission of McGraw-Hill Book Company.)

## ANTENNA REFERENCE CHART

Antennas may be classified as linear radiators or elements, apertures arrays, and traveling wave types. Basic information on a few types of antennas is tabulated. For each type the following is given: the antenna name, physical size in wavelengths, a line drawing superimposed on coordinate axis, the impedance $R$ in ohms at the resonant frequency $f_{f}$, the half-power ( 3 dB ) bandwidth in percent, the gain in dB above an isotropic radiator, as well as the conventional half-wavelength dipole, the polarization for the given configuration, and a set of Fraunhofer Zone field strength patterns for each of the three orhogonal planes of the axis system shown.

An isotropic radiator is given, even though such an antenna for electromagnetic waves does not exist. It is a convenient and frequent reference, however, for gain and pattern measurements.

The antennas tabulated may be vertically or horizontally polarized radiators. The configuration shown in the chart is the one most frequently used in practice. The antennas listed may be fed by balanced transmission lines, by coaxial lines and a balun (balanced-to-unbalanced transformer) when necessary, or in some cases by waveguides. Aperture antennas, such as parabolic dishes and horns, are usually fed by waveguides and, for such feed systems, impedance is not too meaninglut.


## roadsids Array

$l,=\lambda / 2$ polarization: verlicat

Theoretical Gain of Broadside $1 / 2$.


| $5 / 4$ | 4.8 |
| :--- | :--- |
| $3 / 4$ | 4.6 |
| $1 / 2$ | 4.0 |
| $3 / 4$ | 2.4 |
| $1 / 4$ | 1.0 |
| $1 / 4$ | 0.3 |

Theoratical Gain ol Broadside $1 / 2 \times$ eloments for dilfsent numbers of elements.

| Number of <br> elemenls | Gain, d8 <br> above $\mathbf{0}$ ipole |
| :---: | :---: |
| 2 | 4.0 |
| 3 | 5.5 |
| 4 | 8.0 |
| 5 | 9.0 |
| 6 |  |

End Fire Aeray
$h=\lambda / 2$
polarizalion: verlical

| $5 / 18$ | 1.7 |
| :--- | :--- |
| 13 | 2.2 |
| $3 / 8$ | 3.0 |
| $1 / 48$ | 3.8 |
| $1 / 8$ | 4.1 |
| $1 / 8$ | 4.3 |



## Collinear Array

$L=2 / 2$


| Spacing "a" between centors of adjacent I/2 $\lambda$ elements | Number of $1 / 2 \times$ elements in array versus gein in dB above a paference Dipose |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 2 | 3 | 4 | 5 | 6 |
| $a=1 / 2 \lambda$ | 1.8 | 3.3 | 4.5 | 5.3 | 6.2 |
| a $=1 / 4$ | 3.2 | 4.8 | 6.0 | 7.0 | 7.8 |




## MICROWAVE ANTENNA CHART

Shown here is the relationship between circular antenna aperture size, frequency, and gain. Also listed are the antenna performance requirements for various system applications. Practical factors, such as whether the antenna is solid or perforated, the type of aperture illumination, accuracy of construction, and shadowing from the feed system will tend to reduce the gain somewhat.

FOR EXAMPLE: To achieve a gain of 40 dB at 10 GHz requires an antenna with a diameter of 10 m . An antenna with a diameter of 100 m has a gain of 100 dB at 100 GHz .

Antenna Performance Requirements

| APPLICATHON | PATIEAN | POLAfII* 2ATHOH | GAIN <br> 0. $\mathrm{Cd}_{\mathrm{B}}^{5}$ <br>  tsoleqpic rod. | BEAMWIDTH <br> (H) degraes | POINTING accuracy. to dngrees | TYPICAL TYPES |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\dagger_{\text {, }}$ SATELIITE Link or Prober | Pantilal Boam | any | $10 \mathrm{ta} 40 \mathrm{~dB}$ or mors | BD to 2 or lass | 6 to 28 or better | Hapri, Phased artray, Parahola, Catsegrain |
| 2. POINT TO POINT RELAY <br> e. On Earth <br> b. Earth to Sateilite to Earth <br> c. Salellite to Satellite | Pencill Beam | 1ny | a. 3010120 <br> b. $\$ 019120$ <br> c. 5010180 | $\begin{aligned} & \begin{array}{l} 5.8 \times 10^{-1} 10 \\ 10 \times 10^{-6} \end{array} \\ & 5.8 \times 10^{-1} 10 \\ & 1.8 \times 10^{-5} \end{aligned}$ | $\begin{aligned} & 5.8 \times 10^{-2} 10 \\ & 1.8 \times 10^{-4} \end{aligned}$ | Horn, Pariboll Cathogralh |
| 7. BROADCAST <br> a. Earih Trans. <br> b. Sat. Trans. | omnidit, <br> wide of fan <br> beam | An) | 2. 3 to 40 <br> b. 1 to 10 | $\begin{aligned} & 100 \text { to } 1.9 \\ & 180 \text { to } 80 \end{aligned}$ | 10 to. 16 | a. Unileal radietion <br> b. Cylindrical paldodita |
| 4. NAVIGRTION | omnidir. or lun beant | *ny | 3 to 50 | 10060.59 | 40 tor.05s | Vortical rathater. Horti, or Partowas |
| 5. MADAR <br> a. Search <br> b. Track | esc ${ }^{2}$ <br> Pancll Borm | any | 40 to 120 | . $8 \mathrm{to} 1.8 \times 10^{-4}$ | .18 ta $1.4 \times 10$ | Mern, Paratiole, Castetrific Phted atray |
| 6. RADIO ASTRONOMY <br> n. Passiva <br> b. Aclly | Pancll Buam | paly | $\begin{aligned} & 50 \text { to } 160 \\ & \text { or } \mathrm{p} \text { tente\% } \end{aligned}$ | -5840 $10.8 \times 10-6$ | . 057 to $1.8 \times 10^{-1}$ | Parihath Gagengraln. Prouted arrify |
| 7. RADIOMETRY Industrial | any | *iry | undnown | unknown | Unionuman | Any |

Antenna Gain and Size vs Frequency for Uniformly Ifuminated Circular Aperture


## ANTENNA EFFECTIVENESS NOMOGRAM

Antennas are judged on the basis of radiation efficiency or their VSWR. Radiation efficiency is the ratio of the radiated power to the total power fed into the antenna terminals. Total power is the sum of the radiated power and the power lost in ohmic losses in the form of heat. The powergoing into the antenna terminals is the power which a transmitter can put out less the power reflected due to antenna mismatch. Antenna effectiveness is the ratio of the radiated power to the power which a transmitter can put into a matched load, i.e., the forward or incident power.

$$
\text { Effectiveness }=\frac{4 \text { VSWR }}{(V S W R+1)^{2}} \times \text { efficiency }
$$

FOR EXAMPLE: A $60 \%$ efficient antenna with a $2.5: 1$ VSWR has an effectiveness of $48 \%$ compared to a perfectly matched $100 \%$ efficient antenna.

NOTE: in some cases an antenna can be made more effective by lessening its efficiency if this will produce a sufficient reduction in the VSWR.


Characteristics of Various Types of Transmission Lines Erected Parallet to a Perfectly Conducting Earth.

| LOOARITHHS TO THE GASE 10 |  |  |  |
| :---: | :---: | :---: | :---: |
| LINE CONFIOURATIOH |  | CHARACIERISIIC IMPEOAMCE |  |
| Single wir |  | $2_{0}=158 \mathrm{Log} \frac{2 h}{r}$ | $L_{\text {ond }}=1$ |
| 2-Wire balonced |  | $2_{0}-216 \log \frac{3}{r}$ | $l_{\text {ond }}=0$ |
| 2-Wire I wire grounded |  | $I_{0}=276 \frac{\log \frac{5}{r} \log \left[\hat{\rho}^{\hat{2}} t\right]}{\log \left[\rho^{2}\left(\frac{5}{5}\right)^{2}\right]}$ | $I_{\text {and }} \Rightarrow I_{1} \frac{\log \frac{5}{r}}{\log \frac{2 h}{r}}$ |
| 3-Wire 2 wires grounded |  | $Z_{0} \sim 69\left[\log \frac{3^{3}}{2 r^{3}}-\frac{\left(\log \frac{5}{2}\right)^{2}}{\log \frac{2 h^{2}}{5 L}}\right]$ | $\begin{array}{ll} I_{\text {Gnd }}=I_{1} & \log \frac{5}{7 r} \\ \rho-\frac{2 h}{s} & \log \frac{52^{2}}{2 r} \end{array}$ |
| 4-Wire balanced |  | $z_{0}=138\left(\log \frac{3}{5}\right)-21$ | $t_{\text {Gnd }}=0$ |
| 4-Wire 2-wires grounded |  | $\begin{aligned} & Z_{0}=138\left[\frac{\log \frac{5}{\pi h} \log \left[\rho^{4} \frac{3}{\pi t}\right]}{\log \left[\rho^{4}\left(\frac{5}{r v}\right)^{2}\right]}\right] \\ & \rho_{=}=\frac{2 h}{3} \end{aligned}$ | $\operatorname{lond}_{\text {ond }}=I_{1} \frac{\log \frac{5}{r \sqrt{2}}}{\log \frac{\rho^{2} s}{r \sqrt{2}}}$ |
| 5- Wire 4 wires grounded |  | $z_{0}=138 ;\left[\log \frac{2 h}{r}-\frac{\left[\log 2 \rho^{2}\right]^{2}}{\log \left[\rho^{3} \frac{h 2 y}{r}\right.}\right]$ | $I_{G n d}=l_{1} \frac{\log \frac{3}{r d \sqrt{2}}}{\log \frac{5 p^{4}}{r \sqrt{2}}}$ |
| Concentric (cocaxial) |  | $x_{0}=138 \frac{\log \frac{c}{b}}{\sqrt{1+\left(\frac{c-1) \omega}{5}\right.}}$ <br> e $\boldsymbol{\sim}$ Dielectric consfant of insulating moterial |  |
| Double tooxiol balonced |  | $L_{0}=2.76 \frac{\log \frac{c}{b}}{\sqrt{1+\frac{(\varepsilon-1) \omega}{5}}}=$ |  |
| Snitlded poir molaneod |  | $z_{0} \frac{120}{\sqrt{2}}\left[2.303 \log \left(2 v \frac{1-\sigma^{2}}{1 \cdot \sigma^{2}}\right)-\right.$ <br> c- Dieletric constant of <br> e. Unity for goseovs med <br> $v=\frac{h}{b} ; \sigma=\frac{h}{b}$ | $\left.\frac{4 y^{2}}{6}\left(1-4 \sigma^{2}\right)\right]$ <br> dium m |

(From Radio Engineers' Handbook by Frederick E.Terman. Copyright ©1943 by McGraw-Hill Book Company. Used with permission of McGraw-Hill Book Company.)

This nomogram determines the theoretical exact impedance of air-dielectric parallel lines in air or in a vacuum, and remote from any conducting plane. It covers conductors having diameters from 0.01 to 5 in ., spaced from 0.01 to 100 in . center-to-center.

$$
\begin{gathered}
z_{0}=276 \log _{10} \frac{2 D}{d} \\
D>2 d
\end{gathered}
$$

FOREXAMPLE: (1) The impedance of a line using \#12 wire spaced $11 / 2$ in. is 430 ohms. (2) What is the wire diameter for a $300-0 h m$ line spaced $1 / 4 \mathrm{in}$ ? Answer: 0.20 in ,

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SC-idver plated copper, C-bor* capper, PE-polyealhylent, HCY-now-cantaninating vinyl,
Y-polyrinyichloride, IC-linsed copper. CN-mpperveld
start here to select by characteristic lmpeoance

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## ULTRA-HIGH FREQUENCY HALF-WAVE SHORTING-STUB NOMOGRAM

This nomogram is used to determine the length in inches of shorting stubs required to eliminate interference in the UHF television range.

FOR EXAMPLE: To eliminate an interfering signal at 575 MHz (channel 31) requires a $81 / 2 \mathrm{in}$. long hall-wave shorting stub, if 300 -ohm Iwin lead is used. If 75 -ohm twin lead is used, the stub has to be $71 / 4$ in. for the same frequency.


This nomogram gives the actual length of line in centimeters and inches when given the length in electrical degrees and the frequency provided that the velocity of propagation on the transmission line is equal to that in free space. The length is equal to that in free space and is given on the $L$ scale intersection by a line between $\lambda$ on $\ell^{\circ}$. FOR EXAMPLE:

$$
\begin{aligned}
f= & 600 \mathrm{MHz} \quad \ell^{\circ}=30^{\circ} \\
& \text { Length } L=1.64^{\prime \prime} \text { or } 4.2 \mathrm{~cm}
\end{aligned}
$$



This nomogram is used to determine the VSWR and the magnitude of the reflection coefficient by the use of width-of-minimum measurement fechnique. This technique relies on the fact that there are two comparatively easy-to-find 3 - dB points straddling any minimum, as illustrated.

FOR EXAMPLE: A slotted-line width-ot-minimum measurement of 0.18 cm , with a $1-\mathrm{GHz}$ source, indicates a VSWR of 53 or a reflection coefficient magnitude of 0.963 .

NOTE: The signal-to-noise ratio at the bottom of the minimum must be at least 10 dB for accurate results.


## SLOTTED UNE WIDTH-OF-MINIMUM ATTENUATION CALCULATION NOMOGRAM

This nomogram is used to determine the total attenuation between the probe position and the reference plane based an width-of-minimum measurements.

FOR EXAMPLE: with a shor circuit termination at the reference plane, if the width-of-the-minimum measured 30 cm from the reference plane is 0.014 cm at 3.5 GHz , then the attenuation is 0.045 dB .

NOTE: The signal-to-noise ratio at the bottom of the minimum should be at least 10 dB for accurate results.


## WAVEGUIDE NOMOGRAM

This nomogram relates three significant waveguide characteristics:

```
waveguide wavelength ( }\mp@subsup{\lambda}{g}{}\mathrm{ )
free space wavelength ( }\mp@subsup{|}{0}{\prime})\mathrm{ or frequency (f)
cutoff wavelength ( }\mp@subsup{\lambda}{c}{}\mathrm{ )
```

The vertical scale gives waveguide wavelength in centimeters. The horizontal scale is for the cutoff wavelength, and the points corresponding to the cutoff wavelength in the $\mathrm{TE}_{10}$ mode of three common waveguides are indicated. The sloping center scale is calibrated in free space wavelength and frequency.

FOR EXAMPLE: (1) The waveguide wavelength at 6 GHz ( 5 cm free space wavelength) in an RG-50 waveguide is 7.17 cm . (2) Measurement on an RG-51 waveguide whows the waveguide wavelength to be 6.5 cm . The frequency is 7 GHz , which corresponds to a free space wavelength of 4.27 cm .


If a transmission line is not terminated in its characteristic impedance, then some of the energy sent along the line will be reflecled back, and standing waves form on the line. The ratio of the maximum to the minimum voltage of the standing waves is the VSWR (voltage standing wave ratio) and indicates the effectiveness of the match between line and load. For a perfectly matched line, the VSWR is 1 . The VSWR can be given in a number of ways:

$$
\text { VSWR }=\frac{Z_{L}}{Z_{0}}=\frac{E_{\max }}{E_{\min }}=\frac{1+\sqrt{\frac{\text { Reflected power }}{\text { Forward power }}}}{1-\sqrt{\frac{\text { Reflected power }}{\text { Forward power }}}}
$$

This nomogram is based on the last expression and solves for VSWR from measurements of reflected power and forward power.

FOR EXAMPLE: For a forward power of 180 W and a reflected power of 2.7 W , the VSWR is $\mathbf{1 . 2 7}$.


## VSWR REDUCTION AS A RESULT OF ATTENUATION

This nomogram relates load VSWR, input VSWR, and attenuation, It can be used to find the resultant VSWR with a given amount of attenuation, or to determine the attenuation required for a given VSWR.

FOR EXAMPLE: (1) A $5-\mathrm{dB}$ attenuator will reduce input VSWR to 1.23 if the load VSWR is 2.0 . (2) The required attenuation to reduce a load VSWR of 1.8 to an input VSWR of 1.06 is 10.0 dB .


Radar or sonar frequency may be converted to hundreds of miles per hour or knots per hour by using this chart. The base sonar frequency in kHz is given on the left scale and the base radar frequency in GHz is given on the right. Doppler frequency, in Hz for sonar and hundreds of Hz for radar, is shown at the bottom. The diagonals represent target rate of change of range, which is the velocity speed vector in the source's direction.

The basic formula for Doppler speed is:

$$
\text { Doppler frequency }=\frac{\text { base } f . \times \text { target range rate }}{\text { signal velocity in medium. }}
$$

The signal velocity in medium is $5,000 \mathrm{ft} / \mathrm{sec}$ for sonar and $186,000 \mathrm{mi} / \mathrm{sec}$ for radar.
FOR EXAMPLE: (1) The base frequency of a sonar system is 40 kHz and its Doppler frequency is 55 Hz . The speed vector is found by the intersection of these two lines on the chart to be approximately 4.1 knots. (2) The base frequency of a radar system is 11 GHz , and the Doppler frequency is $8,000 \mathrm{~Hz}$. The speed vector of the aircratt in miles per hour is found (from the intersection of these two lines) to be approximately 480 mph .


## DOPPLER FREQUENCY NOMOGRAM

This nomogram solves for the Doppler frequency, which is produced as a result of relative motion between a transmitter and its receiver or target. The Doppler frequency is a function of transmitted frequency and velocity of motion. The angle to the velocity vector determines the actual relative velocity. For a navigation system (Fig. A) in an airplane, the earth is the target, and the angle $A$ is the acute angle between the aircraft heading and the radar beam. In this case the Doppler shilt is downward. A forward-looking radar will produce an upward Doppler shift. For surveillance-type radars (Fig. B), the angle $A$ is the acute angle between the radar beam and target velocity. (Note that the nomogram is based on the Doppler equation for radar and that the Doppler shift for a passive listening device will be half the frequency indicated.)

FOR EXAMPLE: A helicopter navigation system transmits at 10 GHz at an angle of $70^{\circ}$. What is the audio bandwidth required for aircraft veiocities of 10 through 200 mph ? On the left scales, connect 10 GHz and 10 mph to the turning scale. From that point on, the turning scale connecting through $70^{\circ}$ gives 100 Hz as the lowest frequency. Repeating the steps using 200 mph in place of 10 mph shows the highest frequency to be 2 kHz . Thus the required bandwidth is 100 to $2,000 \mathrm{~Hz}$. The nomogram is based on the formula

$$
f_{\sigma}=89.4 \frac{V}{\lambda}
$$

where
$f_{c}=$ Doppler frequency $(\mathrm{Hz})$
$V=$ velocity in miles per hour
$\lambda=$ transmitted wavelength in centimeters
Angle-to-velocity vector depends on type of target.



This graph determines the combined signal level and shows the number of dB that must be added to the larger signal.

FOR EXAMPLE: Two in-phase signals are -25 dB and -27 dB respectively. The difference is 2 dB and, from the graph, 2.2 dB must be added to the larger signal. Thus, the combined signal power level is -25 dB plus 2.2 dB or -22.8 dB.


When making transmission loss or crosstalk measurements, the presence of noise is a potential source of error. If the total voltage measured across the load resistance when a signal is being transmitted is $\mathbf{1 5} \mathbf{d B}$ or more greater than the noise voltage alone, the error in the received voltage measurement will be negligible. It, however, the dB difference between the combined signal and noise voltage and the noise voltage alone is less than 15 dB , a correction must be made. To do so, two voltage measurements must be made. Namely, (1) the noise power in dBm , and (2) the combined noise and signal power in dBm . On the horizontal axis locate the point equal to the difference between the two powers and read on the vertical axis the number of dB to be subtracted from the noise plus signal power and obtain the power of the signal alone.

FOR EXAMPLE: The difference between the measurements of combined noise and crosstalk and noise alone is 5 dB . Thus, 1.7 dB must be subtracted from the combined signal and noise level to obtain the level of the signal alone.


Power density is related to field strength by the equation

$$
P=\frac{E_{2}}{10 \pi}
$$

where

$$
\begin{aligned}
P & =\text { the power density } \\
E & =\text { the field strength } \\
120 \pi & =\text { the resistance of free space }
\end{aligned}
$$

and
This chart converts between field strength and power density.

FOR EXAMPLE: A field strength of $3,000 \mu \mathrm{~V} / \mathrm{m}$ corresponds to a poler density of $0.024 \mu \mathrm{~W} / \mathrm{m}^{2}$ and is 70.5 dB above $1 \mu \mathrm{~V} \cdot \mathrm{~m}$.

## Q SIGNALS (MNEMONIC CODE)

The Q code was first adopted in 1912 by international treaty agreement to overcome the language barriers faced by ship operators of all nations as they fried to communicate with shore stations all over the world. Many of the original list of 50 signals are still in use with their definitions unchanged. Many more have been added from time to time, and the official meanings of some signals have been changed. In addition, many signals have been informally adopted for use by amateurs in situations not covered by the official lists.

The list below includes virtually every $Q$ signal which could, even remotely, be thought to have an application in amateur radio communication. To simplify the task of finding the definition of an unfamiliar signal, we have combined all the signals into a single alphabetical list, mixing "official" and unofficial signals. The definitions listed are, in most cases, the official ones, taken verbatim from the trealy. In other cases, where definitions are not the official ones, they are as amateurs universally understand them, for purposes of amateur communications. The ON signals, adopted by ARRL for traffic net use, have official definitions which refer to aeronautical situations.

QAM What is the latest available meterological observation for (place)?
The observation made at (time) was . . . .
QAP Shall I listen for you (or for . . . 0 on.. kHz ? Listen for me (or for . . .) on . . . kHz.
QAF May 1 stop listening on the watch frequency for . . . minutes? You may stop listening on the watch frequency for . . . minutes?
QBF Have we worked before in this contest? We have worked before in this contest.
OHM I will tune from the high end of the band toward the middle
(Used after a call or CQ.)
QIF What frequency is . . . using? He is using . . . kHz .
OJA is my RTTY (1-tapie, 2-M/S) re. versed?
It is reversed.
Q.JB Shall 1 use (1-TTY, 2-reperf)? \{For RTTY use.) Use (1-TTY, 2-reperf)
QJC Check your RTTY $11-T^{\circ} \mathrm{C} .2$-auto head, 3-repert, 5-Peinter, 7-keyboard).

QJD Shall I transmit (1-letters, 2-figs? ? For RTTY:
Transmit (1-letters, 2-1igs).
QJE Shall I send (1-wide, 2 -narrow, 3-correct) RTTY shift?
Your RTTY shift is (1-wide, 2-narrow, 3-correct).
QJF Does thy RTTY signal check out OK? Your RTTY signal checks out OK.
OJH Shall I transmit 11 -test lape, 2-test sentencel by RTTY?

Transmit (1-test tape, 2 -test sentence) by RTTY.
QUi Shall I transmit continuous $\{1$-mark. 2-space) RTTY signal?
Transmit continuous (1-mark, 2-space) signal.
OJK Are you receiving continuous 11 -mark, 2-space, 3-mark bias, 4-space bias)?
I am receiving continuous (1-mark, 2space, 3-mark bias, 4-space bias).
QKF May I be relieved at . . . hours? You may expect to be relieved at... hours by. . . .
OLM I will tune for answers from the low end of the band toward the middle.
QMD I will tune for answers from my frequency down.
QMH I will tune for answers from the middle of the band toward the high end.
QML I will tune for answers from the middle of the band toward the low end.
QMU I will tume for answers from my trequency upward.
QMT Will you mail the traffic?
I will accept the traffic for delivery by mail.
QNA* Answer in prearranged order.
QNB* Act as re'ay between. . . and.
ONC All net stations copy.
I have a messoge for all net stations.
OND. Net is directed (controlled by net control station).
QNE Entire not stand by.
QNF Net is tree (not controlled).
ONG Take over as net contral station.
ONH Your net frequency is high.
ONI Net stations report in.'
*For use only by Net Contral Station.

|  | I am reporting iato the net. (Follow with list of traffic ar QRU.) |
| :---: | :---: |
| QNJ | Can you copy me? |
|  | Can you copy . . . ? |
| ONK* | Transmit messages lor . . . to |
| ONL | Your net frequency is low. |
| ONM ${ }^{\text {* }}$ | You are QRMing the net. Stand by, |
| ONN | Net control station is. |
|  | What station has net control? |
| QNO | Station is leaving the net. |
| QNP | Unable to copy you. |
|  | Unable to copy |
| QNO* | OSY to . . . . . . and wait for . . . to finish. |
|  | Then send him traffic for |
| QNR ${ }^{*}$ | Answer . . . and receive tratic. |
| QNS | Follow ing stations are in the net.* (Follow with list.) Request list of stations in the net. |
| QNT | I request permission to leave the net for . . , minutes. |
| QNU* | The net has traffic for you, Stand by. |
| QNV | Establish-contact with... on this freq. If successful OSY to ... and send traffic for .. . |
| ONW | How do I route messages ior . . . ? |
| QNX | You are excused from the net.* |
|  | Aequest to be excused from the net. |
| ONY* | Shift to another frequency tor to . . . kHz to clear traffic with |
| ONZ* | Zero beat your signal with mine. |
| QRA | What is the name of your station? |
|  | The name of my station is. . . . |
| QRB | How far approximately are you from my station? |
|  | The approximate distance between our |
|  | station is,.. nautical miles for kilo. meters). |
| QRO | Where are you bound for and where are you from? |
|  | I am bound for, . . Irom. .. . |
| ORE | What is your estimated time of arrival at . . . (or over . . . ) (place)? |
|  | My estimated time of arrival at . . , tor over . . .) (placel is . . . hours. |
| QRF | Are you returning to . . (place)? |
|  | I am returning to . . . \{place $\}.$ or |
|  | Return to .. . (place). |
| QRG | Will you tell me my exact frequency for that of . . .l? |
| or us | ly by Nei Control Station. |

        I am reporting into the net. (Follow with
        list of traffic ar ORU.)
    copr we?
        Can you copy . . . ?
    ONK* Transmit messages lor . . . to . . . .
    ONL Your net frequency is low
    QNM* You are QRMing the net. Stand by.
        What station has net control?
    QNO Station is leaving the net.
    Unable to copy....
        Then send him traffic for ....
    QNR* Answer . . . and receive tralfic.
    QNS Followng stations are in the net. * (Fol-
        low with list.) Request list of stations in
        the net.
    QNT I request permission to leave the net for
        . . , minutes.
    QNU* The net has traffic for you, Stand by.
QNV Establish-contact with... on this freq.
If successful QSY to ... and send traffic
for . . .
ONW How do I route messages for ... ?
Request to be excused from the net.
(or (o. . . .kHz)
ONZ* Zero beat your signal with mine.
QRA What is the name of your station?
The name of my station is. . . .
station?
The approximate distance between our
station is,., nautical miles for kilo.
meters).
QRD Where are you bound for and where are
you from?
I am bound for . . . Irom. .. .
at . . . (or over . . .) (place)?
My estimated time of arrival at... tor
over . . .) (place) is . . . hours,
Am relurning to ...
or
Return to . . . \{place).
that of . . .l?

- For use onty by Net Control Station.

|  | Please inform... that 1 am talling him on... kHz . |  | I can communicate with . . . direct (or by relay through . . .). |
| :---: | :---: | :---: | :---: |
| QRX | When will you call me again? | QSP | Will you relay to ... free of charge? |
|  | I will call you again at . . . hours (on |  | I will relay to ... free of charge. |
|  | kHz). | QSO | Have you a doctor on board lor is... |
| ORY | What is my ur |  | (name of person) on boardl? |
|  | (Relates to communication) |  | I have a doctor on board lor . . . Inam |
|  | Your turn is Number . . . (or according to any other indication). <br> (Relates to communication) | QSR | of person) is on board). <br> Shail I repeat the call on the calling frequency? |
| QRZ | Who is calling me? <br> You are being called by . . . (on . . kHz ). |  | Repeat your call on the calling frequency; did not hear you (or have interference). |
| OSA | What is the strength of my signals for those of . . . ? | ass | What working frequency will you use? I will use the working frequency . .kHz. |
|  |  | OST | Calling all radio amateurs. |
|  | .) is (1-scarcely perceptible, 2-weak. 3 -fairly good, 4 -good, 5 --very good). | OSU | Shall I send or reply on this Irequency for on... kHz ? |
| QSB | Are my signals fading? <br> Your signals are lading. |  | S.end or reply on this frequency for on ...kHz. |
| OSD | Is my keying defective? Your keying is defective. | asv | Shall I send a series of V 's on this fre. quency for ... kHz )? |
| OSG | Shall 1 send . . . messages at a time? Send . . . messages at a time. |  | Send a series of $V$ 's on this frequency for ... kHz). |
| ash | Are you able to home on your D/F equipment? <br> I am able to home on my D/F equipment | OSW | Will you send on this frequency for on . . . kHzl? <br> I am going to send on this frequency (or on...kHz). |
| QSI | (on station...). <br> I have been unable to break in on your transmission. <br> or | OSX | Will you listen to... (call sign(s)) on ... kHz ? <br> I am listening to... (call sign(s)) on $\ldots \mathrm{kHz}$ |
|  | Will you inform . . . (call sign) that I have been unable to break in on his trans. mission (on... kHz). | OSY | Shall I change to transmission on another trequency? |
| OSK | Can you hear me between your signals and if so can I break in on your trans- |  | Change to transmission on another frequency (or on ... kHz). |
|  | mission? <br> I can hear you between my signals: break | Qsz | Shall I send each word or group more than once? |
|  | in on my transmission. |  | Send each word or group twice for . times). |
| QSL | Con you acknowledge receipt? 1 am acknowledging receipt. | OTA | Shall i cancel message number . . . ? |
| CSM | Shall I repeat the last telegram which : seat you for some previous telegram)? Repeat the last telegram which you sent me (or telegram(s) number(s) . . .). | OTB | Do you agree with my counting of words? <br> I do not agree with your counting of |
| QSN | Did you hear me (or ... (call sign)] on ...kHz? |  | words; I will repeat the first letter or digit of each word or group. |
|  | I did near you [or ... (call sign)] on . . kHz . | OTC | How many messages have you to send? I have . . . messages for you (or for . . .). |
| oso | Can you communicata with . . . direct (or by relayl? | atg | Will you send two dashes of ten second each followed by your call sign tre |

peated,..times) \{on ... kHz )? or Will you request..., to send two dashes of ten seconds followed by his call sign (repeated . . . times) on ... $\mathrm{kHz}_{z}$ ?
I am going to send two dashes of ten seconds each followed by my call sign (repeated... times) ton ...kHz). or I have requested. . . to send two dashes of ten seconds followed by his call sign (repeated . . . times) on . . . kHz .
QTH What is your position in latitude and longitude for according to any other indication)?
My position is . . . latitude . . . longitude for according to any other indication).
OTN At what time did you depart from... (place)?
I departed from ... (place) ar , . . hours.
QTO Have youleft dock lor port)? or Are you airborne?
I have left dock (or port). or I am airborne.
QTP Are you going to enter dock (or port)? or Are you going to alight (or land)?
I am going to enter dock for port). or I arn going to alight (or land).
QTQ Can you communicate with my station by means of the International Code of Signals?
I am going to communicate with your station by means of the International Code of Signals.
QTA What is the correct time?
The correct time is . . . hours.
QTS Will you send your call sign for tuning purposes or so that your frequency can be measured now (or at ... hours) on ... kHz ?
I will send my call sign for tuning purposes of so that my frequency may be measured now (or at... hours) on ... kHz .
QTU What are the hours during which your station is open?
My station is open from . . . to . . . hours.
QTV Shall I stand guard for you on the fre quency of . . kHz (from ... to . . . hours)? Stand guard for me on the frequency of . . . kHz \{from . . . to hours).
QTX Will you keep your station open for further communication with me until further notice (or until... hours)?

I will keep my station open for further communication with you until further notice (or until, . . hours).
OTY Are you proceeding to the position of incident and it so when do you expect to arrive?
I am proceeding to the position of incident and expect to arrive at . . . hours on. . . (date).
OTZ Are you continuing the search?
I am continuing the search for ... (aircraft, ship, survival craft, survivors, or wreckage).
QUA Have you news of . . . (call sign)? Here is news of +. (call sign).
QUB Can you give me in the following order information concerning: the direction in
degrees TRUE and speed of the sarface wind; visibility; present weather; and amount, type, and height of base of cloud above surface elevation at... (place of observation)?
Here is the intormation requested: . .
(The units used for speed and distances should be indicated.?
QUC What is the number for other indication) of the last message you received from me [or from . . . \{call signt]?
The number (or other indication) of the last message 1 received from you for from . . . (call sign)] is . . . .
QUE Can you use telephony in ... (language). with interpreter if necessary; if so, on what frequencies?
I can use telephony in . . . (languagel on .. . kHz ,

QUF Have you received the distress signal sent by .. . (call sign of station)?
I have received the distress signal sent by . . (call sign of station) at . . . hours.
OUH Will you give me the present barometric pressure at sea level?
The present barometric pressure at sea level is . . (units).
OUK Can you tell me the condition of the sea observed at . . . (place or coordinates)?
The sea at ... (place or coordinates) is....
QUM May I resume normal working? Normal working may be resumed,

## RADIO TEIEPHONE CODE

## General Station Operation

10－1 Receiving poorly．
10－2 Signals good．
t0－3 Stop transmitting．
10－4 Okay－Affirmative－Acknowledged．
10－5 Relay this message．
10－6 Busy，stand by．
10－7 Leaving the air．
10－B Back on the air and standing by．
10－9 Repeat message．
10－10 Transmission completed，standing by．
10－11 Spask slower．
10－13 Advise weather and road conditlons．
10－18 Complate assignment as quickly as possible．
10－19 Return to base．
10－20 What is your location？My location is ．．．．
10－21 Call ．．．by telephone．
10－22 Report in person to
10－23 Stand by．
10－24 Have you finished？I have finished，
10－25 Do you have contact with ．．．？
Emergency or Unusual
10－30 Does not conform to Rules and Regulations．
10－33 Emergency traffic this station．
10－35 Confidential information．
10－36 Correct time．
10－4．1 Tune to channel ．．．for test، operation，or emergency service．
10－42 Out of service at home．
10－45 Call．．．by phone．
10－54 Accident．
10－55 Wrecker or tow truck needed．
10－56 Ambulance needed．
Net Message Handling
10－60 What is next message number？
10－62 Unable to copy，use CW．
10－63 Net clear．
10－64 Net is clear．
10－66 Cancellaton．
10－68 Repeat dispatch on message．
10－69 Have you dispatched message ．．．？
10－70 Net message．
10－71 Proceed with transmisslon in sequence．

## Personal

10－82 Reserve room for
10－84 What is your telephone number？
10－88 Advise present phone number of

## Technical

10－89 Repairman needed．
10－90 Repairman will arrive at your station
10－92 Poor signal，have transmitter checked．
10－93 Frequency check．
10－94 Give a test without voice for frequency check．
10－95 Test with no modulation．
10－99 Unable to receive your signals．

INTERNATIONAL MORSE CODE
Alphatetical

| A－－ | J•－－－ | S ．． |
| :---: | :---: | :---: |
| B $-\cdots$ | K－$\cdot$－ | T－ |
| C－． | L．${ }^{\text {，}}$ ， | U．．－ |
| D ——＇ | M－－ | V．．． |
| E． | N－． | W $\cdot$－－ |
| F．．．． | O－－－ | X－－－ |
| G－－ | P－－－ | Y－－－ |
| H ．．． | Q－－－ | Z－－$\cdot$ |
| 1． | R－－ |  |

By Groups

| Group One | Group Two | Group Three |
| :---: | :---: | :---: |
| E． | A－－ | R •－＊ |
| 1．＇ | W＝－－ | F．$\cdot$－ |
| S．．． | J・ーーー | L＇－＇ |
| H．．．． | N－． | U．・ー |
| T－ | ロー・• | V ．．．－ |
| M－－ | 日 |  |
| O－－－ |  |  |
| Group Four |  |  |
| K－－－ | Q－－－ |  |
| X－$\cdot$－ | G－－ |  |
| C－ | Z－－． |  |
| Y－－－ | P $\cdot$－－ |  |

Numerals and Punctuation
1・ーーーー 6 －．．．．
2・ーー一 7 ーー・••
$3 \cdots$－ 8 －
4••・ー $\quad$－
5．．．．＇ 0 —————
Period •－：－．－
Comma－－．－－
Question mark $\cdot$ ．———．
Error
Double dash－．．．．．
Fraction bar —．．－•
Wait •－．．
Invitation to transmit－．－
End of message（AR）•－•－
End of transmission • ．．－•－

## Special Foreign Letters

A（German）•－－
A or A（Spanish－Scandinavian）•－－－
CH （German－Spanish）－－－－
É（French）．．－．．
$\widetilde{N}$（Spanish）－－$\cdot$－
O（German）－－－．
Ü（German）••－

## RST Code

The standard amateur method of giving signal strength reports. For phone operation only the first two sets of numbers are used with the words "readability" and "strength."

## Readabllity ( R )

1. Unreadable
2. Barely readable, occasional words distinguishable
3. Readable with considerable difficulty
4. Readable with practically no difficulty
5. Perfectly readable

## Signal Strength (S)

1. Faint; signal barely perceptible
2. Very weak signal
3. Weak signal
4. Fair signal
5. Fairly good signal
6. Good signal
7. Moderately strong signal
8. Strong signal
9. Extremely strong signal

## Tone ( T )

1. Extremely rough, hissing signal
2. Very rough ac signal
3. Rough, low-pitched ac signal
4. Rather rough ac signal
5. Musically modulated signal
6. Modulated signal, slight whistle
7. Near dc signal, smooth ripple
8. Good dc signal, trace of ripple
9. Purest dc signal

If the signal has the steadiness of crystal control, add "X" after the RST report; add " C " for a chirp; and " K " for a keying click.

A typical report might be: "RST579X," meaning "Your signals are perfectly readable, moderately strong, have a perfectly clear tone, and have the stability of a crystal-controlled transmitter."

This reporting system is used on both CW and voice, leaving out the "Tone" report on voice.

## SINPO Code

A reporting method used in the shortwave field. All the numbers after the letters range from one to five. Q-code equivalents for each characteristic are also shown.

FOR EXAMPLE: A typical report for a station that is coming in loud and clear would read: SINPO 55555.

| $S$ <br> Signal Strength (QSA) | interference (QRM) | N <br> Atmospheric Noise (QRN) | $P$ <br> Propagatbon Disturbance (QSE) | 0 Overall Menit (QRK) |
| :---: | :---: | :---: | :---: | :---: |
| 5 Excellent | 5 None | 5 None | 5 None | 5 Excellent |
| 4 Good | 4 Stight | 4 Slight | 4 Slight | 4 Good |
| 3 Fair | 3 Moderate | 3 Moderate | 3 Moderate | 3 Fair |
| 2 Poor | 2 Severe | 2 Severe | 2 Severe | 2 Poor |
| 1 Barely audible | 1 Extreme | 1 Extreme | 1 Extreme | 1 Unusable |

## 555 Code

Another reporting code sometimes used in the shortwave field.

|  | Signal Strength | Interference | Overall Merit |
| :--- | :--- | :--- | :--- |
|  | 0 Inaudible | 0 Total | 0 Unusable |
|  | 1 Poor | 1 Very severe | 1 Poor |
| 2 Fair | 2 Severe | 2 Fair |  |
| 3 Good | 3 Moderate | 3 Good |  |
| 4 Very good | 4 Slight | 4 Very good |  |
|  | 5 Excellent | 5 None | 5 Excellent |

## SINPFEMO Code

This eight-figure signal reporting method rates eight characteristics of a signal. (If a characteristic is not rated, the letter " $x$ " is used instead of a numeral.)

| Hating Scale | S | 1 | N | $\rho$ | $F$ | $E$ | $M$ | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Signal Strength | Degrading Effect of |  |  | Frequency of Fading | Modulation |  | Overall Rating |
|  |  | Interference (QRM) | $\begin{aligned} & \text { Noise } \\ & \text { (QRN) } \end{aligned}$ | Propagation Disturbance |  | Quality | Depth |  |
| 5 | Excellent | Nil | Nil | Nil | Nil | Excellent | Maximum | Excellent |
| 4 | Good | Slight | Slight | Slight | Slow | Good | Good | Good |
| 3 | Fair | Moderate | Moderate | Moderate | Moderate | Falr | Fair | Fair |
| 2 | Poor | Severe | Severe | Severe | Fast | Poor | Poor or nil | Poor |
| 1 | Barely audible | Extreme | Extreme | Extreme | Very last | Very poor | Continuously overmodulated | Unusable |

## Amateur Operator Licenses

| Class | Prior Experience | Code Test | Written Examination | Privileges | Term |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Novice | None | 5 w.p.m. | Elemenlary theory and regulations | Al Telegraphy in 3.73.75, 7.1-7.15, 21.121.2, 28.1-28.2 MHz. 250 watts maximum input. | 5 years, renewable |
| Technlelan | None | 5 w.p.m. (Credit given 10 Novice Class Licensees) | General theory and regulations | All amateur privileges above 50 MHz . Also novice privileges. | 5 years, renewable |
| General | None | 13 w.p.m. | General theory and regulations (Credil givan to Technician Class Licensees) | $1.6 \cdot 2{ }^{4}{ }^{4} 3.525-3.775$. <br> 3.89-4, 7.025-7.15, <br> 7.225-7.3. 14.025. <br> 14.2, 14.275-14.35, <br> 21.025-21.25, 21.35- <br> 21.45, 28.0.29.7 <br> MHz , and all amateur <br> privileges above <br> 50 MHz . | 5 years, renewable |
| Advanced | None | 13 w.p.m. (Credit is given to General Class Licensees) | Intermediate theory and regulations | $\begin{aligned} & 1.8-2,{ }^{a} 3.525 \cdot 3.775 \\ & 3.8-4,7.025 \cdot 7.3 \\ & 14.025-14.45,21.025- \end{aligned}$ <br> 21.25, and all amateur frequencies abova 21.27 MHz . | 5 years, renewable |
| Amateur Extra | None | 20 w.p.m. | Advanced theory and regulations | All amateur privileges | 5 years, renewable |
| ${ }^{\text {a }}$ The 1,8-2 band frequency and power assignments differ from state to stale. Check with nearest FCC office. |  |  |  |  |  |

Commercial Radio Operator Licenses

| Type of License | Age Minimum | Code Requirement | Written Test | Term <br> of License |
| :---: | :---: | :---: | :---: | :---: |
| Restricted Radiotelephone Permil | 14 years | None | None; obtained by declaration (FCC Form 753) | Lffetime |
| Marine Radio Operator Permit | None | None | Elements 1, 2 | 5 years, renewable |
| General Radiotelephone License | None | None | Element 3 | 5 years, renewable |
| Thind Class Radiotelegraph Permit | None | 16 code groups 20 plain words per minute | Elements 1, 2, 5 | 5 years renewable |
| Second Class Radiotelegraph License | None | 16 code groups 20 plain words per minute | $\begin{array}{r} \text { Elements 1, } 2, \\ 5,6 \end{array}$ | 5 years, renewable |
| First Class Radiotelegraph License | 21 years; one year experience | 20 code groups, 25 plain words per minute | Elements 1, 2, 5, 6 | 5 years, renewable |

## Commercial Examination Elements

NO. 1, BASIC LAW-
Provisions of laws, treaties and regulations with which every marine operator should be familiar. (20 Questions, multiple choice type)
NO. 2, BASIC OPERATING PRACTICE-
Operating procedures and practices generally followed or required in communicating by marine radio-telephone stations. (20 Questions, multiple choice type)
NO. 3, BASIC RADIOTELEPHONE-
Technical, legal and other matters including basic operating practices and provisions of laws, treaties and regulations applicable to operating radiotelephone stations other than broadcast. ( 100 Questions, multiple choice type)
NO, 5, RADIOTELEGRAPH OPERATING PRACTICE-
Radio operating procedures and practices generally followed or required in communicating by radiotelegraph stations primarily other than in the maritime mobile services of public correspondence. ( 50 Questions, multiple choice type)
NO. 6, ADVANCED RADIOTELEGRAPH-
Technical, legal matters applicable to operaling all classes of radiotelegraph stations including maritime mobile services of public correspondence, message lraffic routing and accounting, radio navigational aids, etc. (100 Questions)
NO. 7, AIRCRAFT RADIOTELEGRAPH-
Special endorsement on Radiotelegraph First and Second Class Operator Licenses. Theory and practica in operation of radio communication and navigational systems in use on aircraft. (100 Ouestions, multiple choice type; code test of 20 code groups per minute and 25 WPM plain language.)
NO. 8, SHIP RADAR TECHNIQUES-
Special endorsement on Radiotelegraph or Radiotelephone First or Second Class Operator Licenses. Specialized theory and practice applicable to proper installation, servicing and maintenance of ship radar equipment in use for marine navigational purposes. ( 50 Questions, multiple choice type)

INTERNATIONAL PHONETIC ALPHABET
To avoid errors or misunderstanding during voice communication, the new international phonetic alphabet has been adopted.

| Letter | Name | Pronunciation | Letter | Name | Pronunciation |
| :---: | :---: | :---: | :---: | :---: | :---: |
| A | Affa | AL-fah | N | November | No-VEM-ber |
| B | Bravo | BRAH-voh | 0 | Oscar | OSS-cah |
| C | Charlie | CHAR-lee <br> (or SHAR-lee) | P | Papa Quebec | Pah-PAH <br> Keh-BECK |
| D | Delta | DELL-tah | 8 | Romeo | ROW-me-oh |
| E | Echo | ECK-oh | S | Sierra | See-AIR-rah |
| F | Foxtrot | FOKS-trot | T | Tango | TANG-go |
| G | Golf | GOLF | U | Uniform | YOU-nee-form |
| H | Hotel | HOH -tel |  |  | (or OO-nee-form) |
| 1 | india | IN-dee-ah | V | Victor | VIK-tah |
| J | Juliett | JEW-lee-ett | W | Whiskey | WISS-key |
| K | Kilo | KEY-loh | $X$ | $X$-ray | ECKS-ray |
| L | Lima | LEE-mah | Y | Yankee | YANG-key |
| M | Mike | MIKE | Z | Zulu | ZOO-100 |

## ARRL (AMERICAN RADIO RELAY LEAGUE) WORD UST FOR VOICE COMMUNICATION

| A-Adam | N-Nancy |
| :--- | :--- |
| B-Baker | O-Otto |
| C-Charlie | P-Peter |
| D-David | Q-Queen |
| E-Edward | R-Gobert |
| F-Frank | S-Susan |
| G-George | T-Thomas |
| H-Henry | U-Union |
| I-Ida | V-Victor |
| J-John | W-William |
| K-King | X-X-Ray |
| L-Lewis | Y-Young |
| M-Mary | Z-Zebra |

Example: W1AW . . . W1
ADAM WILIAM . . . W1AW

## TRANSMISSION TRAVEL TIME

The time required for electromagnetic energy to travel interplanetary distances is significant. Shown here are some typical times and distances related to the earth's position.

| Moon | $=23.9 \times 10^{4} \mathrm{n} \mathrm{mi}$ |
| :--- | :--- |
| Venus | (overhead) <br> (nearest) <br> (farthest) |
| $=139.4 \times 10^{6} \mathrm{n} \mathrm{mi}$ |  |
| Mars | $=10^{6} \mathrm{nmi}$ |
| (nearest) | $=42.4 \times 10^{6} \mathrm{n} \mathrm{mi}$ |
| (farthest) | $=203.9 \times 10^{6} \mathrm{n} \mathrm{ml}$ |
| Jupiter |  |
| (nearest) | $=339.8 \times 10^{6} \mathrm{n} \mathrm{mi}$ |
| (farthest) | $=501.2 \times 10^{6} \mathrm{n} \mathrm{mi}$ |

1.27 sec one way
139.00 sec one way
859.00 sec one way
262.00 sec one way
1259.00 sec one way
2099.00 sec one way
3096.00 sec one way

In accordance with Federal Communications Commission Rules and Regulations 2.201, Subpart C, the following systern of designating emission, modulation, and transmission characteristics is employed.


| Class | Name | Code | Action of Modu- <br> lating Signal |
| :---: | :---: | :---: | :---: |
| A | Pulse-time modulation | PTM | Varies some characteristic of pulse with respect to time. |
|  | Pulseposition modulation | PPM | Vagies position (phase) of pulse on time base. |
|  | Pulseduration modulation | PDM | Varies width of pulse (also called PWM, or PulseWidth Modulation). |
|  | Pulse-shape modulation |  | Varies shape of pulse. |
|  | Pulsefrequency modulation | PFM | Varies pulse recur. rence frequency. |
| B | Pulseamplitude modulation | PAM | Varies amplitude of pulse-consists of two types: one ubing unipolar pulses. the other using bipolar pulses. |
| C | Pulse-code modulation | PCM | Varies the makeup of a series of pulses and spaces, Individual systems are chastified as follaws: Binary-pulse and spaces, or positive and negative pulses. Ternary-positive pulses, negative pulses, and spaces. N-ary-more complex combinations of pulset and apaces. |

## MICROPHONE OUTPUT NOMOGRAM

This nomogram determines the output voltages for various microphone ratings and relates this output to actual sound pressure levels.

Two methods of specifying microphone levels are in general use. Acoustic input and electrical output are specified so that the microphone can be considered as a generator, with sound pressure input and voltage or power output.

For low-impedance microphones, output is given in decibels referenced to 1 mW for 10 dynes $/ \mathrm{cm}^{2}$ sound pressure. For high-impedance microphones, output is given in decibels referenced to 1 V for $1 \mathrm{dyne} / \mathrm{cm}^{2}$ sound pressure. (In both, output is into a resistive load equal to the impedance of the microphone.)

This nomogram is prepared for microphone preamplifiers with low input impedances matched to the microphone impedance. (Open-circuit voltage is 6 dB higher than the nomogram value.) Connecting the mj crophone impedance and the decibel rating solves for the voltage across a matched load for the standard 10 dynes $/ \mathrm{cm}^{2}$ sound pressure field. By referring to the absolute sound pressure vs decibel scale, any other sound pressure level can be found and the decibel difference (with respect to $10 \mathrm{dynes} / \mathrm{cm}^{2}$ ) can be determined, and adjustments can be made in the output voltage by adding or subtracting decibels.

For high-impedance microphones, the nomogram is used in the same way, except that the impedance is always considered as $40,000 \mathrm{ohms}$, and the reading will be that for a 10 dynes $/ \mathrm{cm}^{2}$ field. These microphones are usually operated into a very high impedance circuit, hence 6 dB must be added to the output voltage. (Use of this method results in an error of approximately 2 dB .)


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## ATTENUATOR NOMOGRAMS

These two nomograms solve for the resistor values required for the following: $\mathrm{T}, \mathrm{Pi}, \mathrm{H}, \mathrm{O}$, lattice, bridged T , bridged $\mathrm{H}, \mathrm{L}$, and U-type attenuators. The nomograms are based on the equations shown. The keys next to the nomograms show which scales must be used for a particular type of attenuator.

FOR EXAMPLE:

1. $Z_{o}$ is 600 ohms and the required attenuation is 20 dB . Design $\mathrm{T}, \mathrm{H}$, and Pi attenuators. From nomogram 1 , for a T type, $R_{1}$ is 480 ohms and $R_{4}$ is 120 ohms. For an $H$ type each of the four series amns would be 240 ohms. For Pi type (middle key) $R_{2}$ is 750 ohms and $R_{3}$ is 3,000 ohms.
2. A lattice attenuator (key three, nomogram 1) that gives 20 dB of attenuation at 500 ohms requires $R_{1}$ to be 410 ohms and $R_{2}$ to be 610 ohms.
3. A bridged T attenuator (nomogram 2, first key) with an attenuation of 20 dB and terminal impedances of 450 ohms has $R_{5}$ as 4,000 ohms and $R_{6}$ as 50 ohms.
4. Design an L-type attenuator (middle key, nomogram) with an attenuation of 14 dB , and an impedance of 50 ohms with the shunt arm at the output end. In this case $R_{5}$ is 200 ohms and $R_{8}$ is 62.5 ohms.

NOTE: In all cases the input and output impedances are the same.

$$
\begin{array}{llll}
R_{1}=Z_{0}\left(\frac{K-1}{K+1}\right) & R_{3}=Z_{0}\left(\frac{K^{2}-1}{2 K}\right) & R_{5}=Z_{0}(K-1) & R_{7}=Z_{0}\left(\frac{K-1}{K}\right) \\
R_{2}=Z_{0}\left(\frac{K+1}{K-1}\right) & R_{4}=Z_{0}\left(\frac{2 K}{K^{2}-1}\right) & R_{6}=Z_{0}\left(\frac{1}{K-1}\right) & R_{5}=Z_{0}\left(\frac{K}{K-1}\right)
\end{array} \text { where } K=\frac{E_{\text {in }}}{E_{\text {out }}}
$$

NOMOGRAM 1 FOR T, Pi, H, O, AND LATTICE TYPE ATTENUATORS.


NOMOGRAM 2 FOR BRIDGED T, H, L, AND U TYPE ATTENUATORS.

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## TWIN-T FILTER NOMOGRAM

Twin-T filters with symmetrical response curves are frequently used to reject specific frequencies, or they may be included in the negative feedback loop of a frequency-selective amplifler as the tuning element. Other component combinations may be used, but the one selected here has the greatest possible selectivity. With this general configuration, any filter exhibits infinite attenuation at the notch frequency ( $f_{o}$ ) which is specified by the values of $R_{1}$ and $C_{4}$. If it is only desired to reject $f_{0}$, then the choice of these values is atbitrary. However, if it is desired to design a filter with a symmetrical response curve so the dc gain is equal to that at high frequencies, that is aocomplished when $R_{1}=\sqrt{R_{8} R_{i} / 2}$, and the notch frequency is determined by the expression $f_{0}=1 / 4 \pi C_{1} R_{1}$. The nomograms are based on these two equations. Usually $R_{g^{\prime}}, R_{L^{\prime}}$, and $f_{o}$ are known, and the values of $R_{1}$ and $C_{1}$ are to be determined. It is also possible to use chart 2 alone and select arbitrary values for $A_{1}$ or $C_{1}$ if symmetrical response is not essential.

FOR EXAMPLE: Design a filter with infinite attenuation at 800 Hz which is to be inserted between a 2,000 -ohm source impedance and a load resistance of 100,000 ohms. From nomogram 1 determine that $R_{1}$ should be 10,000 ohms, and with that value determine from nomogram 2 that $C_{1}$ must be $0.01 \mu \mathrm{~F}$ to achieve a symmetrical response curve.

Twin-T notch filter, with component values related as shown, yields maximum selectivity and symmetrical gain-frequency response.

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## MINIMUM-LOSS MATCHING PADS

This nomogram solves for the resistance values needed for an impedance matching pad having a minimum of atlenuation. $Z_{1}$ is the greater and $Z_{2}$ is the lesserterminal impedance in ohms. To use the nomogram, calculate the ratio of $Z_{2} / Z_{1}$ and connect that point on the center scale with $Z_{1}$ to find $R_{1}$, and with $Z_{2}$ to find $R_{3} 890$ ohms also read on the center scale.

FOR EXAMPLE: If $Z_{2}$ is 400 ohms and $Z_{1}$ is 500 ohms, the value of $R_{1}$ must be 225 ohms and of $R_{3} 890$ ohms for a minimum insertion loss pad that has 4.2 dB of insertion loss.

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## PREFERRED VALUES Of COMPONENTS

Preferred numbers for nominal values of resistance, capacitance, and inductance have been adopted by the electronics industry. Each value differs from its predecessor by step multiples of (10) $1 / 16,(10) 1 / 12$, or (10) $1 / 24$ resulting in incremental increase of approximately $40 \%, 20 \%$, and $10 \%$ per step as shown in the table, to yield an orderly progression of component values of $\pm 20 \%, \pm 10 \%$, and $\pm 5 \%$.

Standard values outside of the range listed can be obtained by multiplying by suitable multiples of 10 . (For example, 15 can represent $1.5,150,15 \mathrm{k}, 1.5 \mathrm{M}$, etc.)

MIL and EIA Standard for Component Values and Tolerances

| $\pm 20 \%$ | $\pm 10 \%$ | $\pm \mathbf{5 \%}$ |
| :---: | :---: | :---: |
| 10 | 10 | 10 |
|  | 12 | 11 |
|  |  | 12 |
| 15 | 15 | 13 |
|  |  | 15 |
|  | 18 | 16 |
|  |  | 18 |
| 22 | 22 | 20 |
|  |  | 22 |
|  | 27 | 24 |
|  | 33 | 27 |
| 33 |  | 30 |
|  |  | 33 |
|  |  | 36 |
|  |  | 39 |
| 47 |  | 43 |
|  |  | 47 |
|  |  | 51 |
|  |  | 56 |
| 68 |  | 62 |
|  |  | 68 |
|  |  | 75 |
|  |  | 32 |
| 100 |  | 91 |
|  |  | 100 |

## THERMAL NOISE VOLTAGE NOMOGRAM (A)

Given frequency, input $C$, and amplifier input $Z$, only two operations are required to find the equivalent thermal noise vollage.

When an amplifier is fed from a capacitive source, the spot (one frequency) noise is generated by the real part of the impedance. This nomogram reduces the calculation required to arrive at the noise value. Impedance al the amplifier input is

$$
\begin{equation*}
z=\frac{R-j R^{2} \omega C}{R^{2} \omega^{2} C^{2}+1} \tag{1}
\end{equation*}
$$

Thermal noise is generated by the real part of this expression, which is

$$
\begin{equation*}
(\text { REAL } Z)=\frac{R}{R^{2} \omega^{2} C^{2}+1}=\frac{1}{R \omega^{2} C^{2}} \tag{2}
\end{equation*}
$$

The mean square thermal noise vollage associated with the real part of $Z$ is given by

$$
\begin{equation*}
\overline{\mathrm{e}}^{2}=4 k T \text { of }(R E A L Z) \tag{3}
\end{equation*}
$$

For this case

$$
\begin{gathered}
d f=1 \text { (spot frequency) } \\
\quad T=25^{\circ} \mathrm{C}
\end{gathered}
$$

Combining (2) and (3)

$$
\begin{equation*}
E^{2}=4 k T d f \frac{1}{R \omega^{2} C^{2}} \tag{4}
\end{equation*}
$$

Equation (4) forms the basis for the nomogram. Nomogram of equivalent spot thermal noise voltage of the parallei combination of a capacitor and an amplifier input resistance.
Using the nomogram:

1. Choose $f, C$, and $R$ (in the example $f=10 \mathrm{kHz}, C=0.001 \mu F_{\text {, }}$ and $R=1 \mathrm{M}$ ohm).
2. Draw a line between the chosen $f$ and $C$.
3. Mark its intersection on the reference line.
4. Draw a line from the marked point on the reference scale to the chosen $R$.
5. The intersection of this line with the $\overline{\mathrm{e}}^{2}$ scale is the desired equivalent thermal noise voltage in dB re 1 V .



Thermally produced noise voitage of any linear conductor is determined by Nyquist's equation

$$
E=2 \sqrt{R k T B}
$$

where $E=$ noise voltage in rms microvolts $\quad T=$ absolute temperature $\left({ }^{\circ} \mathrm{K}\right)$
$k=$ Boltzmann's constant, $1.38 \times 10^{-23} \mathrm{j} /{ }^{\circ} \mathrm{K} \quad B=$ bandwidth in hertz
$R=$ resistance
This nomogram solves the above equation if any three of the four variables are given.
FOR EXAMPLE: An amplifier has a voltage gain of 1,000, and input resistance of 470,000 ohms, and a bandwidth of 2 kHz . Find the output noise level due to the input resistance if the amplifier is operated at an ambient temperature of $100^{\circ} \mathrm{C}$.

Connect $100^{\circ} \mathrm{C}$ ( $T$ scale) with 470 K ( $R$ scale) and note intersect point on turning scale. Connect that point with 2 kHz ( $B$ scale) and read noise voltage as $4.4 \mu \mathrm{~V}$ on $E$ scale. The amplifier has a gain of 1,000 ; thus, the outside nolse of the amplifier due to the input resistance is 4.4 mV .


This nomogram is based on the formula for the inductance of a single-layer coil

$$
L=\frac{a^{2} N^{2}}{9 a+10 b}
$$

where $L=$ inductance in microhenries
$a=$ coil radius in inches
$b=$ coil length in inches
$N=$ number of turns

2-2 - -


FOR EXAMPLE: (1). Find the inductance of a 100 -turn coil with a diameter of $\mathbf{2} \mathbf{i n}$. and a winding length of 0.8 in. Find K (diameter/length) $2 / 0.8$ to be 2.5. Connecting 2.5 on the K scale to 100 on the N scale intersects the turning axis at 3.8. Now connect 3.8 with 2 on the D scale, and read the inductance as $600 \mu \mathrm{H}$. (2) Determine the number of tums required for a $290-\mu \mathrm{H}$ coil 3 in . Iong with a diameter of 2.5 in . K is equal to 0.8 . Connect 290 on the $L$ scale with 2.5 on the 0 scale, and read 4.6 on the turning axis. Connecting 4.6 and 0.8 on the K scale gives the answer as 90 turns on the N scale.


This nomogram solves for the number of close-wound tums required to achieve inductances in the range of values required for television, fm, and radar if transformers. The nomogram is based on a slight modification of H.A. Wheeler's inductance formula that was used to construct nomogram $A$. The formula used here (with all dimensions in inches) is

$$
L=\frac{a^{2} N^{2}}{8.85 a+10 b}
$$

FOR EXAMPLE: Ten turns of number 30 AWG enameled wire closewound on a 0.25 -inch diameler coil form will produce an inductance of $0.7 \mu \mathrm{H}$.

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INDUCTANCE OF STRAIEHT, ROUMO WRE AT HAEH FREQUENCIES
Above several megahertz the inductance of relatively short lengths of wire becomes important because of the effect on circuit performance. The chart shows the relationship between diameter, wire length, and inductance for various diameters. A more precise tabulation is also shown for short lengths of commonly used wire sizes.

FOR EXAMPLE: A straight piece of wire 4 in . long with a diameter of 25 mil has an inductance of $0.2 \mu \mathrm{H}$. At a frequency of 80 MHz , this represents an inductive reactance of about 100 ohms .

| AWG <br> Wire Size | Length <br> (in.) | Approx. <br> inductance <br> $(\mu H)$ |
| :---: | :---: | :---: |
| 20 | $1 / 4$ | 0.0031 |
|  | $1 / 2$ | 0.0064 |
|  | $1 / 4$ | 0.0115 |
|  | 1 | 0.019 |
|  | $11 / 2$ | 0.031 |
|  | 2 | 0.04 |
| 24 | $1 / 4$ | 0.0037 |
|  | $1 / 2$ | 0.0082 |
|  | $3 / 4$ | 0.014 |
|  | 1 | 0.022 |
|  | $11 / 2$ | 0.036 |
|  | 2 | 0.05 |


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## TRANSFORMER IMPEDANCE NOMOGRAM

Tapped transformers provide standard impedances between the various taps and the common terminal. If a nonstandard impedance is required, it can often be found between the taps. This nomogram determines the impedance between terminals $B$ and $C$ if the impedance from $A$ to $B$ and $A$ to $C$ are known, and it is based on the following formula

$$
z_{(\theta-C)}=\left(\sqrt{Z_{(A-C)}}-\sqrt{Z_{(A-B)}}\right)^{2 \cdot}
$$

FOR EXAMPLE: If the impedance from $A$ to $B$ is 15 ohms, and the impedance from $A$ to $C$ is 250 ohms, then the impedance from $B$ to $C$ is $\approx 145$ ohms.

$$
\text { -Derived from } Z_{(B-C)}=Z_{A-B}\left(\sqrt{\frac{Z_{(A-C)}}{Z_{(A-B)}}}-1\right)^{2}
$$



|  |  | $\left.\begin{array}{r} 0 \\ 1 \\ 3 \\ 7 \\ 10-1 \\ 15 \\ 20 \\ 25 \\ 30 \\ \hline 40 \\ 40 \\ 50 \\ 60 \\ \hline 10 \\ 70 \\ 80 \\ 90 \\ \hline 100 \\ 100 \end{array}\right]$ |
| :---: | :---: | :---: |

## ENERGY STORAGE NOMOGRAM

The nomogram relates capacitance, charging voltage, and stored energy in a capacitor in accordance with the formula

$$
J \text { or } W=\frac{C V^{2}}{2}
$$

where $J$ or $W=$ energy in joules or watt-seconds
$C=$ capacitance in microfarad
$V=$ charging voltage
FOR EXAMPLE: The energy stored in a $525-\mu \mathrm{F}$ capacitor charged to 450 V is 53 W -sec or joules.


POWER-FACTOR CORRECTION
Power factor is the ratio (usuaily given in percent) of the actual power used in a circuit to the power apparently drawn from the line.

$$
P F=\frac{\text { actual power }}{\text { apparent power }}
$$

A low power factor is undesirable, and it can be raised by the addition of power-factor correction capacitors which are rated in kVAR (kilovoll-ampere reactive). To determine the kVAR of the capacitors needed to correct from an existing to a higher power factor, multiply the proper value in the table by the average power consumption on kllowatts, of the load.

FOR EXAMPLE: Find the kVAR of capacitors that is required to raise the power tactor of a $500-\mathrm{kW}$ load from $70 \%$ to $85 \%$.

From the table select the multiplying factor 0.400 which corresponds to the existing $70 \%$ and required $85 \%$ power factor. Multiplying 0.400 by 500 shows that 200 kVAR of capacitors are required.

| Existing Power Factor \% | Corrected Power Factor |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 100\% | 95\% | 90\% | 85\% | 60\% | 75\% |
| 50 | 1.732 | 1.403 | 1.247 | 1.112 | 0.982 | 0.850 |
| 52 | 1.643 | 1.314 | 1.158 | 1.023 | 0.893 | 0.761 |
| 54 | 1.558 | 1.229 | 1.073 | 0.938 | 0.808 | 0.676 |
| 55 | 1.518 | 1.189 | 1.033 | 0.898 | 0.768 | 0.636 |
| 56 | 1.479 | 1,150 | 0.994 | 0.859 | 0.729 | 0.597 |
| 58 | 1.404 | 1.075 | 0.919 | 0.784 | 0.654 | 0.522 |
| 60 | 1.333 | 1.004 | 0.848 | 0.713 | 0.583 | 0.451 |
| 62 | 1.265 | 0.936 | 0.780 | 0.645 | 0.515 | 0.383 |
| 64 | 1.201 | 0.872 | 0.716 | 0.581 | 0.451 | 0.319 |
| 65 | 1.168 | 0.839 | 0.683 | 0.548 | 0.418 | 0.286 |
| 66 | 1.139 | 0.810 | 0.654 | 0.519 | 0.389 | 0.257 |
| 68 | 1.078 | 0.749 | 0.593 | 0.450 | 0.328 | 0.196 |
| 70 | 1.020 | 0.691 | 0.535 | 0.400 | 0.270 | 0.138 |
| 72 | 0.964 | 0.635 | 0.479 | 0.344 | 0.214 | 0.082 |
| 74 | 0.909 | 0.580 | 0.424 | 0.289 | 0.159 | 0.027 |
| 75 | 0.882 | 0.553 | 0.397 | 0.262 | 0.132 |  |
| 76 | 0.855 | 0.526 | 0.370 | 0.235 | 0.105 |  |
| 78 | 0.802 | 0.473 | 0.317 | 0.182 | 0.052 |  |
| 80 | 0.750 | 0.421 | 0.285 | 0.130 |  |  |
| 82 | 0.698 | 0.369 | 0.213 | 0.078 |  |  |
| 84 | 0.646 | 0.317 | 0.161 |  |  |  |
| 85 | 0.620 | 0.291 | 0.135 |  |  |  |
| 86 | 0.594 | 0.265 | 0.109 |  |  |  |
| 88 | 0.540 | 0.211 | 0.055 |  |  |  |
| 90 | 0.485 | 0.156 |  |  |  |  |
| 92 | 0,426 | 0.097 |  |  |  |  |
| 94 | 0.363 | 0.034 |  |  |  |  |
| 95 | 0.329 |  |  |  |  |  |

The power factor $(\cos \phi)$ of a series RL or a parallel RC network is given by the following formulas

$$
\begin{aligned}
& \text { P.F. (inductive) }=\frac{R_{2}}{\sqrt{R_{s}^{2}+(\omega L)^{2,}}} \\
& \text { P.F. (capacitive) }=\frac{1}{\sqrt{\left(R_{p} \omega C\right)^{2}+1}}
\end{aligned}
$$

To use the nomogram connect frequency with the desired value of $L$ or $C$ and note the intersect point on the turning scale. Using this intersect point, connect to the resistance, and by extending this line, read power factor and phase angle.

FOR EXAMPLE:

1. A $1-\mathrm{H}$ Inductance in series with 100 ohms is connected to a $60-\mathrm{Hz}$ source. in this case $\phi$ is $75^{\circ}$ and $\cos \phi$ $=0.26$.
2. An inverter operating at 2 kHz is used to supply a 100 -ohm load which is in parailel with a capacitance of $0.047 \mu \mathrm{~F}$. In this case $\phi$ is $3.5^{\circ}$ and $\cos \phi=0.998$.


## kVAR-CAPACITY NOMOGRAM FOR 6O-Hz SYSTEMS

This nomogram is based on the formula

$$
k V A R=\frac{2 \pi f C E^{2}}{10^{9}}
$$

where $C$ is in microfarad $E$ in volts, and $f$ is 60 Hz .
FOR EXAMPLE: To provide 5 kVAR at 460 V requires $62 \mu \mathrm{~F}$.


The curves show the approximate sell-resonanil frequency of capacitors with various lead lengths. They apply to parallel lead wires of equal length \#20 to $\# 24$ AWG, spaced no further than 0.375 in . apar.

FOR EXAMPLE: A $1,000-\mathrm{pF}$ capacitor with 2 -in. leads resonates at about 18 MHz . The same capacitor with $0.2-\mathrm{in}$. leads will resonate at 60 MHz .


## REACTANCE NOMOGRAMS

The set of three nomograms on the following pages covers the frequency range of 1 Hz to $1,000 \mathrm{MHz}$ in three ranges which give direct answers without the need for additional calculations to locate the decimal point. These nomograms may be used to find capacitive reactance, inductive reactance, as well as resonant frequency ( $X_{L}=$ $X_{c}$ ) of any combination of inductance and capacitance.

FOR EXAMPLE:

1. The reactance of a $10 \cdot \mathrm{mH}$ inductor at $10-\mathrm{kHz}$ is 630 ohms.
2. The reactance of a $3-\mathrm{pF}$ capacitor at 5 MHz is 10,500 ohms.
3. A $5-\mu \mathrm{F}$ capacitor and a $1.4-\mathrm{H}$ inductance resonante at 60 Hz .


[^0]
r-
--FREQUENCY-

C


At very high frequencies current travels close to the outer surface of the conductor and edoy current losses increase beneath the surface. This effect is called "skin resistance" or "it resistance." This chart shows the minimum required conductor depth related with trequency. The depth varies with the resistivity of the material and is least for silver. Therefore, a silver plating is frequently applied to conductors that are used at high frequencies so as to reduce the skin resistance.

FOR EXAMPLE: At 200 MHz a minimum thickness of 0.81 mils of cadmium is required, whereas anly 0.18 mils of silver are needed at the same frequency.


| Circuit | Series combinution | Smpertance $\mathbf{Z}=\boldsymbol{R}+\boldsymbol{j} \boldsymbol{X}$ | Magrivive of imperdance $\|Z\|=\sqrt{R^{T}+X^{\prime}}$ | $\begin{gathered} \text { Phase nngle } \\ \phi=\tan ^{-1}(X / R) \end{gathered}$ | $\begin{aligned} & \text { Admintance } \\ & \mathbf{Y}=1 / \mathbf{z} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\longrightarrow \mathrm{M}$ | $R$ | ohms $\pi$ | oluns R | $\begin{gathered} \text { radians } \\ 0 \end{gathered}$ | $\begin{aligned} & \text { mhos } \\ & 1 / R \end{aligned}$ |
| $\xrightarrow{\sim}$ | 1 | +jut | $\sim 1$ | $+\pi / 2$ | -j(t/ $/ \omega L$ |
| 1 | $c$ | $-8(1 / * C)$ | $1 / \omega C$ | - $/$ /2 | $j \omega C$ |
| N-N | $R_{1}+R_{1}$ | $R_{4}+R_{4}$ | $R_{4} \div \boldsymbol{R}_{\mathbf{4}}$ | 0 | $1 /\left(R_{1}+R_{1}\right)$ |
|  | $L_{1}(M) L_{1}$ | $+j \vee\left\langle L_{4}+L_{0} \pm 2 S_{1}\right\}$ | $-\left(L_{0}+L_{t} \pm 2 \mathrm{M}\right)$ | + $/ 2$ | $-j / \psi\left(L_{1}+L_{1} \pm 2 M_{1}\right.$ |
| $\longrightarrow \longmapsto$ | $c_{3}+\ldots$ | $-j \frac{1}{2}\left(\frac{C_{1}+C_{3}}{C_{1} C_{7}}\right)$ | $\frac{1}{4}\left(\frac{C_{1}+c_{1}}{C_{2} C_{1}}\right)$ | $-\frac{\pi}{2}$ | $j \omega\left(\frac{C_{1} C_{1}}{C_{1}+C_{1}}\right)$ |
| N-CM- | $\boldsymbol{R}+\mathrm{L}$ | $R+f w L$ | $\sqrt{R^{\prime}+w^{\prime \prime}}$ | $\tan ^{-1} \frac{\operatorname{coL}}{R}$ | $\frac{R-j \omega L}{R^{\prime}+\omega L^{n}}$ |
| $N$ | $R+C$ | $R=j \frac{1}{-C}$ | $\sqrt{\frac{e^{7} C^{1} R^{4}+1}{{ }^{1} C^{4}}}$ | $=\tan ^{-1} \frac{1}{\omega R C}$ | $\frac{\omega^{2} C^{\prime} R+j \omega C}{\omega^{\prime} C^{\prime} R^{1}+1}$ |
| Mrnll | $L+C$ | $+j\left(\omega L \div \frac{1}{\omega C}\right)$ | $\left(\omega L-\frac{1}{\omega C}\right)$ | $\pm \frac{10}{2}$ | $-\frac{j \omega C}{\omega^{L} C} C-1$ |
| -m-rryl | $R+L+C$ | $R+j\left(\omega L-\frac{1}{m c}\right)$ | $\sqrt{R^{2}+\left(-L-\frac{1}{\operatorname{coc}}\right)^{2}}$ | $\tan ^{-1}\left(\frac{\omega L-1 / \omega}{R}\right)$ | $\frac{R-j(\omega L}{R^{i}+(\omega L} \frac{-1 / \omega C)}{-1 / \omega C)}$ |


| Circuit | Paratiti combination | $\begin{gathered} \text { tmpedance } \\ \mathbf{z}=\boldsymbol{R}+i \boldsymbol{X} \end{gathered}$ | Magnitade of impedince $\|Z\|=\sqrt{R^{\prime}+X^{k}}$ | $\begin{gathered} \text { Phase nagle } \\ \phi=\tan ^{-1}(X / R) \end{gathered}$ | $\begin{aligned} & \text { Admitunce } \\ & Y=1 / Z \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | $R_{1}, R_{2}$ | $\frac{R_{1} R_{n}}{R_{1}+R_{n}}$ |  | $\begin{gathered} \text { redienas } \\ 0 \end{gathered}$ | $\frac{R_{3}^{\text {mhen }}+R_{1}}{R_{1} R_{1}}$ |
|  | c, 6 , | $-j \frac{1}{2\left(C_{1}+C_{5}\right.}$ | $\frac{1}{S\left(C_{1}+C_{2}\right)}$ | $=\frac{1}{2}$ | $+i 凶 C_{1}+C_{V}$ |
|  | L, R | $\frac{4^{2} L^{4} R+j-L A^{2}}{S^{3} L^{3}+R^{2}}$ | $\frac{\sigma L R}{\sqrt{* L^{4}+R^{*}}}$ | $\underline{\tan }=1 \frac{R}{4}$ | $\frac{1}{R}=\frac{1}{\omega L}$ |
|  | R, C | $\frac{R-i-R^{4} C}{1+r^{2} R^{4} C^{4}}$ | $\frac{R}{\sqrt{1+\omega^{4} R^{2} C^{*}}}$ | $\operatorname{con}^{-1}(-\omega \mathrm{R} C)$ | $\frac{1}{R}+i \omega C$ |
|  | L, G | $+i \frac{-L}{1-L^{*} L C}$ | $\frac{\operatorname{sit}}{1-\omega^{\underline{1} L C}}$ | $\pm \frac{\pi}{2}$ | $j\left(\omega C-\frac{1}{\omega L}\right)$ |
|  | $L_{1}(M) L_{3}$ |  | $\frac{L_{1} L_{1}-M^{4}}{L_{1}+L_{1} F 2 M}$ | $\pm \frac{\pi}{2}$ | $-J \frac{1}{\omega}\left(\frac{L_{3}+L_{1} \mp 2 M}{L_{1} L_{1}-M^{\prime}}\right)$ |
|  | $L, C, R$ | $\frac{\frac{1}{R}-j\left(-C-\frac{1}{\omega L}\right)}{\left(\frac{1}{R}\right)^{2}+\left(-C-\frac{1}{\omega L}\right)^{\prime}}$ | $\frac{R}{\sqrt{1+R \cdot\left(-C-\frac{1}{4 L}\right)^{2}}}$ | $\operatorname{wn~}^{-1}-R\left( \pm C-\frac{1}{w L}\right)$ | $\frac{1}{R}+j\left(\operatorname{soc}-\frac{1}{m L}\right)$ |

Tabulated here are the effects when potentials of increasing frequency are applied to resistors, capacitors, and inductors.

As the irequency increases from dc to above resonance, the effeclive "look" of the component changes as shown.

| DC AND LOW FREQ. $\begin{gathered} \text { N }=A \\ X_{L} \cong 0 \end{gathered}$ | HIGH FREQ. <br> BELOW SELF-RESONANCE $\begin{aligned} & Z=\sqrt{R^{2}+x_{L}^{2}} \\ & x_{C} \gg x_{L} \end{aligned}$ | SELF-RESONANCE $\begin{aligned} & Z=R_{\text {EQUMV }} \\ & X_{C}=x_{L} \\ & R_{\text {EQUVV }}=\frac{(\omega L)^{2}}{R} \end{aligned}$ | $\triangle B O V E$ SELF-RESONANCE |
| :---: | :---: | :---: | :---: |
| $\begin{aligned} & z=x_{C} \\ & x_{L} \cong 0 \\ & x_{C} \gg R \end{aligned}$ | $\cdots(\cdots)$ | $\begin{aligned} & \text { Z } \\ & Z=\frac{L}{C_{D} R} \\ & x_{C}=y_{L} \\ & x_{C} \leftrightarrow x_{C_{D}} \end{aligned}$ | $\cdots \cdots m$ |
| $\begin{aligned} & Z=R \\ & x_{L} \approx 0 \\ & X_{C}=\infty \end{aligned}$ | $\begin{aligned} & Z=X_{L} \\ & X_{L}<X_{C} \\ & R \approx 0 \end{aligned}$ | $\begin{aligned} & Z=R_{\text {Equiv. }} \\ & x_{C}=X_{L} \\ & R_{\text {EQuIV. }}=\frac{(\omega L)^{2}}{R} \end{aligned}$ | $\frac{1( }{1}$ |

## RESISTANCE-VDLTAGE-CURRENT-POWER NOMOGRAM

This nomogram is based on Ohm's law, and one straight line will determine two unknown parameters if Iwo others are given. Preferred ( $\pm 20 \%$ ) resistance values are marked in addition to the ordinary resistance scale divisions. The power scale is calibrated in watts and dBm with a reference level of $0 \mathrm{dBm}=1 \mathrm{~mW}$ into 600 ohms . This, direct conversion between dBm and watts can be made. To cover a wide range of values and yet maintain accuracy, a dual numbering system is used. To avoid confusion, all members should be read from either the regular or the gray-barred scales.

FOR EXAMPLE:

1. The current through a $150-\mathrm{k}$ resistor with a polential drop of 300 V is 2 mA , and the power dissipated is 600 mW or 0.6 W .
2. When a 12,000 -ohin resistor has a current of 6 mA through it, the power dissipated is 0.43 W and the voltage across the resistor is 72 V .
3. The vollage across a 4.7 M ohm resistor with a signal level of -30 dBm is about $2,15 \mathrm{~V} \mathrm{rms}$.
4. The maximum allowable current through a 10 W 200 -ohm resistor is 0.22 A . Under these operating conditions there will be 45 V across the resistor.


## VOLTAGE DIVIDER NOMOGRAM

This nomogram aids in the rapid selection of component values for the simple resistive and capacitive voltage dividers illustrated, where

$$
\frac{\theta_{0}}{e_{t}}=\frac{R_{g}}{R_{9}+R_{s}} \text { or } \frac{\theta_{0}}{e_{j}}=\frac{C_{s}+C_{g}}{C_{s}}
$$

Only two decades are covered on the left and right scale to achieve maximum accuracy. The range of the nomogram can be extended by multiplying these two columns by the same power of ten without making any changes in the center column.

FOR EXAMPLE:

1. A blocking oscillator must be held at cutoff by means ol a voltage divider between $B$ - and ground. Cut-off bias is -15 V , the negative supply is 150 V , and the grid-to-ground resistor is 22,000 ohms. Thus, $e_{0} / \theta_{i}$ is 0.1 . Joining that value with 2.2 on the $R_{g}$ scale gives 20 on the $R_{s}$ scale, which makes that resistor equal to 200,000 ohms since each scale had to be multiplied by $10^{4}$.
2. Design an rif probe with a $5: 1$ attenuator using standard capaciance values. Rotating about the 0.2 point on the center scale gives typical values of 30 pF for $C_{9}$ and 7.5 pF for $C_{s}$.

NOTE: The longer lines outside the left and righi columns locate standard $\pm 10 \%$ values and the shorter lines locate standard $\pm 5 \%$ values.



It is often necessary to know the portion of the input voltage that will appear across the load resistor in a capacitively coupled circuit. This is a function of frequency and a factor of the ratio of $R$ to $X_{c^{\prime}}$, the required ratio is shown on the center scale. It is interesting to note that any ratio of $R 10 X_{c}$ greater than $7.4: 1$ yields over $99 \%$ output. The $X_{c}$ and $R$ scales can be multiplied by any common power of ten to extend the range of the nomogram.

FOR EXAMPLE: For $A=100 \mathrm{k}$ and $X_{c}=10 \mathrm{k}, V_{2}$ will be $99.4 \%$ of $V_{r}$.


This nomogram is used to calculate phase shift and attenuation in R-C coupling networks. To use, connect capacitance with frequency and note the intersect point on the turning scale. Using this intersect point, connect to the resistance, and by extending this line, read attenuation and phase shiit.

FOR EXAMPLE: At 60 Hz, a $0.01-\mu \mathrm{F}$ capacitor and 10,000 -ohm resistor will exhibit $\begin{aligned} & \mathrm{p} \\ & \text { phase shift of } 72^{\circ} \text { and }\end{aligned}$ an attenuation factor of 0.35 .


This table illustrates how performance characteristics of an amplifier can be determined by observing the waveform of the oulpul, when the input is a square wave.

| Output Waveform | Low Frequency |  | High Frequency |  | Damping |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Gain | Delay | Gain | Delay |  |
| -- | Ideal | Ideal | Ideal | Ideal | Ideal |
|  | Inadequate | Good | Excessive | Good | High |
|  | Excessive | Good | Inadequate | Good | High |
|  | Good | Excessive | Good | Inadequate | High |
|  | Good | Inadequate | Good | Excessive | High |
|  | Excessive | Excessive | Inadequate | Inadequate | High |
| - | Excessive | Inadequate | Inadequate | Excessive | High |
|  | Inadequate | Excessive | Excessive | Inadequate | High |
|  | Good | Good | Excessive | Good | Medium |
|  | Good | Good | Excessive | Good | Low |
| 1-- | Good | Good | Excessive | Good | Poor |
| ------] | Good | Good | Sharp <br> Cutoff or Peaked | Good | Low |

## LOW-END AMPLIFIER RESPONSE

In an RC-coupled amplifier, the coupling capacitanca ( $C$ ), combines with the output load ( $R$ ), to form a potential divider or filter.

The response curve of this combination usually is specified in terms of the relative gain -3 dB point which can be calculated from the equation:

$$
\frac{e_{2}}{e_{1}}=\frac{1}{\sqrt{1+\frac{1}{(2 \pi I T)^{2}}}}=0.708
$$

where $T=R C$ and 0.708 is used to calculate the 3 dB point.
The accompanying nomogram relates the parameters $R, C$ or ${ }_{-301}$. Given any two, the third term can be determined by a simple straight-line alignment.

EXAMPLE: With a load of 10 k , what capacitance will give a low cutoff frequency of 20 Hz ?
The alignment shows that a capacitor of $0.8 \mu \mathrm{~F}$ will yield the desired high-pass characteristic.


## TIME-CONSTANT NOMOGRAM (A)

This nomogram is besed on the formula $T=R C$ where $T$ (the time constant) is the time required for the capacitor in an $R C$ series circuit to reach $63.2 \%$ of the applied voltage.

FOR EXAMPLE: The time constant of 10 msec can be achieved with a $1-\mathrm{M}$ ohm resistor and a $0.01-\mu \mathrm{F}$ capacitor.


TIME-CONSTANT NOMOGRAM (B)
This chart is used to determine the time required in an RC series circuit to reach a given fraction of an applied step input, or to determine the percent of the applied input when the time constant is given.

The nomogram is based on the relationship.

$$
\frac{E_{\text {out }}}{E_{\text {in }}}=1-\theta^{-u A C}
$$

FOR EXAMPLE: Determine the time required to charge a $50-\mu \mathrm{F}$ capacitor to 400 V through $1,000 \mathrm{ohms}$ from a 450 V supply. The percent of applied voltage is $88.5 \%(400 / 450)$ which requires 2.2 time constants. The time constant is 50 ms (from time-constant nomogram A), so the time required to charge to 400 V is 110 ms .


The expression $t=1 / 2 \pi R C$, where $f$ is in hertz, $C$ and $R$ in ohms, is the expression for:

1. The $3-\mathrm{dB}$ bandwidth of a single tuned elrcuit having parameters as shown in Figure 1.
2. The frequency at 3 dB relative attenuation of the paraliel AC low-pass network shown in Figure 2 ,
3. The frequency at 3 dB relative transfer attenuation of the series AC high-pass network of Figure 3.
4. Wien bridge balance.

FOR EXAMPLE:

1. The circuit shown in Figure 1 is used to couple two successive stages of an amplifier. The $3-\mathrm{dB}$ bandwidth of the circuit must be 3.4 MHz and the equivalent shunt capacitance of the circuit is 25 pF . What equivalent resonant resistance will the circuit exhibit? Connect 3.4 MHz and 25 pF and find the equivalent resonant resistance as 1,850 ohms.
2. The low-pass network of Figure 2 uses a $0.05-\mu \mathrm{F}$ capacitor. What value of resistance is required for the output to drop to 0.707 of the input at 5 kHz ? Connect $0.05 \cdot \mu \mathrm{~F}$ with 5 kHz and read answer as 620 ohms.


Figure 1. Characteristios of a single tuned circuit.


Figure 2. Characteristics of a parallel AC low-pass network.


Figure 3. Transfer characteristics of an RC high-pass network.
3. It is required that the RC high-pass network in Figure 3 attenuate rapidly below 300 Hz . What value resistor must be used with a $0.1-\mu \mathrm{F}$ capacitor? Connect $0.1-\mu \mathrm{F}$ with $300 \mathrm{~Hz}(0.3 \mathrm{kHz})$ and read answer as 5,250 ohms.
4. Figure 4 shows an AC coupled amplifier and its equivalent circuits. It is assumed that the reactance of the bypass capacitors is negligible throughout the frequency range of the amplifier. If the equivalent circuit resistance has a value of 1.300 ohms and the equivalent capacitance is 25 pF , at what frequency is the amplification 0.707 of the midfrequency range of the amplifier? Connect 25 pF and 1,300 ohms and read frequency of 4.75 MHz at which amplifier gain is down 3 dB .
5. The Wien bridge circuit shown in Figure 5 has $R_{1}$ and $R_{2}$ equal to 10,000 ohms and $C_{1}$ and $C_{2}$ equal to $0.1-\mu \mathrm{F}$. With those values the balance frequency of the circuit is 1.59 kHz .

$$
\begin{aligned}
& R_{1}=R_{2}=R \\
& C_{4}=C_{2}=C \\
& R_{3}=2
\end{aligned}
$$

For the measurement of frequency, the unknown frequency is connected across A and B and a null delector, across $C$ and $D$.

When used with an oscillator, the circuit is connected to a suitable amplifier with regeneralive feedback.



Figure 5. ConventionalWien bridge circuit.

Figure 4. An RC-coupled amplifier and its equivalent circuits.


HIGH FREQUENCY EQUIVALENT


MID FREQUENCY EQUIVALENT


LOW FREQUENCY EQUIVALENT

Figure 4. Circuit Diagram of N-Channel JFET Transistor Amplifer. (Continued from page 111.)


Note: Scales with corresponding letters ( $A$ or B) are used together.

## BANDWIDTH NOMOGRAM

This nomogram is used to compute the bandwidth of a tuned circuit at $70.7 \%(-3 \mathrm{~dB})$ of maximum gain. It is based on the equation

$$
\Delta f=\frac{f}{Q}
$$

where
$\Delta f=$ bandwidth in kiloherlz
$f_{r}=$ resonant frequency in megahertz
$Q=$ flgure of merit of the inductance
FOR EXAMPLE:

1. A circuit that has a resonant frequency of 6 MHz , and uses an inductance with a $Q$ of 140 , will have a bandwidth of 43 kHz . NOTE: The range of the nomogram can be extended to cover other frequencies by multiplying or dividing both frequency scales by the same power of 10 .
2. To achieve a bandwidth of 2.5 kHz at a resonant frequency of 600 kHz the inductance must have a $Q$ of 240.
$\sim$
$\sim$

(d) Seriez fype, 6 ds per octaun.

(e) Paralled type. 6 as per octave.

(b) Serics t/pen 12 da per octave.

(d) Paraticl type. 12 dB jer octaut.

| $c_{1} \cdot \frac{1}{\omega_{t} R_{0}}$ | Mad | $L_{1}=\frac{H_{a_{2}}}{w_{c}} \text { MEWAY }$ | $\mathrm{Cr}_{5}$ - STH |
| :---: | :---: | :---: | :---: |
| $c_{2}=\sqrt{2} c_{1}$ | Farat | $L_{2}-\frac{L_{1}}{\sqrt{2}}$ HEMRY | $\mathrm{R}_{9}$. SPEAKER IWPEOANCE |
| $c_{3}+\frac{c_{1}}{\sqrt{\frac{1}{2}}}$ | FAFAD | L3: $\sqrt{2}$ L HENAY | ${ }^{1} \mathrm{E}$, CROSSOVER FRED |

m-derived crossover network.

(a) Parallel fype. Itces ptr ottave,

(c) Saries tipe, 15d per octaue.

(古) Purglte1 type. 12 as per octatet.

(d) Serisu type, 12 ds per ocrawe.





Conslant-resistanct, constant-k nefowark


Crostower curves showing 6,12 , and 18 dB/octave crossovef net-work culdif rate.
(Reprinted from Radio-Electronics, copyright © Gainsback Publicatlons, Inc., March, 1968.)

## PASSIVE LC FILTER DESIGN

Previous editions of the Electronic Databook used nomograms to determine the component values of image parameter lowpass and highpass filters. This edition provides computer-calculated tabulations of modern filter designs that are based on network synthesis. These modern designs are more versatile, less complicated and easier to build than the old image parameter designs. For example, to simplify construction, the tabulated modern filter designs require fewer components than comparable image parameter designs, and all (or most) of the capacitor values of the modem filter designs are standard values.

Most filtering applications do not require a precisely defined cutoff frequency, and as long as the actual cutoff frequency is within about five percent of the desired cutoff frequency, and the passband and stopband attenuation levels are satisfactory, the design will be acceptable. Of almost equal importance is finding a design that has the minimum number of components and that requires standard-value capacitors to simplify the ordering of parts and the assembly of the filter. Standard values for the inductors is less important because the inductors are usually hand-wound or ordered to specification from inductor manufacturers.

Each filter table provides many designs over one frequency decade in which the change in cutoff frequency from one design to the next is sufficiently small so that virtually any cutoff requirement can be satisfied within a few percent. The 50 -ohm impedance level for source and load was used for most of the tabulations because this impedance termination is most frequently needed by the electronics engineer. All component values and frequencies versus selected stopband attenuation levels have been computer-calculated for each design for the convenience of the user. Although the tabulated designs are only for the equally terminated condition at the listed impedance level and frequency decade, a simple scaling procedure allows the tables to be scaled to any equally terminated impedance level and any frequency decade, while keeping the important advantage of all designs requiring only standard-value capacitors. These pre-calculated filter tables are therefore universally applicable because they can be used to select a suitable design having standard-value capacitors for any impedance level or any cutoff frequency.

Only the passive LC filter was considered for tabulation because this filter type is capable of passing if power, whereas the active filter is not. Also, the passive filter does not require a power supply, and it usually is easier to assemble in small quantities than the active filter.

## Filter Types and Responses

Only the lowpass and highpass filter types having the Chebyshev or elliptic attenuation responses are considered. For design information on other filter types (bandpass, bandstop, etc.), and responses (Butterworth, Bessel, etc.), see References 13-18. Only the 5 th- and 7 th-degree Chebyshev designs ( 5 and 7 elements each, respectively) and the 5 th-degree elliptic design are included in the tables because these designs are suitabie for almost all of the non-stringent filtering requirements encountered by the non-professional filter designer.

The Chebyshev attenuation response is characterized by attenuation ripples in the passband and a constantly (monotonic) increasing attenuation in the stopband. The level of maximum passband ripple ( $A_{p}$ ) is directly related to the filter reflection coefficient (RC) and VSWR (see Appendix A), and these parameters can be increased or decreased to get a corresponding increase or decrease in the rate of attenuation rise in the filter stopband in the vicinity of the filter cutoff frequency.

The elliptic attenuation response is characterized by altenuation ripple in the passband, attenuation peaks in the stopband, and a specific level of minimum stopband attenuation. The presence of the two resonant circuits in the elliptic filter configuration results in a more abrupt rise in attenuation than is possible with the Chebyshev configuration.

[^1]Filter Tables
Lowpass and highpass filter designs are listed in ten tables, with eight tables based on a 50 ohm impedance level, and two tables (5B and 8 B ) based on 600 ohms. The schematic diagram and a typical attenuation response of each tabulated filter appears at the head of each table, except Tables 5 B and 8 B , where the only difference is the impedance level. The component designations in the schematic diagram and the frequency designations ( $F_{c o}, F 3$, F20 and F50) in the attenuation response diagram correspond to similar designations in the table column headings.

Although there is passband ripple in all these designs, the amplitude of the ripple is so small that it is usually swamped out by the losses of the filter componenls. Consequently, when the completed design is measured, the passband response appears to be flat. For this reason, the passband in the response diagrams is shown flat.

The filter reflection coefficient (RC) provides an indication of the flatness of the passband and the VSWR of the filter. For rf filtering applications where low VSWR is desired, designs with low reflection coefficients are preferred. For audio filtering applications, where a faster rise of attenuation is more important than minimizing VSWR, designs having high RC values are preferred.

## Lowpass Filters

Chebyshev Designs and Applications. Tables 1 through 4 list 5 - and 7-element Chebyshev lowpass designs. Use the 5 -element designs when about 30 dB of attenuation is needed at one octave above the cutoff frequency, and the filter component count must be minimized. Use the 7 -element designs when about 42 dB of attenuation is needed at one octave above the cutoff frequency. A typical application for these filters is to reduce the harmonic output of transistor amplifiers. Normally, the capacitive input/oulput configurations shown in Figures 1 and 3 are preferred to the alternative inductive input/output configuralions in Figures 2 and 4 to minimize the number of inductors, Inductors are usually more bulky, more expensive and have higher losses than capacitors. Both filter types have identical attenuation responses, but the filter input impedances in the stopbands are markedly different. For the inductive input filter, the input impedance starts increasing between the 3 and $15-d B$ attenuation level, and continues increasing with increasing stopband trequency. The reverse is true for the capacitive Input fllter. Under certain conditions, transistor if amplifiers may become unstable when looking into a decreasing or increasing reactive impedance (see Bibliography, Nos. 8 \& 15). Because of this, it is necessary that the if filter designer be able to design lowpass filters having either capacitive or induclive input elements.

Elliptic Designs and Applications. Tables 5A and 58 list 5th-degree elliptic lowpass designs for 50 and 600 ohms, respectively. This type of filter is preferred where a more abrupt rise in attenuation is desired. This type is also useful because the attenuation peaks at F4 and F2 somelimes can be placed at the second and third harmonic frequencies of a constant-frequency il amplifier to provide more than 60 dB attenuation to the harmonics.

In this filter type, only capacitors C1, C3 and C5 are standard value. The fact that C2 and C4 are not standard values is not important because these capacitors should be tuned to precisely resonate L2 and L4 at F2 and F4. This is necessary if the minimum stopband attenuation level $\left(A_{s}\right)$ is to be achieved throughout the entire stopband. A slight variation in the values of C2, L2 and C4, L4 is not important as long as the F2 and F4 frequencies are as close as possible to the tabulated frequencies.

Table 5B is provided for audio filtering applications where this impedance level is very common. This table also serves to provide 600 -ohm designs that can be used to confirm the correctness of the impedance scaling procedure to be explained later.

## Highpass Filters

Chebyshev Designs and Applications. Tables 6 and 7 list 5-and 7-element Chebyshev highpass filter designs, but unlike the lowpass designs only the capacitive input/output configuration is considered. This is because they are very few applications for the alternate L-input/output configuration. The C-input/output configuration has the imporiant advantage of increasing input impedance with decreasing frequency. This configuration is therefore suitable as an isolation network between a signal source and a detection system being used to examine the Marmonics of the signal source fundamental. The highpass filter passes the harmonic frequencies unattenuated,
but provides considerable altenuation to the fundamental signal. Also, the high input impedance of the filter will not cause excessive loading of the generator. This is not true for the alternate inductive inpul filter.

Elliptic Designs and Applications. Tables 8 A and 8 B list the 5th-degree elliptic highpass designs for 50 and 600 ohms, respectively. This type filler is preferred where a more abrupt increase in attenuation is desired as compared to the Chebyshev filter. The comments concerning the elliptic lowpass design relative to $\mathrm{C} 1, \mathrm{C} 3$ and C5 being standard values and the importance of tuning C2 and C4 to F2 and F4 are equally applicable here. The concluding comments about the elliptic 600 -ohm lowpass filter are equally applicable to the highpass filter.

## How to Use the Precalculated Design Tables

For 50-0hm Impedance Levels. Before selecting a suitable filter design, the reader must know or be able to specity the important parameters of the fitter, such as type (highpass or lowpass), cutoH frequency, impedance level, and an approximation of the required stopband attenuation. It is obvious as to which tables to use lor lowpass or highpass applications, but it is not so obvious as to which one design of the many possible choices is optimum for the intended application. Generally, the Chebyshev is preferred over the elliptic because ihe Chebyshev does not require tuning of the inductors; however, if the gradual rise in attenuation of the Chebyshev is nol satislactory, then the elliptic should be considered. For audio frequency filtering, the elliptic designs with high values of RC are preferred because they have a much more abrupt rise in attenuation as compared to the Chebyshev. For if appllcations, RC values less than $8 \%$ are recommended to minimize VSWR. Low VSWR is also important when cascading high and lowpass designs to achieve a bandpass response of more than iwo octaves wide. Each filter will operate as expected if it is correctly terminated, but this condition will exist only if both designs have the relatively constant terminal impedance that is associated with low values of $R C$.

Knowing the filter type and the response needed, the table of designs most appropriate for the application is selected on a trial basis. Find the table and search the cutof frequency column for a cutoff frequency nearest the deslred cutoff frequency. After finding a possible design, examine the stopband attenuation levels to see if they are satisfactory. Then check the RC value to see if it is appropriate for the application. Finally, check the component values 10 see if they are convenient. Usually, it is easler to obtain capacitors with the ten-percent tolerance than the five-percent value. For example, in the audio frequency range, the capacitor values will probably be in the microfarad range, and capacitors in this size are available only in the ten-percent tolerance group.

Because all the important parameters of each design are listed, it is possible to quickly check many designs so the most suitable design can be selected. After the final choice has been made, interconnect the components in accordance with the schematic diagram above the table headings. Use good engineering practices in assembling the filter components as explained in listing number 12 of the bibliography.

For Impedance Levels Other Than $\mathbf{5 0}$ Ohms. All tabulated designs are easily scaled to impedance levels other than 50 ohms while maintaining the advantage of slandard-value capacitors. If the impedance level differs from fifty ohms by a factor equal to an integral power of ten (such as ,01, 1, 10 or 100), the design tables can be scaled by inspection (by shifting the decimal points of the component values). The tabulated frequency, $A_{s}$ and $R C$ values remain unchanged. For example, if the 50 -ohm impedance level is raised by a factor of ten to 500 ohms, the new capacilance and inductance values are found by multiplying the tabulated inductance values by len, and by dividing the capacitor values by len. This means that the decimal points of the inductor values are shifted one place to the right, and the decimal points of the capacitor values are shifted one place to the left. The reverse is true if the impedance level is reduced from 50 to 5 ohms. For example, the impedance level of Design \#1, Table 1, can be increased to 500 ohms by shifting the decimal points of L. 2 and L4 one place to the right (to become 107.3 $\mu \mathrm{H}$ ), and by shifting the decimal points of the capacitance values one place to the lef (to become 300 pF and 560 pF ).

To change the tabulated frequency decades to another frequency decade differing by a factor equal to an integral power of ten, mulliply all tabulated frequencies by the factor, and diwide all capacitance and inductance values by the same factor. For example. the frequency decade of Table 1 can be reduced from $1-10 \mathrm{MHz}$ to $1-10$ kHz by multiplying all frequencies by .001 (the frequency units in the column headings become kHz ), and by
dividing the capacitance and inductance values by the same factor. (The units of capacitance and inductance become nanofarads and millihenries.)

Filter designs wilh standard-value capacitors may be found for impedance levels thal differ from 50 ohms by a factor equal to a non-integral power of ten (such as 1.2, 12, etc.). To do this, use the following procedure:

1. Calculate the scaled impedance factor, $R=Z_{x} / 50$ where $Z_{x}$ is the desired new impedance levelin ohms.
2. Calculate the cutof trequency of a "rrial" 50 -ohm filter using the equation: $F_{50_{c o}}=R \cdot F_{x_{c o}}$ where $F_{x_{c o}}$ is the desired cutoff Irequency of the filter at the new impedance level.
3. From the 50 -ohm tables, select a design having its cutoff frequency closest to the calculated $\mathrm{F}_{\text {so }}$ value. The tabulated capacilor values will be used directly, and the frequencies and inductance values will be scaled.
4. Calculate the exact values of $F_{x_{c 0}}=F_{50_{c o}}^{\prime} / R$, where $F_{50_{\infty}}^{\prime}$ is the tabulated cutoff frequency. In a similar manner, calculate all the other frequencies.
5. Calculate the new inductance values for the new filter from $L_{x}=R^{2} \cdot L_{30}$, where $L_{s 0}$ is the tabulated inductance value of the trial filter design, and $\mathrm{L}_{x}$ is the Inductance value of the scaled filter.

An example follows showing how the $50-0 \mathrm{hm}$ design \#3 of Table 5A can be replaced with a 60 -ohm design having a similar cutoff frequency and other similar characteristics. Using the same previously numbered steps:

1. $R=60 / 50=1.2$
2. $F_{50_{\mathrm{co}}}=1.2(1.06 \mathrm{MHz})=1.272 \mathrm{MHz}$
3. From Table 5A, design \#15 has a cutoff frequency closest to the calculated $F_{50}$ value. The $A_{s}$ and $R C$ values are similar to design \#3. Design \#28 is also suitable as a replacement. The tabulated capacitor values of design \#15 are copied directly. Thus, C1, 3, 5, 2 and $4=2,200,3,900,1,800,271$ and 779 pF , respectively.
4. The exact values of $F_{x_{c 0}}, F_{x_{3}}$ and $F_{A_{3}}$ are calculated, and are equal to: $1.27 \mathrm{MHz} / 1.2=1.058 \mathrm{MHz}, 1.45$ $\mathrm{MHz} / 1.2=1.208 \mathrm{MHz}$ and $2.17 \mathrm{MHz} / 1.2=1.808 \mathrm{MHz}$.
5. The L2 and L4 induclance values of the 60 ohm filter are calculated: $L_{x}=(1.2)^{2} \cdot 7.85 \mu \mathrm{H}=11.3 \mu \mathrm{H}$, $\mathrm{L}_{x}=(1.2)^{2} \cdot 6.39 \mu \mathrm{H}=\mathrm{H}=9.20 \mu \mathrm{H}$. The validity of the scaling procedure can be confirmed by scaling the new $60-0 \mathrm{hm}$ filter to an impedance level of 600 ohms, and scaling the frequency from 1 MHz to 1 kHz , and then comparing the $600-\mathrm{hm}, 1 \mathrm{kHz}$ filter with design $\# 5$ of Table 5B. All parameters of the designs will be identical, thus confirming the correctness of the scaling procedure.

The validity of the pre-calculated tables may be confirmed by independently calculating the component values using previously published normalized tables from authoritative sources such as References 8 - 10 and 13. This is done by finding a labulaled pre-calculated design that has a reflection coeflicient nearly identical to that of a published normalized design. For example, design \#80, Table 3 is suitable to match a $10 \%$ AC Chebyshev design. The pre-calculated impedance level and the cutoff frequency are then used with the normalized values, and the inductance and capacitance component values are calculated in the usual manner. Because the pre-calculated tabulaled values agree within less than $1 \%$ variation with the independently calculated values, the correctness of the tables is confirmed.

## APPENDIX A

Equations and Table Relating RC, $A_{p}$ and VSWR for all Modern Design Filters

$$
\begin{align*}
& \mathrm{AC} \\
& \text { where }  \tag{1}\\
& \text { wher } 100 * S Q R=100 \text { times the square root of } \ldots \\
& x=0.1\left(A_{p}\right) \\
& \uparrow=\text { symbol for exponentiation } \\
& *=\text { symbol for multiplication }
\end{align*}
$$

$$
\begin{equation*}
A_{D_{(d \mathrm{~dB})}}=-4.3429 * \operatorname{LOG}[1-(.01 * R C) \uparrow 2] \tag{2}
\end{equation*}
$$

VSWR $=[1+(.01 * R C)] /[1-(.01 * R C)]$
where $\quad A_{p}=$ Maximum passband ripple amplitude in $d B$
RC $=$ Reflection coefficient in percent
$V S W R=$ Voltage standing wave ratio
Equations $1-3$ are presented in a format suitable for computer programming. The LOG function in Eq. (2) is based on the natural log.

Table 1. Reflection Coefficient with Correspending Values of $A_{p}$ and VSWR.

| REFLECTION COEFFICIENT <br> (\%) | MAX. RIPPLE AMPLITUDE (dB) | MAX. VSWR $\qquad$ | REFLECTION COEFFICIENT <br> (\%) | MAX. AIPPLE AMPLITUDE (dB) | MAX. VSWA $\qquad$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1.0 | 0.000434 | 1.020 | 12.0 | 0.0630 | 1.273 |
| 2.0 | 0.001738 | 1.041 | 14.0 | 0.0860 | 1.326 |
| 3.0 | 0.003910 | 1.062 | 16.0 | 0.1126 | 1.381 |
| 4.0 | 0.006954 | 1.083 | 18.0 | 0.1430 | 1.439 |
| 5.0 | 0.010871 | 1.105 | 20.0 | 0.1773 | 1.500 |
| 6.0 | 0.015663 | 1.128 | 22.0 | 0.2155 | 1.564 |
| 7.0 | 0.021333 | 1.151 | 24.0 | 0.2576 | 1.632 |
| 8.0 | 0.027884 | 1.174 | 26.0 | 0.3040 | 1.703 |
| 9.0 | 0.035321 | 1.198 | 28.0 | 0.3546 | 1.778 |
| 10.0 | 0.043648 | 1.222 | 30.0 | 0.4096 | 1.857 |

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The first four references are recommended as authontative sources on image parameter passive LC filter design.
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Fgure 1. Lowpass filter schemetic diagram and attenuation response, capacitive input and output.
Table 1. 50 -Ohm 5-Element Chebyshev Lowpass Fitter Designs Using Standard-Vafue Capacitors, Capacitive Input and Output.
(Continued on page 124.)

| Filher . . . . Frequency ( MHz ) . . . . |  |  |  |  | RC <br> (\%) | $\begin{gathered} \mathrm{Cr}, \mathrm{C} 5 \\ (\mathrm{pf}) \end{gathered}$ | $\begin{gathered} \mathrm{L}, \mathrm{~L} 4 \\ (\mu \mathrm{H}) \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{C}_{3} \\ \text { ( } \mathrm{PF} \text { ) } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| No. | Cutoff | $3-\mathrm{dB}$ | 20-dB | $50-\mathrm{dB}$ |  |  |  |  |
| 1 | 1.616 | 1.209 | 1.652 | 3.936 | 9,58 | 3068 | 10.73 | 5600 |
| 2 | 1.161 | 1.329 | 1.869 | 3.334 | 9.98 | 2700 | 9.882 | 5190 |
| 3 | 1.69\% | 1.371 | 1.944 | 3.65 | 4. 16 | 2200 | 9.818 | 4709 |
| 4 | 1.146 | 1.405 | 1.951 | 3.618 | 7.19 | 2460 | 9.373 | 4796 |
| 5 | 1.127 | 1.496 | 2.125 | 4.062 | 3.88 | 2006 | 9.063 | 4300 |
| 6 | 1.256 | 1.541 | 2.133 | 3.955 | 7.27 | 2208 | 8.564 | 4396 |
| 7 | 1.054 | 1.619 | 2.379 | 4. 565 | 1.89 | 1684 | 8.351 | 3906 |
| 8 | 1.232 | 1.646 | 2.344 | 4.420 | 3.67 | 1896 | 8.187 | 3559 |
| 9 | 1.388 | 1.761 | 2.353 | 4.364 | 7,38 | 2906 | 7.754 | 3960 |
| 19 | 1.169 | 1.755 | 2.576 | 4.922 | 1.69 | 1506 | 7.703 | 3660 |
| 11 | 1.275 | 1.771 | 2.547 | 4.935 | 2.77 | 1696 | 7.635 | 3690 |
| 12 | 1.462 | 1.825 | 2.542 | 4.731 | E. 30 | 1889 | 7.281 | 3609 |
| 13 | 1,430 | 1.939 | 2.775 | 5.241 | 3.29 | 1569 | E.950 | 3300 |
| 14 | 1,541 | 1.971 | 2.768 | 5,175 | 5.16 | 1699 | 6.789 | 3300 |
| 15 | 1.315 | 2.101 | 3.108 | 5.989 | 1. $0^{7}$ | 1209 | 6.424 | 3001 |
| 16 | 1.481 | 2.117 | 3.065 | 5.685 | 2.26 | 1394 | 6. 393 | 3096 |
| 17 | 1.754 | 2.190 | 3.050 | 5.677 | 5.36 | 1596 | 6.067 | 3096 |
| 18 | 1.827 | $2 \times 25$ | 3. 1180 | 5.069 | 9.35 | 1690 | 5.773 | 3060 |
| 19 | 1.506 | 2.337 | 3.440 | 6.611 | 1.29 | 1109 | 5.782 | 2786 |
| 29 | 1.701 | 2.361 | 3.396 | E. 4.41 | 2.77 | 1264 | 5.72E | 2769 |
| 21 | 1. 6.68 | 2.493 | 3.385 | 6. 335 | 4.93 | 13010 | 5.573 | 2700 |
| 22 | 1. 7.75 | 2.634 | 3.854 | 7.383 | 1.59 | 1081 | 5.135 | 2496 |
| 23 | 1.985 | 2.671 | 3.816 | 7.193 | 3.43 | 1100 | 5. 0149 | 2400 |
| 24 | 2.193 | 2.737 | 3.813 | 7.696 | 6.30 | 1200 | 4.854 | 2400 |
| 25 | 2.402 | 2.83\% | 3.965 | 7.694 | 18.21 | 1360 | 4.547 | 2496 |
| 2 E | 1.892 | 2.378 | 4.216 | 8.013 | 1.56 | 515 | 4.799 | 2206 |
| 27 | 2.145 | 2.599 | 4.159 | 7.861 | 3.29 | 1095 | 4.641 | 2204 |
| 28 | 2. 392 | 2.966 | 4.159 | P.P41 | 6. 56 | 1189 | 4.449 | 2 CaH |
| 29 | 2.153 | 3.157 | 4.639 | 8.965 | 1.38 | 829 | 4.263 | 2 mb |
| 30 | 2.362 | 3.261 | 4.555 | 8.645 | 3.31 | 915 | 4.217 | 2060 |
| 31 | 2.631 | 3.284 | 4.575 | 8.515 | e.30 | 5000 | 4.045 | 2904 |

Table 1. 50-0hm 5-Element Chebyshev Lowpass Filter designs
Using Standard-Value Capacitars, Capacitive Input and Output. (Continued from Page 123.)

| Filter - - . . Frequency ( MHz ) - . . . |  |  |  |  | RC | C1, C 5 | L2, L4 | $\mathrm{C3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| No. | Cutof | 3-dB | $20-\mathrm{dB}$ | 50-dB | (\%) |  | ( $\mu \mathrm{H}$ ) | ( PF ) |
| 32 | 2.368 | 3.512 | 5.139 | 9.643 | 1.60 | 759 | 3.851 | 1896 |
| 33 | 2.623 | 3.557 | 5.523 | 9.603 | 3.34 | 8Сй | 3.794 | 18 mb |
| 34 | 2.960 | 3.664 | 5.689 | $9.45 \%$ | 6.7E | 910 | 3.614 | 1809 |
| 35 | 2.185 | 3.959 | 5.763 | 11.81 | 1.32 | ES9 | 3.418 | 16.40 |
| 36 | 3.058 | 4. 423 | 5.710 | 16.74 | 4.10 | 756 | 3.340 | 166 |
| 37 | 3.381 | 4.145 | 5.734 | 15.58 | 7.35 | 820 | 3.182 | 16 Ca |
| 35 | 2.772 | 4.212 | E. 175 | 11.34 | 1.49 | 52¢ | 3.211 | 1590 |
| 39 | 3.135 | 4.265 | 6.161 | 11.54 | 3.22 | E89 | 3.166 | 1500 |
| 40 | 3.508 | 4.379 | E.106 | 11.35 | 5.36 | P59 | 3. 633 | $15 \mathrm{El3}$ |
| 41 | 3.391 | 4.891 | 7.679 | $13.4 \%$ | 2.15 | 560 | \% 772 | 1300 |
| 42 | 3.398 | 4.359 | 7. 225 | 13.13 | 4.52 | E20 | 2.695 | 1380 |
| 43 | 4.259 | 5.147 | 7.980 | 13.68 | 0.33 | 683 | 2.545 | 1300 |
| 44 | 3.687 | 5.279 | 7.534 | 14.20 | 1.92 | 510 | 2.563 | 12月6 |
| 45 | 4.956 | 5. 564 | 3.514 | 14.33 | $3 \times 25$ | 56 | 2.509 | 12000 |
| 46 | 4.550 | 5.545 | 7.654 | 14.17 | 7.72 | 620 | 2.372 | 1290 |
| 47 | 3.563 | 5.762 | 8.376 | 15.98 | 2.01 | 475 | 2.346 | 1109 |
| 48 | 4.391 | 5.843 | 8.369 | 15.56 | 3.881 | 519 | 2.395 | 1108 |
| 49 | 4.831 | E. 012 | 8.334 | 15.45 | 7.65 | 560 | 2.198 | 1160 |
| 513 | 4.398 | 6.344 | 9.205 | 17.55 | E.12 | 4.36 | 2.133 | 1090 |
| 51 | 4.957 | E. 448 | 9.135 | 17.18 | 4.18 | 479 | 2. 1885 | 1090 |
| 52 | 5.380 | E.E1E | 9.159 | 17.01 | $7 \times 18$ | 516 | 1.996 | 16060 |
| 53 | 4.811 | 6. 968 | 11.12 | 17.35 | 2.96 | 336 | 1.942 | 910 |
| 5 | 5.426 | 7.995 | 10.64 | 16, 6 | 4.34 | 436 | 1.394 | 910 |
| 5.5 | 5.997 | 7.311 | 10.99 | 13.88 | 7.76 | 476 | 1.799 | 910 |
| 55 | 4.862 | 7.690 | 11.35 | 21.85 | 1.14 | 830 | 1. 75 | E2G |
| 5 | 5.511 | 7.758 | 11.20 | 21.23 | 2.51 | 360 | 1.743 | E26 |
| 5 | E.06E | 7.887 | 11.14 | 20. 96 | 4.54 | 396 | 1.702 | 820 |
| 59 | E. 771 | E. 169 | 11.23 | 24.73 | 8.44 | 435 | 1.602 | 820 |
| 8 | 5.252 | E. 494 | 12.43 | 23, 95 | 1.93 | 3619 | 1. 606 | 756 |
| $\underline{E}$ | 5.842 | 8.485 | 12.24 | 23.25 | 2.56 | 386 | 1.594 | 750 |
| 6 | 6.792 | 8.845 | 12.18 | 22.82 | 4.83 | 360 | 1.550 | 750 |
| 5 | 7.338 | 3.897 | 12.26 | 22.65 | 3.03 | 3'98 | 1.475 | 75 |
| 154 | 6.837 | 9.363 | 13.47 | 25.62 | 2.51 | 361 | 1.444 | 680 |
| 65 | 7.484 | 9.555 | 13.43 | $2{ }^{2} 5.13$ | 5.29 | 354 | 1.398 | 6.84 |
| EE | 8.254 | 9.896 | 13.57 | 25.60 | 8,93 | 360 | 1.317 | 650 |
| 5 | $7.21 \%$ | 10.25 | 1.4 .82 | 28.200 | 2.35 | \%76 | 1.325 | E200 |
| 53 | 8.131 | 10.48 | 14.73 | 27.57 | 5.10 | 36 | 1.2\% | Est |
| 63 | 9.169 | 16.89 | 14.98 | 27.43 | 9.22 | 350 | 1.195 | 620 |
| 7 | 7.818 | 11.32 | 16.45 | 31.37 | 2, 06 | 249 | 1.195 | 5609 |
| 71 | 9.021 | 1.1. 59 | 16. ${ }^{\text {E }}$ | 38.54 | 4.98 | 27 E | 1.153 | 56 |
| 72 | 16.16 | 12.54 | 16.52 | 36.38 | \% 18 | G601006 | 1. 1.73 | 560 |
| 3 | 3.659 | 12.44 | $1 \% .94$ | 34.35 | 2.17 | 226 | 1.887 | 510 |
| 14 | 9.ES6 | 12.65 | 17.91 | 33.67 | 4.22 | - 4 | 1. 163 | 515 |
| 7 | 9.824 | 13.48 | 1.9.E! | 37.45 | 1.94 | 2060 | 1.603 | $4 \%$ |
| TG | 16.964 | 13.71 | 13.44 | 36.57 | 4.36 | 2201 | 4.931 | 470 |
| 77 | 9.651 | 14.71 | 21.519 | 41.14 | 1.67 | 186 | 0.919 | 436 |
| 3 | 19.54 | 10.19 | 25.79 | 45.66 | 1.39 | 10.0 | 8.835 | 354 |



Figure 2. Lowpass tilter schematic diagram and attenuation response, inductive input and oulput.
Table 2. 50-Dhm 5-Element Chebyshev Lowpass Fitter Designs Using Standard-Value Capacitors, Inductive Input and Dutput. (Continued on page 126.)

| Filler No. | - - Frequency (MHz) - . . . |  |  | 50-dB | AC(\%) | $\begin{array}{r} \mathrm{L}, \mathrm{~L}, 5 \\ (\mu \mathrm{H}) \end{array}$ | $\begin{gathered} \mathrm{C}, \mathrm{C} 4 \\ (\mathrm{pF}) \end{gathered}$ | $\begin{aligned} & \mathrm{L} 3 \\ & (\mu \mathrm{H}) \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Cutott | $3-\mathrm{dB}$ | 20-dB |  |  |  |  |  |
| 1 | 9, 74 | 1.15 | 1.69 | 3.25 | 1. 32 | 5.6 | 4760 | 13.72 |
| 2 | B. 98 | 1.2E | 1.81. | 3.44 | " | 5 | 4300 | ) ${ }_{\text {¢ }} 6$ |
| 3 | 1. 0 | 1.38 | 1.94 | 3.64 | 4.60 | $5 \times 6$ | 3900 | 11.75 |
| 4 | 1.19 | 1. 47 | 2.85 | 3.82 | E.47 | 5.6 | 3680 | 11. 1.5 |
| 5 | 1.28 | 1. | E. ${ }^{\text {a }}$ | $4 \times 10$ | E.76 | 5 | 330 | $1 \mathrm{E}_{1} \mathrm{E}$ |
| $E$ | 0.91 | 1.39 | 2. 93 | 3.96 | 1.47 | 4.7 | 3040 | 11.58 |
| 7 | 1.08 | 1.56 | 2.16 | 4.18 | 2.71 | 4.7 | 5686 | 10.60 |
| 8 | 1. 2 | 1.63 | 2. 36 | 4, F | 4.42 | 4.7 | 3500 | 9.92 |
| 0 | 1.42 | 1.77 | 2.46 | 4.56 | 6.85 | 4.3 | 3016 | 9.32 |
| 18 | 1, E1 | 1.92 | 2.63 | 4.84 | 9.47 | 4.7 | 276 | 8.75 |
| 11 | 1. 8 c | 1. 44 | \% ${ }^{2}$ - 1 | 4.64 | 1.22 | 3.8 | 50 |  |
| 12 | 1.29 | 1.86 | $2 . E E$ | 4.93 | 2.64 | 3.9 | 3060 | 8.83 |
| 13 |  | 1.95 | 2.80 | 5.25 | 4.73 | 3.5 | 2760 | 8.15 |
| 14 | 1.8E | 2.19 | 3.8 | $5 \times 1$ | 7- " | 3.6 | 246 | 7.57 |
| 15 | 1.99 | 2.35 | 3.21 | 5.89 | 16.60 | 3.9 | 220000000 | 7.23 |
| 16 | 1. 34 | 2.00 | 2.98 | E.E1 | 1. 6.0 | 3.3 | 2708 | 7.89 |
| 17 | 1. 68 | $2 \times$ | -20 | B.03 | 3.69 | 3 y | 24 | 7.1.is |
| 18 | 1.92 | 2. 48 | 3.40 | 6, 34 | 5.59 | 3.3 | 2 Ec | 6.72 |
| 15 | 2.16 | 2.63 | 3.62 | E.69 | $7 \times 9$ | 3.3 | 2968 | 6.95 |
| 2 l | 2.43 | 2, 25 | $3.8{ }^{\text {\% }}$ | Pus | 160.8 | 3.3 | 180 |  |
| 21 | 1.60 | 2.46 | 3.59 | 8.87 | 1.72 | 2. ${ }^{\text {a }}$ | 2900 | 6.43 |
| 22 | 1. 99 | 己, For | 5.86 | $\overline{7} .29$ | 2.35 | 2, ${ }^{2}$ | $2 \mathrm{ED0}$ | 5.93 |
| e. | E. 4 | B. 9 | 4.15 | 7.75 | "-5\% | ※ッ" | 4 mby | 5.50 |
| 24 | 2.71 | 3.27 | 4.49 | E, 20 | 3.61 | 2.7 | 1608 | 5.13 |
| 25 | 2.92 | 3.44 | 4.68 | 8,58 | 1.80, 4. 4 | 2.7 | 1560 | 4.57 |

Table 2. 50-Ohm 5-Element Chebyshev Lowpass Filter Designs
Using Standard-Value Capacitors, Capacitive Input and Output. (Continued from Page 125.)

| FilteNo. | Frequency (MHz) . . . . |  |  | $50-\mathrm{dB}$ | RC <br> (\%) | $\begin{gathered} \text { L1, L5 } \\ (\mu \mathrm{H}) \end{gathered}$ | $\begin{gathered} \mathrm{C}, \mathrm{C} 4 \\ (\mathrm{pF}) \end{gathered}$ | $\begin{gathered} \text { L3 } \\ (\mu \mathrm{H}) \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Cutoff | $3-\mathrm{dB}$ | $20-\mathrm{dB}$ |  |  |  |  |  |
| 26 | 2.01 | 3.91 | 4.39 | E. 41 | 1.E6 | 2.2 | 1600 | 5.26 |
| 27 | $2 \times 2$ | 3.37 | 4.35 | 9.04 | 3.69 | cue | 1606 | 4,76 |
| 23 | 2.78 | 3. $\mathrm{EF}_{6} 7$ | - $\mathrm{B}_{2}$ | 9.38 | $5{ }_{5}{ }^{3}$ | c. | 15 yc | 4.5 |
| 29 | 3.34 | 4.82 | 5.5 | 16.18 | E.68 | 2.2 | 1300 | 4.18 |
| 5 | 3.65 | 4.28 | 5.88 | 10.63 | 10.96 | 2 z | 1290 | 4. 21 |
| 31 | E.35 | 3. ${ }^{1} 1$ | 5.29 | 16.16 | 1. 4.4 | 1.8 | 158 | 4.36 |
| 32 | 3.12 | 4.14 | 5.89 | 11.10 | 3.83 | 1.8 | 1300 | 3.88 |
| 3 | 3.51 | 4.45 | 8.2 | 11.E3 | 5.59 | 1. 8 | 1200 | 3.67 |
| 34 | 3.95 | 4.38 | 5.6 | 12. | Fn ${ }^{\text {a }}$ | 1. 8 | 1160 | 3.48 |
| 3 | 4.37 | 5 S | 7.18 | 12.86 | 11.44 | 1. 8 | 1009 | 3.31 |
| 36 | 3.10 | 4.51 | 6.56 | 12.51 | 2. 010 | 1.5 | 1200 | 3,51 |
| 57 | 3.65 | 4.96 | 6.95 | 18,20 | 3.52 | 1.5 | 12 l | \% 4 |
| 38 | 4.21 | 5.34 | $7 \times 4$ | 13.95 | 54 | 1. 5 | 1808 | 5, 国 |
| 39 | 4.75 | 5.73 | 7.96 | 14.71 | 7.97 | 1.5 | 910 | 2.89 |
| 48 | 5.34 | E.26 | 8. 50 | 15.57 | 1090 | 1.3 | 820 | 8.74 |
| 41. | 3, 5\% | 5.4 | $7 \times 4$ | 15.24 | 1.41 | 1. | 1 ELO | \% |
| 42 | 4.30 | 5.94 | 8.53 | 16.17 | 2.89 | 1.2 | 916 | 2.63 |
| 43 | 5.69 | 6.58 | 9.15 | 17.20 |  | 1.2 | 820 | 2.49 |
| 4, 4 | \% ${ }^{\text {\% }}$ | 7.14 | 9.75 | 13.09 | $7 \times 18$ | 1. 2 | P69 | 2.35 |
| 45 | E.420 | 7.62 | 10.39 | 19.69 | 9.87 | 1.2 | 660 | 2.23 |
| 4 | 4.48 | 6.60 | 9.65 | $18.4 \%$ | 1.63 | 1.8 | geg | 3.40 |
| 47 | 5. $5_{1} 7$ | F.eg | $1 \mathrm{I}_{1} 3$ | 19 | 8.89 | 1. 8 | 76 | cez |
| 48 | E. 15 | 7.87 | 1. 1.16 | 20.70 | 5.13 | 1.6 | 680 | 2.96 |
| 49 | 6.95 | 8.51 | 11.77 | 21.81 | 7.89 | 1.980 | 620 | 1.95 |
| E6 | 7.80 | 92 | 12.56 | 3, 95 | 10.21 | 1. ${ }^{\text {a }}$ | 5 | 1.85 |
| 5 | 5.23 | 7.96 | 11.6" | 2 m , c | 1.48 | 0.82 | 680 | 1.99 |
| 52 | 6, 35 | 8.72 | $12 \times 1$ | 2-76 | 2.95 | 6. 82 | 620 | 1.83 |
| 5 | 7. 4.5 | 9.58 | 13.45 | 25.18 | 5, 80 | ®, E | 56 | 1.76 |
| 54 |  | 1635 | 14.32 | 26.55 | 7.31 | *, \% | 510 | 1,60 |
| 55 | 3.28 | 11. | 15.18 | 27.7E | 9.54 | 0.82 | 476 | 1.53 |
| 56 | E. 41 | 9.66 | 14.418 | 27.10 | 1.57 | 6.68 | 56 | 1.84 |
| 57 | 7.75 | 10.59 | 15.16 | 28, ${ }^{2}$ | E, 8 | (1) 5 | 510 | 1. 51 |
| 5 | 8. 8 y | 11.41 | 18.09 | 30.15 | 4.76 | \%.68 | 470 | 1. 42 |
| 59 | 9.97 | 12.31 | 17.68 | 31.72 | $E .88$ | 0.63 | 430 | 1.34 |



Figure 3．Lowpass fitter schematic diagram and altenuation response，capacitive input and output．

Table 3．50－ahm 7－Element Chebyshev Lompass Filter Designs Using Standard－Value Capacitors，Capacitive Input and Output．

| Filter ．．－．．Frequency（MHz）－．－－ |  |  |  |  | $\begin{aligned} & \mathrm{RC} \\ & \text { (\%) } \end{aligned}$ | $\begin{gathered} \mathrm{C} 1, \mathrm{C} 7 \\ (\mathrm{pF}) \end{gathered}$ | $\begin{gathered} L_{2}, L_{6} \\ (\mu \mathrm{H}) \end{gathered}$ | $\begin{gathered} \mathrm{C} 3, \mathrm{C} 5 \\ (\mathrm{pF}) \end{gathered}$ | $\begin{aligned} & 14 \\ & (\mu-H) \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| No． | Cutof | $3-\mathrm{dB}$ | 20－dB | $50-\mathrm{dB}$ |  |  |  |  |  |
| 1 | 1.097 | 1．15\％ | 1.401 |  | 6． 63 | 2760 | 10.96 | 5646 | 12.57 |
| 2 | 1． 1.47 | 1．229 | 1.511 | 2.250 | 3．4．1 | 2200 | 10.89 | 5100 | 12.29 |
| 3 | 1．119 | 1．2E4 | 1． $53 \%$ | 2． 298 | 5.7 | 240 | $11_{1} 194$ | 51.00 | 11．65 |
| 4 | 1．033 | 1．29\％ | 1．63\％ | 2.456 | 1．4．4 | 150\％ | 9.518 | 4760 | 11.83 |
| 5 | 1.124 | 1．32\％ | 1．E3\％ | 2.455 | \％．12 | 200 ${ }^{\text {cta }}$ | 9.502 | 476 | 11.40 |
| 5 | 1．298 | 1．36\％ | 1．E58 | 2．4．4 | 5.50 | 2200 | 7.276 | 47 BE | 10.78 |
| $\vec{i}$ | 1．2．78 | 1．423 | 1． 297 | 2．47＇ | 9.617 | 2446 | 8.824 | 47 mb | 10.01. |
| 8 | 1.161 | 1．412 | 1．785 | 2．731 | 1．16 | 160 | 9.681 | 4960 | 10．97 |
| 9 | 1.214 | 1.448 | 1.788 | 2.637 | 2.8 | 1809 | 8.769 | 43901 | 16.51 |
| 16 | 1.314 | 1.493 | 1.510 | 2.677 | 5.46 | 26193 | 8，562 | 4306 | 9.916 |
| 11 | 1．417 | 1.556 | 1． 657 | 2．305 | 9.17 | 2260 | 8． 8151 | 75040 | 9.138 |
| 92 | 1． 2 200 | $1.56{ }^{\circ}$ | 1． 367 | 2． 994 | 1．51 |  | T．901 | 3515 | 9.846 |
| 13 | 1．318 | 1.593 | 1． 279 | 2． 36 | 2． 4.4 | 16 | 7．91近 | 396 | 9.617 |
| 14 | 1.446 | 1.641 | 1.993 | 2．951 | 5．16． | 1569 | 7.733 | 3900 | 9.035 |
| 15 | 1．565 | 1.718 | 2． 049 | 2.484 | 9，28 | 2695 | 7.298 | 3966 | E． 268 |
| 16 | $1 \times 445$ | 1．72も | 2．135 | $3 \times 210$ | 2.71 | 15 L | 7．294 | 5608 | 8．817 |
| $1{ }^{\prime}$ | 1．5．7 | 1．730 | 2．1．48 | 3.197 | 4.11 | 16 ar | 7.219 | 3615 | $8.5{ }^{3}$ |
| 15 | 1．664 | 1.837 | 2． 201 | 3．213 | 8.10 | 1806 | 2． 260 | 3e0a | 7． 885 |
| 19 | 1．567 | 1.806 | 2.325 | 3． 5 20 | 1.82 | 13 n 4 | $6 . E 94$ | 35139 | S．265 |
| 26 | 1.682 | 1.929 | 2.350 | 3．43i | 4.71 | 1．5906 | 8， 577 | 3\％ | 7．721 |
| 21 | 1． 767 | $10_{0} 9$ | 2．38\％ | 3． $49{ }^{\text {\％}}$ |  | 1 Emb | 6.45 | कंE16 | i－370 |
| 2 | 1．596 | 2． $\mathrm{B}_{2} \mathrm{O}$ | 2． 560 | 3． 925 | 1．52 | 1120 | 5.043 | \％ 6 164 | 7.082 |
| $\bigcirc$ | 1.659 | 2．053 | 2．55 | 3.87 | 2.64 | 1200 | 6.088 | 3610 | 7.472 |
| 24 | 1．760 | ¢，H\％\％ | 2.576 | 3.841 | 3.51 | 1369 | 6．변을 | 3 Sty | 7.213 |
| Et | 1.303 | 2.245 | 2． 641 | 3．862 | 3.16 | 1.5197 | S． $71 . \mathrm{E}$ | \％ | E．52z |
| 2 | 1．34 | 2.248 | 2． 5.4 | 4.35 | 1． 1.1 |  | 5.447 | 2\％＇00 | 6.394 |
| 27 | 1．853 | 2.289 | 2． $4+4$ | 4.371 | 2.32 |  | 5.437 | 2769 | 6.577 |
| 23 | 2． 422 | E． 341 | 2．963 | 4．203 | 4.11 | 1200 | 5．414 | 2309 | 5.418 |
| 2 | 2．14\％ | 2.409 | 2.064 | 4．ごア | 6.58 | 13010 | 5.358 | 2？ | E． 0164 |
| \％ | E． 6 | 2.59 | 3． 198 | $4 \mathrm{3} \%$ | 1.35 | 915 | ＋．350 | 24010 | E， 05 |
| 31 | 2.160 | 2.523 | 3.213 | 4． 515 | 2.71 | 1.5198 | 4.358 | ट4 ${ }^{\text {a }}$ | 5.875 |
| － | 2.325 | 2.60 | 3.255 | 4．7－5 | 4.95 | 116 | 4.750 | 2490 | 5.556 |
| 3 | 2． 4.31 | 2． 756 | 3.341 | 4 ACz | 8.15 | 1200 | 4． 4.3 | 2466 | 5.217 |
| 34 | 2．1吅家 | 2， $\mathrm{F}_{6}$ | 3．4．96 | 5 | i． 17 \％ | 826 | 4.442 | ど19 | 5.667 |
| 35 | 2． 31 | 2.819 | E，嵒灾 | （12） | 二．50 | 910 | 4.460 | 229010 | 5．40t |
| 3 | E．5－24 | 2.894 | 3.5 | ¢，\％ | 4.71 | 1969 | 4． 464 | 2－5 | 5.147 |
| ¿＂ | 2．717 | 3.6415 | 3．601 | 5.208 | 8． 16 | 1161 | 4.192 | 220］ | 4．782 |

Table 3．50－ohm 7－Element Chebyshev Lowpass Filter Designs
Using Standard－Value Capacitors，Capacitive Input and Output．（Continued from Page 127．）

| Fiiter－．．．Frequency（ MHz ）－．－－ |  |  |  |  |  | C1，C7 | L2，L6 | C3，CS |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| No． | Cutofi | 3－6B | 20－dB | 50－dB | （\％） | （pF） | （ $\mu \mathrm{H}$ ） | （pF） | $(\mu H)$ |
| 3 | 2.384 | 3.8141 | 3.838 | 5．853 | 1．24 | \％ | 4.1041 | 261919 | 5.689 |
| 59 | 2．568 | 3.044 | 3． 640 | 5． 733 | 2.45 | 6er | 4.056 | 2060 | 4.933 |
| 45 | 2．78 | 3.134 | 3.878 | 5.753 | 4.74 | 916 | 3.985 | 2965 | 4.675 |
| 41 | 2.989 | 3．307 | 3．9E1 | 5.792 | 5.19 | 106\％ | 3． 811 | 2 3 5 | 4.348 |
| 42 | 2．606 | 3.353 | 4.264 | E． 507 | 1．31 | 85090 | 3.646 | 18919 | 4.596 |
| 43 | 2.883 | 3.451 | ＋．2．1 | 6.421 | 2.71 | 75 | 3.647 | 1805 | 4.469 |
| 44 | 3.1090 | 3.899 | 4． 319 | c． 33 | 4．78 | 820 | 3.585 | 1890 | 4.205 |
| 45 | 3.351 | 3．695 | 4.417 | 5．44： | 8.80 | 519 | 3.464 | 1580 | 3.851 |
| 46 | 1．06E | 3.823 | 4.795 | P． 290 | 1． 61 | E\％C | 3.243 | $16.6{ }^{\text {a }}$ | $4 \times 8$ |
| $4 ?$ | 3.306 | 3.902 | 4.811 | P．211 | 3.95 | 8 | 3.235 | 1650 | 3.8104 |
| 48 | 3.552 | 4.022 | 4.873 | $\overrightarrow{-196}$ | 5.65 | 756 | 3.154 | 1690 | 3.667 |
| 49 | 3.814 | 4.185 | $4 \times 992$ | ？，272 | 9.85 | E29 | 2.995 | 1500 | 3.394 |
| 59 | 3.166 | 4.551 | 5.118 | P－824 | 1.19 | 56 | 3.829 | 1500 | 3.821 |
| 51 | 3.445 | 4.133 | 5.122 | $\cdots 711$ | 2．5\％ | 5， | 3．041 | 1500 | 3．687 |
| 52 | 3.694 | 4.240 | 5.168 | 3.671 | 4.64 | 63.4 | 2.992 | 1566 | 3.515 |
| 5 | 3.985 | 4.499 | 5.282 | 7.723 | 8．10 | 75 | 2.358 | 1509 | 3.261 |
| 54 | 2.813 | 4.717 | 5．902 | 8.955 | 1．76 | 514 | 2．E36 | 1300 | 3.269 |
| 55 | 4.183 | 4.819 | 5.927 | $8.86 ?$ | 3.39 | $5 E 10$ | 2.623 | 1300 | 3.155 |
| 56 | 4.423 | 4.783 | 5.619 | 8.665 | 6.23 | 520 | 2.543 | 1390 | 2.941 |
| 57 | 4.125 | 5． 108 | 6． 394 | 9.764 | 1.74 | 471 | 2.433 | 1299 | ＊．511 |
| 58 | 4.400 | 5.202 | 6.414 | 9.615 | 3.15 | 515 | 2.426 | 1206 | 2.913 |
| 59 | 4.719 | 5.354 | 6.491 | 5.59 | 5．5010 | 560 | 2．36 | 1260 | 2．759 |
| 60 | 5.129 | 5.606 | E．E．7 | 3.313 | 9.85 | 520 | 2.233 | 12 c | 2．5．24 |
| 61 | 4.493 | 5．579 | 6.975 | 18.59 | 1．72 | 431 | 2.839 | 1109 | 2.762 |
| 62 | 4.819 | 5.683 | 7.000 | 10.48 | 3.24 | 476 | 2.222 | 1109 | 2， 653 |
| 63 | $5.12 \%$ | 5.827 | 7．0．3 | 10.46 | 5.8 | 514 | －${ }^{\text {app }}$ | 11 m | 2． 540 |
| 84 | 5．516 | 6.067 | 7．24 | 16．5 | 9．${ }^{\text {a }}$ | 569 | \％．00．3 | 11 1900 | 2． 349 |
| 6.5 | 4.933 | E． 125 | 7.673 | 11.65 | 1.69 | 390 | 2.07 | 1495 | 2.513 |
| EG | 5.82 E | E．262 | 7．704 | 11.58 | 3.34 | 430 | 2．019 | 1409 | 2.415 |
| 67 | 5.654 | E－442 | $\bar{i}=\operatorname{Bic}_{6} 1$ | 11.52 | $5.3,3$ | 471 | 1．565 | 160000 | 2.267 |
| 58 | 6.677 | E．680 | 7．974 | 11.62 | 9.91 | 510 | 1．8\％ | 1040 | 2， 132 |
| 59 | 5.485 | $5.74 \%$ | 8.432 | 12.78 | 1.88 | 360 | $1.34 \%$ | 919 | 2．275 |
| 7 | 5.055 | 6.875 | 8.454 | 12.57 | 3.27 | 390 | 1.837 | 914 | 2．200 |
| 71 | 8.283 | $\because .993$ | B．Ed | 12.65 | 5.91 | 480 | 1．73＇ | 915 | $2 \times 9$ |
| 72 | E．750 | 3.391 | 8.893 | 12.81 | 9.84 | 48 | 1.593 | 916 | 1.914 |
| 73 | 5.682 | － 387 | 9.368 | 14.37 | 1.00 | उपй | 1.651 | 324 | E． 161 |
| 74 | 5.172 | 7.515 | 9.851 | 14.15 | 2.13 | 330 | 1．5E4 | 826 | z．937 |
| T 5 | 8.597 | 7.681 | 9.415 | 14.34 | 3.81 | Fint | 1．6．4．7 | 82 | 1． 259 |
| 76 | B． 307 | 3.895 | 9.536 | 14.05 | 6.14 | 39 | 1.506 | 520 | 1.859 |
| $\vec{i}$ | 5.715 | 8.208 | 10.23 | 15.45 | 2.64 | $3{ }^{3}$ | 1.522 | 750 | 1.363 |
| 3 | $\cdots 225$ | 8.403 | 16． 30 | 15.35 | 3.56 | 330 | 1.507 | P50 | 1．788 |
| 7 | 7． 716 | 8． 660 | 16．45 | 15．37 | 6.46 | 360 | 1．46 | 750 | 1．68E |
| द0 | B．2．3 | －5， 618 | 10．？ 1 | 15，515 | 9.5 | 30 | 1．337 | 756 | 1． 5.5 |
| 81 | 7.362 | 7.159 | 11.29 | 17．0 | 1.35 | 270 | 1.379 | －86 | 1．693 |
| E2 | 7．935 | 4.275 | 11.36 | 16.93 | 3.93 | 3619 | 1.366 | 583 | 1．6．19 |
| E2 | 5.583 | 3.595 | 11． 5 | 16． | E．EA＇ | 334 | 1.318 | E80 | 1． 517 |
| E4 | 亿゙＂565 | 7．865 | 12．3 | 16．32 | 1． 5 | 245 | 1．256 | 520 | 1.0152 |
| BE | 8． 53 | 18.13 | 12．44 | 18．5E | 3.62 | 270 | 1.248 | E20 | 1．48E |
| 56 | 9.392 | 11． 51 | 12．88 | 18．61 | 6.76 | 301 | 1． 204 | E20 | 1．307 |
| 87 | 8． 56 | 10．95 | 1．3： | 2．${ }^{\text {2 }}$ | 1．7\％ | 220 | 1．135 | 560 | 1．403 |
| 58 | 9.467 | 11．17 | 13．${ }^{5}$ | 261． $5 \%$ | 2.27 | 240 | 1： 12 l | 5 | 1.953 |
| 87 | 16．37 | 11．EE | 14．${ }^{10}$ | 20．50 | 5.63 | 「30 | 1．0．3 | 56.6 | 1.256 |
| 96 | 4.717 | 12．92 | 15．614 | 22．33 | 1．76 | 2 Ca | 1． 1.94 | 515 | 1.279 |
| 9 | 10.47 | 12.23 | 15.11 | 22． 00 | 8.41 | 226 | 1.629 | 510 | 1． 1．$^{\text {cos }}$ |
| $9{ }^{\circ}$ | 19．3\％ | $12.9 \%$ | 15，3\％ | 24.50 | 1．46 | 184 | W． 5.5 | 4 | 1． 1.35 |



Figure 4. Lowpass filter schematic diagram and attenuation response, inductive input and output.

Table 4. 50 -ohm 7 -Element Chebyshev Lowpass Filter Designs Using Standard-Value Capacitors, Indutive Input and Oulput.

| Filter No. | . Frequency (MHz) |  | $20 \cdot \mathrm{~dB}$ | 50.dB | RC <br> (\%) | $\begin{array}{r} \mathrm{L1}, \mathrm{~L} \mathbf{7} \\ (\mu \mathrm{H}) \end{array}$ | $\begin{gathered} \mathrm{C}, \mathrm{C6} \\ (\mathrm{pF}) \end{gathered}$ | $\begin{gathered} \text { L3. L. } \\ (\mu \mathrm{H}) \end{gathered}$ | $\begin{aligned} & \mathrm{C} 4 \\ & (\mathrm{pF}) \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Cutof | 3-dB |  |  |  |  |  |  |  |
| 1 | 1.014 | 1.179 | 1.444 | 2.15 | 3.85 | 5.896 | 4308 | 13.37 | 5100 |
| 2 | 1.067 | 1.293 | 1.5\%7 | 2.355 | 2.88 | 5.962 | 3960 | 12.64 | 4790 |
| 3 | 1.197 | 1.405 | 1. 728 | 2.584 | 3.41 | 4, in 16 | 3609 | 11.15 | 4300 |
| 4 | 1,5\% | 1.53? | 1.879 | 2.797 | 4.16 | 4.51 | 3300 | 16.29 | 3969 |
| 5 | 1.425 | 1.683 | 2.075 | 3.116 | 3.12 | 3.947 | 38610 | 3.274 | 3690 |
| 6 | 1.528 | 1.855 | 2.368 | 3.48E | 2,21 | 3.85 | 2769 | 8.315 | 3300 |
| $\overline{7}$ | 1.534 | $2.05 \%$ | 2. 589 | 3.945 | 1.43 | 2, w | -480 | 7.408 | 3000 |
| 8 | 1.853 | 2.271 | 2.352 | 4.284 | 2, 94 | 2, 110 | 2204 | 6.775 | 2700 |
| 9 | 2,137 | 2.525 | 3.113 | 4.665 | 3,12 | 2.831 | 2000 | 6.182 | 2400 |
| 16 | 2.291 | 2.782 | 3.462 | 5. 2 z | 2, 21 | 2, 242 | 1590 | 5.544 | 2200 |
| 11 | 2.452 | 3.988 | 3.884 | 5.918 | 1.43 | 1.85 | 1600 | 4.939 | 2000 |
| 12 | 2.849 | 3.367 | 4.150 | 6.219 | 3.12 | 1.973 | 1500 | 4.637 | 1800 |
| 13 | 3.126 | 3.838 | 4.791 | 7.256 | 1.93 | 1.589 | 1369 | 4.654 | 1600 |
| 14 | 3.259 | 4.117 | 5.175 | 7.856 | 1.4 4 | 1.414 | 1264 | 3.704 | 1500 |
| 15 | 3.475 | 3.897 | 4.751 | 6.915 | 6.55 | 2.004 | 18.8 | 4.169 | 1509 |
| 15 | 3.985 | 4.616 | 5.637 | 8.396 | 4.16 | 1.527 | 1100 | 3.429 | 1390 |
| 17 | 4.274 | 5.6150 | 6.255 | 9.32 | 3.12 | 1.315 | 1096 | 3.691 | 1208 |
| 18 | 4.633 | 5.533 | 6.348 | 10.25 | 2.72 | 1.170 | 910 | 2.80? | 1109 |
| 19 | 5.95 | E. 115 | ?.604 | 11.47 | 2. 30 | 1.827 | 820 | 2.525 | 1090 |
| 26 | 5.581 | E.762 | 8. 36 | 12.51 | 2.5 | 6. 95 | 750 | 2. 311 | 910 |
| 21 | E. 229 | 7.412 | 9.160 | 13.7E | 2.65 | 6. 8.80 | 680 | 2.695 | 820 |
| 22 | 6. 791 | 8.119 | 19.0.5 | 15.11 | 2.68 | 0.795 | 629 | 1.912 | 750 |
| 23 | 7.453 | 8.973 | 11.13 | 16.76 | 2.54 | 6. 716 | 560 | 1.725 | 680 |
| 24 | E. 176 | 9.347 | 12.22 | 16.41 | 2.44 | 6. 6.44 | 516 | 1. 5171 | 629 |
| 2 S | 9.207 | 19.77 | 13.23 | 19.76 | 3.57 | 0.633 | 476 | 1.457 | 56.1 |
| 26 | 10.14 | 11.79 | 14.44 | 21.52 | 3.89 | 0.589 | 436 | 1.327 | 510 |
| \% ${ }^{\text {r }}$ | 16.87 | 12.93 | 15.97 | 23.98 | 2.80 | 6. 506 | 396 | 1. 200 | 470 |



Figure 5．50－ohm 5th－degree elliptic lowpass filter designs using standard－value capacitors for $\mathrm{Cl}, \mathrm{C} 3$ ，and C 5 ．

Table 5A．50－ohm 5th－Degree Elliptic Lowpass Filter Designs Using Standard－Value Capacitars，Capacitive Inpat and Output．

| Filter No． | F－CO | F－3dB <br> （MHz） | $F-A_{S}$ | $\begin{aligned} & A_{s} \\ & (d B) \end{aligned}$ | RC <br> （\％） | $\mathrm{Cl}$ | C3 | $\begin{array}{r} \mathrm{C5} \\ -(\mathrm{pF}) \end{array}$ | C2 | C4 | $\begin{gathered} \llcorner 2 \quad L 4 \\ \cdots(\mu H)-- \end{gathered}$ | $\begin{aligned} & \mathrm{F} 2 \\ & \cdots(\mathrm{MHz} \end{aligned}$ | F4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 8．86 | 0.59 | 1．5．7 | ＋1．4 | 4.45 | 2764 | 5606 | こども | 24 | 987 | 12.110 .1 | 2.54 | 1．64 |
| 2 | 0.93 | 1． 0.9 | 1．8？ |  | $\cdots 16$ | 3\％园家 | 5 | 20 | W5 | ＇60 | 1 19．6 8．74 | 2．ET | 1．0゙4 |
| 3 | 1.06 | 1．20 | 1.77 | ＋6． | 16．5 | \％r＇er | 470 | 22 ${ }^{\text {20 }}$ | 341 | 98． | 9．56．56 | 6．8． | 1．45 |
| 4 | 1.23 | 1.35 | 1．92 | 45.8 | 15.3 | 2700 | 43015 | 2200 | 352 | 1616 | 7.93 －． 2.7 | 3． 12 | 2.00 |
| 5 | 1.47 | 1．57 | 2．15 | $+5.4$ | ここ．＇ア |  | 3006 | E2914 | $35^{\circ} 4$ | 10.45 | E． 324.82 | 3，32 | 2.33 |
| $E$ | －1．87 | 1．1． 10 | 1183 | 48.7 | 3，${ }^{2}$ | 2490 |  | 20］ | ＂57 | \％${ }^{3}$ | 11．6941 | 2．${ }^{4}$ | 1．911 |
| 7 | 1.46 | 1．20 | 1.93 | 45.2 | C． 014 | 2466 | 4．795 | 2009 | 262 | 746 | 9.918 .36 | 3． 1.6 | 2．191 |
| E | 1.16 | 1.33 | 2． 20. | 4\％， 6 | $\because 37$ | 24日 4 | 4306 | Eด9 | 209 | 765 | 8．67 7.19 | 3．36 | 2,15 |
| 9 | 1． E \％ | 1．51 | 2．25 | 48． 1 | 14.5 | S4里可 |  | 2 100 | 276 | 785 | 7．25 5．06 | 3，55 | 2． 84 |
| 10 | 1.8 | 1.50 | 2．16 | 61.5 | 16．6 | 2200 | 3－40 | 2014 | 189 | 255 | 75.5 | 5.89 | 3.24 |
| 11 | 1．50 | 1．71 | ご列 | 47.3 |  | 2416 | 3638 | 2015 | 24 |  | Ent 4 BE | －1．84 | 2．55 |
| 12 | 1．82 | 1.30 | 3， 3 | 61.3 | 15．6 | 22018 | 36.901 | O6n | 152 | 0 | 6．36 5． 59 | 5.49 | 3.52 |
| 13 | 0.93 | 1．18 | L． $\mathrm{V}^{\text {d }}$ | 48．6 | 3， $\mathrm{r}^{1}$ | 2200 | $4+15$ | 1868 | 257 | 743 | 16．2 2.5 | 1．11 | 1.99 |
| 14 | 1． 18 | 1．sb | 2，可 | 47.3 | 6.05 | 2265 | 4，\％ | 1860 | 2e？ | 759 | 9．4＇8 7.8 | 3．25 | 2．19 |
| 15 | 1.27 | 1.45 | 2.17 | 4 EF .7 | Y．E5 | 2209 | 3904 | 18 tas | 271 | 779 | 7.356 .39 | 3.45 | 2.20 |
| 16 | 1.45 | 1，E1 | 2.32 | 46.3 | 13.3 | 2 zat | 3ent | 1806 | 275 | $\checkmark$ | 5．86 5． 44 | 3.86 | 2.42 |
| $1 \overline{8}$ | 1．47 | 1．70 | 3． 29 | 5 | 9， | 26］ $0^{6}$ | 3 Smb | 180日 | 186 | 351 | 7．177 6． 23 | 5． 34 | 3.35 |
| 1.5 | 1.65 | 1． 5.2 | 2．54 | 45． | 19.7 | 2eण | Fible | 1． 890 | 287 | \＄2． | 5．54 4．42 | 3.95 | 2． 6.4 |
| 19 | 1．$\quad 3$ | 1.93 | 3． 49 | 59.2 | 15.1 | 21948 | 30， | 150 | 132 | 3EE | 5.94 E．2F | 5.000 | 5．6．4 |
| 20 | 1． 1.15 | $1.2 ?$ | 2． 614 | 本里1 | 2． 5 | \％46 | 436 | 1504 | 258 | P¢， | 7，35 i．76 | 3.24 | 2.98 |
| 21 | 1．15 | 1.41 | 2． 12 | 45.4 | E．${ }^{\text {a }}$ |  | 3996 | 1606 | 265 | 771 | 8．276．73 | 3.40 | 2.21 |
| 3 | 1.34 | 1.54 | 2.24 | 44.8 | 3.89 | ？प165 | 3 EgT | 1699 | 272 | 790 | 7．86 8.89 | 2，56 | 2.33 |
| 23 | 1．55 | 1.71 | 2． 41 | 41． 3 | 12－1 | 20415 | 3岳或 | 16 BL | 289 | 312 | 6.354 .95 | 3.18 | 2.501 |
| 24 | 1．56 | 1.82 | 3.32 | 57.3 | 3.91 | 18046 | 33 y | 16.6 | 135 | 360 | E．815．85 | 5.42 | 3.47 |
| 25 | 1．82 | 1.95 | $\underline{2} \times 5$ | 43.8 | 12.1 | 2．9以 | Sn边 | 165 | 2Ч以 | 841 | 5.213 .75 | 4.69 | 2．75 |
| 26 | 1.85 | 2.08 | 3．62 | 59 | 14.1 | 1504 | 3 3018 | 1606 | 136 | 366 | 5.524 .83 | 5.88 | 3.79 |


| Filter <br> No． | F－CO | F－3 dB $-(\mathrm{MHz})-$ | $F-A_{S}$ | $A_{s}$ （dB） | RC <br> （\％） | C¢ | C3 | C5 | C2 | C4 | 12 | $\begin{gathered} \mathrm{L} 4 \\ (\mu \mathrm{H})- \end{gathered}$ |  | $\begin{gathered} \text { F4 } \\ H z)-\cdots \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 27 | 1.12 | 1.44 | 2． 41 | 47.5 | 3.42 | 18อ\％ | 3961 | 1535 | 192 | 545 | 8.45 | 7.25 | 3.95 | 2.52 |
| 28 | 1.28 | 1.56 | 2.55 | 49.3 | 5.41 | 1840 | 3696 | 1564 | 196 | 558 | 7.65 | 6.47 | 4.11 | 2.65 |
| 29 | 1.47 | 1.73 | 2， 79 | 48.6 | 8． 40 | 18010 | 33610 | 1560 | 200 | 576 | 6．75 | 5.62 | 4.35 | 2． 31 |
| 36 | 1.75 | 1．95 | 2．9E | 48.2 | 12． | 1806 | 3090 | 1560 | 20E | 585 | 5.72 | 4．68 | 4.64 | 3.64 |
| 31 | 2.11 | 2.27 | 3.27 | 47.8 | 20． | 1851 | 2760 | 1503 | 213 | 694 | 4.55 | 3.64 | 5.12 | 3.49 |
| 32 | 1．15 | 1.54 | 2．51 | 47.7 | 2．70 | 1686 | 3600 | 1306 | 191 | 553 | 7.96 | 6.65 | 4.11 | 2.63 |
| 33 | 1．35 | 1．68 | 2.64 | 47.1 | 4．5．5 | 1604 | 3）${ }^{606}$ | 1364 | 195 | 564 | 7.10 | 5.92 | 4.23 | 2．75 |
| 34 | 1.56 | 1.86 | 2.31 | 46.4 | 7． 41 | 1609 | 3069 | 1306 | 2 B | 578 | 6． 24 | 5.11 | 4.50 | 2.93 |
| 35 | 1.57 | 1.93 | 3．409 | 53.9 | 5.51 | 156 | 36331 | 1360 | 129 | 362 | 6.33 | 5.54 | 5.57 | 3.55 |
| 36 | 1．83 | 2． 11 | 3． | $4{ }^{4} \mathrm{E} .8$ | 12， | 18104 | 2709 | 1360 | 207 | 596 | 5.26 | 4.21 | 4.82 | 3.10 |
| 37 | 1.89 | 2.19 | 3．63 | 59.3 | 9． 56 | 1560 | 2706 | 1306 | 132 | 369 | 5.39 | 4.65 | 5.96 | 3.84 |
| 38 | 2.31 | 2.48 | 3.44 | 45.3 | 15.5 | 1660 | 2460 | 1396 | 216 | 620 | 4.12 | $3 . \overline{21}$ | 5.33 | 3.57 |
| 39 | 2.35 | 2.58 | 4.12 | 52.9 | 16． | 15610 | 2400 | 1300 | 136 | 379 | 4.28 | 3．62 | 6.59 | 4.30 |
| 46 | 1．28 | 1．EE | 2．E3 | $4 E .3$ | 3.11 | 1500 | 3080 | 1200 | 192 | 561 | 7.29 | 6.96 | 4.28 | 2.74 |
| 41 | 1.51 | 1.83 | 2，78 | 45.6 | 5.33 | 1569 | 3069 | 1260 | 197 | 574 | 6.42 | 5.25 | 4.47 | 2.90 |
| 42 | 1.75 | 2.05 | 2．93 | 44．3 | 9.85 | 1506 | 2760 | 12 O | 264 | 592 | 5.52 | 4.42 | 4.75 | 3.11 |
| 43 | 2.17 | 2.89 | 2． 31 | 44.2 | 14．7＇ | 1508 | 2414 | 1200 | 212 | 616 | 4.49 | 3.49 | 5.16 | 3.43 |
| 44 | e． 5 | 2.75 | 3．63 | 43.8 | 20．8 | 1596 | 2200 | 1200 | 220 | 536 | 3.71 | 2.82 | 5.58 | 3.76 |
| 45 | 1．68 | 2.10 | 3.56 | 51.2 | 4.41 | 1360 | 2769 | 1igb | 129 | 365 | 5.79 | 4.99 | 5.83 | 3.73 |
| 46 | 2.05 | 2.40 | $88^{3}$ | 56． 5 | 8．2 | 1301 |  | 1100 | 133 | 375 | 4.90 | 4.15 | E． 24 | 4.04 |
| 47 | 2.39 | 2.66 | 4.16 | 50.0 | 12．3 | 1341 | 2254 | 1109 | 136 | 383 | 4．22 | 3.52 | 6.65 | 4.34 |
| 48 | 2.84 | 3． 58 | 4.65 | 47.7 | 18.6 | 1364 | 2065 | 1196 | 149 | 39＊ | 3.45 | 2.82 | 7.26 | 4.78 |
| 49 | 1． 56 | 2． 0.18 | 2.55 | 50.1 | 206 | 12001 | 2790 | 1090 | 127 | 363 | 5.88 | 5.37 | 5．83 | 3.71 |
| 50 | 1.92 | 2.35 | 3.50 | 49.3 | 5.41 | 1289 | 2469 | 1506 | 134 | 372 | 5.10 | 4.32 | 6.17 | 3.97 |
| 51 | 2.23 | 2.59 | 4． 14 | 48.8 | 3．4星 | 1294 | 2264 | 1 ECa | 133 | 369 | 4.50 | 3.75 | 6.50 | 4.22 |
| 52 | 2．62 | 2.92 | 4.35 | 48.2 | 13，${ }^{3}$ | 12 Q | 2014 | 1640 | 137 | 390 | 3.81 | 3.12 | 6.95 | 4．5E |
| 53 | 3.24 | 3．Ex | 6.74 | 51.3 | 16．0 | 11010 | गE60 | 16104 | 6.5 .9 | 180 | 3.13 | 2.65 | 11．6 | 7． 64 |
| 54 | 3.17 | 3.41 | 4.90 | 47.8 | 20.2 | 1200 | 18619 | 166 | 142 | 492 | 3.63 | 2.42 | 7.68 | 5.10 |
| 55 | 1.69 | 2， 3 | 8.87 | 49.1 | 3.27 | 116 | 2409 | 910 | 121 |  | 5.21 | 4.45 | 6.33 |  |
| 56 | 2． 89 | E．55 | 4.87 | 48.5 | 5， 39 | 1106 | 2209 | 510 | 124 | 355 | 4.68 | 3.94 | 6.59 | 4.25 |
| 57 | 2.45 | 2.84 | $4.3 E$ | 48.6 | E， 69 | 11561 | 2006 | 910 | 127 | 364 | 4.86 | 3.37 | 6.99 | 4.54 |
| 58 | 2.92 | 3.25 | 4.7 ？ | 47.4 | 13.3 | 1100 | 1560 | 910 | 131 | 375 | 3.38 | 2.74 | 7.55 | 4.97 |
| 59 | 3.64 | 3.68 | $5 \times 45$ | 474 | 2心． | 110 | 1608 | 910 | 137 | 369 | 2.58 | 2.64 | Q．4E | 5.65 |
| 89 | 1，94 | 2．52 | 4.15 | 43.4 | 3.11 | 16 ECG | 2066 | 326 | 115 | $3 \overline{1}$ | 4.79 | 4． 06 | 6.78 | 4.34 |
| E1 | 2.29 | 2.75 | 4.35 | $4 \vec{i}$ ， | 5． 3 | 166日 | 2以10 | 826 | 118 | 359 | 4.2 E | 3.56 | 7.10 | 4.58 |
| 52 | 2.73 | 3.14 | 4.73 | 47.8 | 3．85 | 1996 | 1． E ¢ 6 园 | 326 | 121 | 348 | 3.65 | 2.99 | 7.56 | 4.93 |
| 63 | 3.33 | 3.65 | 5.25 | $4 E .4$ | 15.2 | 16 lal | 10015 | 829 | 126 | 361 | 2.95 | 2.36 | 5.25 | 5.46 |
| 64 | 3.37 | 3.87 | 7.23 | 59.6 | 11.2 | 916 | 1690 | 829 | 58． 3 | 1E1 | 3．68 | 2.75 | 11.8 | 7． 55 |
| 65 | 3.73 | 4.92 | 5． 53 | $4 E 2$ | 19．7 | 19 yc | 1504 | 824 | 129 | 368 | 2.56 | 2.61 | 8， 76 | 5.85 |
| Es | 3.82 | 4.26 | 7.72 | 59.5 | 15.2 | 910 | 1560 | \＄29 | 59.6 | 163 | 2.70 | 2.39 | 12．6 | 8.07 |
| 87 | 2.14 | $2.39^{*}$ | 4.61 | 48.8 | 3.13 | 910 | 264 | 75 | 142 |  | 4.35 | 3.71 | 7.55 | 4.52 |
| 68 | 2，57 | 3.11 | 4.92 | 48.1 | 5.71 | 915 | 136或 | 756 | 105 | 301 | 3.82 | 3.19 | 7.95 | 5.13 |
| 69 | 3．13 | 3.55 | 5.36 | 47.4 | 1．1． 1 | 910 | J． 6819 | 759 | 108 | 310 | 3.29 | 2.62 | 8.55 | 5.59 |
| 70 | 3.49 | 3.87 | 5.68 | 47.1 | 13.4 | 916 | 15.518 | 750 | 111 | 316 | 2.84 | 2.36 | 8.97 | 5.71 |
| 71 | 4.53 | 4.81 | E．6\％ | 46.5 | 24.1 | 919 | 1 366 | 750 | 116 | 331 | 2.84 | 1.60 | 10.3 | 6.92 |

Table 5A．50－ohm 5th－Degree Elliptic Lowpass Filter Designs Using Standard－Value Capacitors，Capacitive Input and Output．（Continued from Page 131．）

| Filter <br> No． | $\mathrm{F}-\mathrm{CO}$ | F－3dB <br> （MHz） | $F-A_{S}$ | $\mathrm{A}_{\mathrm{S}}$ <br> （dB） | RC <br> （\％） | C1 | C3 | $\begin{gathered} \mathrm{C} 5 \\ (\mathrm{pF}) \end{gathered}$ | C 2 | C4 | L2 | $\begin{gathered} \text { L4 } \\ (\mu \mathrm{H})=- \end{gathered}$ | $\begin{aligned} & \mathrm{F} 2 \\ & -\quad\left(\mathrm{MH}_{2}\right. \end{aligned}$ | F4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 72 | 2.39 | 3.11 | 5.26 | 49.4 | 3.15 | 825 | 1896 | 680 | 99．3 | 255 | 3.91 | 2.35 | 2． 51 | 5.44 |
| 73 | 2.93 | 3.52 | 5.54 | 48.5 | E． 14 | 820 | 1 1684 | 689 | 92．5 | 263 | 3.37 | 2.85 | 9.64 | 5.83 |
| 74 | $3.2 E$ | 3.79 | 5． 35 | 18.2 | 3．46 | 820 | 15. | E89 | 9\％．6 | 267 | 3．07 | 2． 54 | 9.37 | E．19 |
| 75 | 4.1 ？ | 4.57 | E． 55 | 47， 5 | 1¢．${ }^{\text {c }}$ | 820 | 1．今或 | ESP | シ7＊${ }^{\text {F }}$ | 278 | 2．36 | 1．74 | 10.5 | 6.92 |
| 76 | 4.23 | 4.82 | F． 15 | 69.8 | 12.1 | 750 | 1360 | 686 | 45.8 | 125 | 2.46 | 2． ＇1 $^{\prime}$ | 15．6 | 9.53 |
| 77 | 4.83 | 5.17 | 7.30 | 47.2 | 22.1 | 820 | 12 뱅 | 889 | 196 | 286 | 1.95 | 1． 54 | 11.4 | 7.59 |
| 76 | 4.97 | 5.47 | 119．0 | © | 17．7 | $7{ }^{7}$ | 12912 | 689 | 46.4 | 127 | 2． 25 | 1.3 .3 | LE． 3 | 10．5 |
| 79 | 2.74 | 3.49 | 5.73 | 48.9 | 3.75 | 750 | 1569 | 529 | 83．E | 246 | 3.45 | 2.94 | 9.36 | 5.99 |
| 90 | 3.97 | 3.73 | 5.73 | 48．5 | 5.39 | 756 | 1506 | 629 | 84.9 | $24 \%$ | 3.19 | 2.68 | 9.67 | 6.23 |
| 81 | 3．968 | 4.41 | E．ES | 47．E | 16，\＃ | 759 | 1309 | 620 | 88＂4 | ごき | 2.57 | 2.16 | 10.6 | 6.91 |
| 日 | 4.47 | 4.91 | 7.15 | 47．2 | 15．3 | $7{ }^{\text {7 }}$ | 1289 | 620 | 98， 6 | 358 | 2，21 | 1．7．7 | 11.3 | 7.43 |
| 83 | 5.24 | 5.51 | 7.39 | 4E．＇3 | 21.8 | 75 | 1160 | 620 | 93．4 | 266 | 1．84 | 1.42 | 12.3 | 6.19 |
| 84 | 2．85 | 3.71 | E．15 | 48.8 | 3． | 689 | 15004 | 5 ECO | アゼ | 208 | 3.26 | 2.78 | 10.1 | E． 43 |
| 8 | 3.64 | 4.32 | E． 72 | 47.8 | E．7 | 680 | 1300 | 56 | 794 | Ezs | －1．72 | 2．26 | 10.8 | ？ B ．${ }^{\text {a }}$ |
| 86 | 4.16 | 4.34 | $\therefore 1.14$ | 47.3 | 7．95 | 684 | 1200 | 56 | 81.3 | 203 | 2．40 | 1．37 | 11.4 | 7.44 |
| 87 | 4.62 | 5.31 | $\cdots \cdot 72$ | 48.9 | 14.5 | 689 | 1100 | 560 | 83.5 | 239 | 2．ge | 1.65 | 12.2 | 8.03 |
| \％ | 4.88 | 5.62 | 10.6 | E9． 1 | 10.7 | E20 | 1190 | 568 | 39， | 137 | 2.15 | 1.91 | 17.4 | 11．1 |
| 89 | 5.72 | 6.13 | 8．58 | $4 E .5$ | 31.5 | 689 |  | 56 | 國， 3 | 245 | 1．ES | 1． 5 | 13.3 | 3． 1 |
| 90 | 5.88 | 6.49 | 11.8 | 59．9 | 15.9 | $6{ }^{\text {ch }}$ |  | 56000 | 可， | 104 | 1.74 | 1.55 | 19.1 | 12.3 |
| 91 | 8.41 | 4.28 | E．93 | 48， | $+.15$ | 626 | 1301 | 510 | rı． 1 | 204 | 2．80 | 2.37 | 11.3 | 7.24 |
| 72 | 3．71 | 4.67 | 7．29 | 47.8 | 6， 38 | 620 | 1290 | 419 | 72．6 | 208 | 2，53 | 2.16 | 11.8 | 7.61 |
| 53 | 4，5\％ | 5.17 | 7.75 | 43 | 9.63 | 4 | 114 | 51.5 | 74．4 | 213 | 2．$¢ 1$ | 1.81 | 12.4 | 8．16 |
| 94 | 5.31 | 5．35 | 6.47 | 48.8 | 14．7 | 520 | 1061 | 510 | 75．7 | $21 \%$ | 1． e ¢ | 1.49 | 13．3 | 9.31 |
| 95 | 6．29 | 6.73 | 9.46 | 40.4 | 21.6 | 320 | 916 | E10．010 | P9\％ | 220 | 1.50 | 1.18 | 14．E | 9.76 |
| PE | 3． 67 | 4.69 | $\cdots$ | 50． 5 | 3，E\％ | 561 | 1200 | 470 | 5pue | 15.4 | 2.59 | 2． 23 | 13.9 | 8.31 |
| 97 | －． 27 | 5.15 | 2．45 | 40．9 | 5．97 | 569 | 1100 | 470 | 58.8 | 187 | 2.32 | 1.97 | 13.6 | 8.77 |
| 寝 | 5.02 | 5.77 | 9.41 | 49.4 | 9．57 | 5605 | 1693 | 470 | 69.3 | 131 | 2． 51 | 1．68 | 14.5 | 9.40 |
| 95 | 5， 91 | 6.5 .3 | － 7.32 | ＋3．9 | 14.6 | 50\％ | 3100 | 479 | 家家 | 175 | 1，es | 1．2\％ | 15， | 15，${ }^{1}$ |
| 100 | T． 1 \％ | 7．65 | 11.1 | 45.6 | 32， | SEC | 家突 | $47^{2}$ | E54． 1 | 181. | 1．32 | 1.16 | 17.3 | 11．5 |
| 151 | 3.99 | 5.13 | E． 51 | 51.0 | 3.52 | 515 | 11日可 | 453 | 51.1 | 145 | 2.36 | 2.06 | 14．4 | 9．20 |
| 182 | 4，71 | 5.69 | 9.34 | 514.4 | 6． 014 | 510 |  | 430 | 52.3 | 148 | $2 \times 11$ | 1．79 | 15.2 | 9．7E |
| 123 | 5.54 | 6.36 | 119．01 | 49．9 | 9．65 | 515 | 914 | 430 | 53.5 | 15 | 1．82 | 1．5．3 | 15.1 | 16.5 |
| 1 104 | E． 6.4 | 7．32 | 11.6 | 49.4 | 15.4 | 516 | 820 | 435 | 55.2 | 156 | 1.50 | 1.23 | 17． | 11.5 |
| 105 | 7.87 | 8.42 | 12.3 | 49.1 | 22.3 | 510 | 756 | 439 | 55.8 | 160 | 1.21 | 5.95 | 19.2 | 12.7 |
| 196 | 4.45 | 5． 0.0 | 9.24 | 49.3 | 3.81 | 476 | 10810 | 396 | 51．4． |  | 2．1．6 | 1.84 | 15.1 | 9． 6.6 |
| 16？ | 5.18 | 6， 17 | 9.32 | 48．6 | 6.39 | 476 | 916 | 396 | 52.6 | 151 | 1.91 | 1.65 | 15.9 | 10.2 |
| 108 | 6.17 | $\stackrel{7}{-1} 81$ | $19 . E$ | 48. | 16．5 | 470 | E20 | 3961 | 54.2 | 155 | 1.63 | 1.34 | 17.6 | 11.1 |
| 109 | 7．19 | $\therefore .70$ | 11.5 | 47.6 | 15．5 | 470 | 8 | 390 | 55． 7 | 159 | 1.37 | 1.11 | 18.2 | 12．0 |
| 119 | 7.6 | 8.34 | 15.9 | 60.9 | 11．7 | 430 | 750 | 396 |  | P1，3 | 1． 4.4 | 1.28 | 25． 1 | 16．6 |
| 111 | 8.63 | 9.20 | 12.9 | 47.3 | 23.2 | 479 | 689 | 396 | 57.6 | 164 | 1.69 | 19．26 | 23.1 | 13.4 |
| 112 | 8．86 | 9.73 | 17.7 | 60.8 | 18.7 | 430 | 680 | 390 | EE．E | 72.4 | 1.15 | 1.02 | 29.5 | 18.5 |


| Filter No． | F－CO | F－3 dB <br> －（MHz | $F-A_{S}$ | $\begin{gathered} A_{S} \\ (\mathrm{~dB}) \end{gathered}$ | RC <br> （\％） | C1 | C3 | C5 | C2 | C4 | $\mathrm{L2}$ $\cdots$ | 4 <br> $\mu \mathrm{H})$－ | $\begin{array}{ll} \text { F2 } & \text { F4 } \\ --(M H z) & -- \end{array}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 113 | 4.80 | 6.18 | 10.4 | 59.1 | 3.94 | 430 | 216 | 350 | 45.6 | 128 | 1.96 | 1.68 | 16.9 | 10.8 |
| 114 | 5.84 | 6.93 | 11.1 | 49.5 | 6． 3.4 | 406 | 88 | 350 | 46.1 | 131 | 1.71 | 1.44 | 17.9 | 11.5 |
| 115 | 6.79 | 7.72 | 11.9 | 49.6 | 10．6 | 464 | \％ 5 | 369 | 47.3 | 134 | 1.48 | 1.23 | 19.6 | 12.4 |
| 116 | 8.86 | 8.83 | 13．1 | 48.5 | 15.3 | 43 b | 689 | 360 | 48.7 | 138 | 1.22 | 1.50 | 20.6 | 13.6 |
| 117 | 9.61 | 16.2 | 14．E | 48.3 | 23.9 | 436 | E20 | 36.9 | 50．ĉ | 142 | 0.97 | 0.78 | 22.8 | 15.2 |
| 110 | 5.47 | 6.91 | 11.8 | 01.3 | 4.11 | 390 | 829 | 335 | 36.5 | 109 | 1．JE | $1.5 \%$ | 19.3 | 12.3 |
| 119 | 5.39 | 7.63 | 12.5 | 50.7 | E． 79 | 390 | 75．4 | 330 | 39.3 | 111 | 1.57 | 1.33 | 20.3 | 13．1 |
| 120 | 7.55 | 8.59 | 13．5 | 50.2 | 10.8 | 398 | 685 | 336 | 46.4 | 114 | 1.34 | 1．12 | 21.7 | 14.1 |
| 121 | 0.90 | 9.7 | 14.8 | 46 | 16.2 | 395 | 620 | 3.30 | 41.4 | 11 ？ | 1.11 | 1．92 | 23．4 | 15．4 |
| 12 c | 10.9 | 11.5 | 16.8 | 49.5 | 24.8 | 390 | 565 | 330 | 42.8 | 123 | 0.86 | 9.70 | 26.2 | 17.4 |
| 123 | 9.87 | 16．7 | 15.7 | 4\％，菏 | $1 \mathrm{P}_{1} 4$ | 360 | 569 | \％ 30 | 42.6 | 119 | 0.97 | 6． 56 | 24.7 | 16.3 |
| 124 | 10．1 | 11.9 | 21．E | E1． 4 | 13.4 | 336 | 560 | 3616 | 19.7 | 53.6 | 1.03 | 9.93 | 8 m | 22.5 |
| 125 | 8．26 | 9.33 | 14.2 | 48.4 | 11.2 | 360 | 520 | 300 | $4 \mathrm{~B} \cdot \mathrm{~T}$ | 116 | 1.22 | 1.80 | 22．6 | 14.8 |
| 126 | 8.28 | 9.84 | 19.6 | 61.7 | 3.03 | 330 | 620 | 391 | 19.3 | 52.8 | 1.25 | 1.14 | 32.4 | 20，6 |
| 127 | $7 \times 1$ | E． 34 | 13．2 | 46 | 7．26 | 360 | 689 |  | 39.7 | 113 | 1.41 | 1.18 | 21.3 | 13.8 |
| 12 | 5.98 | 7.4 | 1203 | 49.6 | 4.41 | 369 | 750 | 360 | 38.7 | 111 | 1.61 | 1.37 | 亩． 1 | 12.9 |
| 129 | 7.69 | 9.63 | 13.8 | 47.1 | 7.37 | 350 | E29 | 270 | 40.0 | 115 | 1． 29 | 1.06 | 22.2 | 14.4 |
| 136 | 6.59 | 8．17 | 13.0 | 478 | 4.54 | 336 | 680 | 270 | 39.9 | 112 | 1.46 | 1.22 | 21.1 | 13．6 |
| 131 | 9.16 | 16.2 | 15．0］ | 4E．5 | 11．g | 390 | 560 | 270 | 41.2 | 118 | 1． 19 | 9． 88 | 2S． 7 | 15.6 |
| 132 | 9.15 | 19.8 | 20.7 | 59.6 | 8.23 | 306 | 56 9 | ご70 | 19.4 | 53.3 | 1.13 | 1．91 | 34.6 | 21.6 |
| 133 | 10.7 | 11．6 | 16.4 | $4 E$－ 0 | 17.4 | 330 | 519 | 275 | 42.5 | 132 | 9． 91 | 5.72 | 25.6 | 17.6 |
| 1，34 | 10．9 | 1．2． | cen 5 | 530 | 13.1 | 304 | 514 | 270 | 17．7 | 54．1 | 0.95 | B． 85 | \％．${ }^{\text {a }}$ | 23.5 |
| 135 | 12．4 | 13．2 | 18．1 | 45.8 | 24.1 | 330 | 476 | 276 | 43．7 | 125 | 6．${ }^{1} 4$ | 0.57 | 2？．3 | 18.8 |
| 136 | 12.8 | 14.0 | 24.7 | 59.2 | 19．2 | 360 | 475 | 279 | 20.1 | 54.7 | 0.74 | 0.63 | 40.1 | 25.8 |
| 137 | 7.14 | 8． 84 | 136 | 4，${ }^{4} 8$ | 4.47 | 309 | 626 | 246 | 39.1 | 114 | 1.34 | 1.19 | 2z．9 | 14.2 |
| 138 | 6.44 | 9.86 | 14．E | 45.1 | 7．탄 | 3801 | 569 | 240 | 40.3 | 117 | 1.17 | 0.94 | 23.2 | 15.2 |
| 139 | 9.81 | 11.0 | 15.6 | 44，5 | 11.4 | 309 | 514 | 249 | 41.6 | 121 | 1． $0 \cdot 0$ | W． 79 | 24.6 | 16.3 |
| 14.1 | 9.85 | 11．7 | 21.6 | 57.4 | ？ 6.6 | 270 | 510 | 246 | 19.5 | 53.8 | 1.04 | 0.93 | 35.4 | 22．6 |
| 1.41 | 11．2 | 1．2．z | 15，${ }^{15}$ | 4．4．1． | 1510 | 304 | 470 | 240 | 42.8 | 124 | 2． 86 | 6． 6.7 | EGu2 | 17.5 |
| 142 | 11.4 | 13．61 | 2\％． 1 | 57.1 | 11．心 | 270 | 49 | E49 | 19.8 | 54.5 | 0.98 | 0.79 | 37.7 | 24.2 |
| 143 | 13.1 | 14.6 | 18．6 | 43.7 | 22.7 | 304 | 430 | 248 | 44.3 | 128 | 6.76 | 6． 58 | 26.6 | 19.3 |
| 144 | 13.6 | 14.9 | 25.4 | 56.9 | 17n4 | 270 | 436 | 240 | 20.2 | 55.4 | 0.75 | 6.65 | 41.0 | 26.5 |

Table 5B．600－0hm 5th－Degree Elliptic Lowpass Fitter Designs Using Standard－Value Capacitors，Capacitive Input and Output．

| Filter No． | $\mathrm{F}-\mathrm{CO}$ | $\begin{gathered} \text { F-3dB } \\ -(\mathrm{kHz}) \end{gathered}$ | F－A | $\begin{gathered} A_{S} \\ (\mathrm{~dB}) \end{gathered}$ | RC <br> （\％） | C1 | C3 | $\begin{aligned} & \mathrm{C} 5 \\ & (\mathrm{nF}) . \end{aligned}$ | C2 | C4 | $\frac{12}{--(n}$ | $\begin{gathered} \mathrm{L} 4 \\ (\mathrm{mH})-- \end{gathered}$ | $\begin{aligned} & \text { F2 } \\ & - \text { (kH } \end{aligned}$ | $\text { F4 } \begin{gathered} \text { F) } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 9．85 | 13． BC | 1．31 | 47.4 | 4．4．4080 | 276 | 566 | 220 | 32.4 | 93.7 | 174 | 145 | 2.12 | 1.36 |
| 2 | 8．89 | 1． $\mathrm{H}_{4}$ | 1．48 | 46.8 | 16．5 | 2？回 | 476 | 2ご0 | 34.1 | 98.2 | 135 | $1{ }^{69}$ | 2．35 | 1．54 |
| 3 | 1.23 | 1．31 | 1.79 | 45.4 | 2̇．7 | 276 | 396 | 22a | 36.4 | 105 | 91．18 | 74，3 | 2.76 | 1．86 |
| 4 | Q． 77 | 0.98 | 1.59 | 48.6 | 3， $\overrightarrow{i l}$ | 2ex | 47419 | 180 | 25.7 | 74.3 | 147 | 124 | 2.59 | 1.66 |
| 5 | 1.86 | 1．21 | 1． 81 | 46.7 | 9． 69 | 22区 | 391 | 189 | 27.1 | 77.9 | 113 | 92． 8 | 2，87 | 1.88 |
| $E$ | 1.41 | 1．52 | 2．12 | 45.9 | 19.7 | 22日 | 334 | 180 | 28.7 | 82.1 | 81.2 | 63.7 | 3，361 | 2.26 |
| 7 | 0.93 | 1． 29 | 2， $0^{1}$ | 49.8 | 3．42 | 120 | 390 | 150 | 19.2 | 54.9 | 122 | 194 | 3.29 | 2.10 |
| 8 | 1.24 | 1． 44 | 2.25 | 48.8 | 8． 41 | 1.80 | 330 | 150 | 29.6 | 57． 6 | 97.1 | 81．0 | 3.61 | 2.34 |
| 9 | 1.75 | 1．9010 | 2.72 | 47.8 | 29.8 | 180 | 279 | 150 | 21.3 | 60.4 | 65.5 | 52.4 | 4.26 | 2.83 |
| 10 | 1． $\mathrm{QF}_{7}$ | 1.36 | e．19 | 46.3 | 3． 11 | 156 | 336 | 120 | 19.2 | 56.1 | 104 | 66． 4 | 3.57 | 2.29 |
| 11 | 1.49 | 1． 71 | 2.49 | 44.6 | 8.89 | 150 | 270 | 120 | 20.4 | 59.2 | 79.5 | 63．E | 3.95 | 2.59 |
| 12 | 2．10 | 2.25 | 3．192 | 43.8 | 20.8 | 150 | 226 | 120 | 22.1 | 63.6 | 53.4 | 40．6 | 4.65 | 3.13 |
| 13 | 1．39 | 1.73 | 2.95 | 51.1 | 2，Es | 129 | 270 | 109 | 12.7 | 36.3 | 84.7 | 73.6 | 4.86 | 3.49 |
| 14 | 1．8E | Cn1E | 3.37 | 48.8 | 8.48 | 1201 | 226 | 190 | 13.3 | 39.0 | 64.8 | 54．6 | 5.41 | 3.51 |
| 15 | 2．64 | 2.84 | 4.09 | 47． | 26．2 | 120 | 185 | 106 | 14.2 | 40.2 | 43.6 | 34.9 | 6.49 | 4.25 |
| 16 | 1．62 | 2.19 | 3.45 | 48.4 | 3． 11 | 106 | 220 | 82 | 11.5 | 33.1 | 68.9 | 58.5 | 5.65 | 3.61 |
| 17 | 込？ | 2.62 | 3.94 | 47.6 | 9.85 | 16 C | 130 | 82 | 12．1 | 34.8 | 52.5 | 43.1 | 6．301 | 4.11 |
| 15 | 3.11 | 3.35 | 4.89 | 46.2 | 19.7 | 1601 | 15is | 82 | 12.9 | 36.8 | 36.9 | 29.0 | 7.30 | 4.87 |
| 19 | 1.99 | 2.59 | 4.33 | 49.4 | 3.15 | 82 | 185 | 63 | 8.93 | 25．6 | 55.3 | 46.2 | 7.10 | 4.53 |
| 29 | 2． 2.2 | 3.15 | 4.88 | $4 \mathrm{G}_{\sim} 2$ | 8． 46 | 边 | 150 | ES | 9.36 | 26.7 | 44.2 | 36.6 | 7．93 | 5.09 |
| 21 | 4.03 | 4.31 | 6.68 | $4{ }^{1} \times 2$ | 22．${ }^{\text {a }}$ | 92. | 120 | 68 | 10．0］ | 28．6 | 28.1 | 22．2 | 9.47 | 6.82 |
| 22 | 2.37 | 3.99 | 5.12 | 48.8 | 3.06 | 68 | 159 | 56 | 7.66 | 22.6 | 47．9 | 4И． 9 | 8.39 | 5.36 |
| 23 | 3.46 | 3.95 | 5.95 | 43.3 | 9．95 | 68 | 120 | 56 | 8.13 | 23.3 | 34．6 | 28.3 | 9.49 | 6.20 |
| 24． | 4.77 | Ein 11 | 7.15 | 46.5 | 21． | 69 | 100 | 56 | 8.63 | 24.6 | 23.8 | 18．7 | 11.1 | 7． 42 |
| 25 | 3． 96 | 3.91 | 6.62 | 50.5 | 3.66 | 56 | 120 | 47 | 5.76 | 16.4 | 37.4 | 32.1 | 10，8 | 6.93 |
| 26 | 4.18 | 4.80 | 7.51 | 49.4 | 9.57 | 56 | 106\％ | 47 | 6.03 | 17.1 | 28.9 | 24.1 | 12.1 | 7.83 |
| 27 | $5 \times 98$ | 6.40 | 9， 22 | 48.6 | 22.5 | $5 \%$ | 82 | 47 | 6.41 | 18.1 | 19.0 | 15.2 | 14.4 | 9.58 |
| 28 | 3.67 | 4.156 | 3.79 | 49.3 | 3.81 | 47 | 109 | 39 | 5.14 | 14.7 | 31.1 | 26.5 | 12.5 | 8.05 |
| 29 | 5.14 | 5.84 | 8.86 | 48.6 | 15.5 | 47 | 82 | 39 | 5.42 | 15.5 | 23.4 | 19.2 | 14.1 | 9.23 |
| $3{ }^{3}$ | 7.19 | 7． 5 \％ | $1 \mathrm{~B}_{6} 8$ | 47.3 | 2\％， | 47 | 68 | 39 | 5.76 | 16.4 | 15.6 | 12.3 | 15，8 | 11.2 |
| 31 | 4.56 | 5.75 | 8.82 | 51.3 | 4.11 | 5 | 82 | 33 | 3.85 | 10.9 | 25.4 | 21.9 | 16.1 | 19．3 |
| 32 | E． 30 | 7.15 | 11．3 | 50.2 | 10.5 | 39 | 68 | \％3 | 4． 94 | 11.4 | 19.3 | 16.1 | 19．1 | 11.7 |
| 33 | 9.95 | 9.62 | 14.6 | 49.5 | 24.8 | 39 | 56 | 33 | 4.23 | 12.0 | 12.4 | 16．0 | 21.8 | 14.5 |
| 34 | 5.49 | 5.81 | 19.8 | 47.7 | 4.57 | 33 | 68 | 27 | 3.79 | 11.2 | 21.1 | 17.6 | 17．E | 11.3 |
| 35 | 7.58 | 3．51 | 12.5 | 46.5 | 11.5 | 33 | 56 | 27 | 4.12 | 11.8 | 15.7 | 12．7 | 19.8 | 13.6 |
| 36 | 10.4 | 11．9 | 15.1 | $4{ }_{4}$ | 24.1 | 33 | 47 | 27 | 4.39 | 12.5 | 10.7 | 8.25 | 23.3 | 15.6 |

＊ $100 \mathrm{nF}=.1 \mu \mathrm{~F}$


Figure 6. Highpass lilter schematic diagram and attenuation response, capacitive input and output.
Table 6. 50-ohm 5-Eiement Chehyshev Highpass Filter Designs, Using Standard-Value Capacitors. Capacitive Ioput and Output. (Continued on Page 136.)

| $\begin{aligned} & \hline \text { Filler } \\ & \text { No. } \end{aligned}$ | Cutoff | $\begin{aligned} & \text { Frequen } \\ & 3-\mathrm{dB} \end{aligned}$ | $\begin{aligned} & (\mathrm{MHz}) \\ & 20-8 \mathrm{~B} \\ & \hline \end{aligned}$ | 50 dB | $\begin{aligned} & \mathrm{AC} \\ & (\%) \end{aligned}$ | $\begin{gathered} \mathrm{C}_{1} \mathrm{C5} \\ (\mathrm{pF}) \end{gathered}$ | $\begin{gathered} \mathrm{L}, \mathrm{~L}, 4 \\ (\mu \mathrm{H}) \end{gathered}$ | $\begin{gathered} \hline \mathrm{C3} \\ (\mathrm{pF}) \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1.043 | 0.726 | 9. 501 | 0.263 | 2.17 | 5106 | 6.447 | 2296 |
| 2 | 1.045 | Q.788 | [1.554 | 3. 29.4 | 3.80 | 4960 | 5.969 | 2046 |
| 3 | 1.169 | 0.800 | 0. 5.55 | 0.289 | 1.94 | 4760 | 5.851 | 2960 |
| 4 | 1.679 | 0.657 | Q. 015 | 0.331 | E. 36 | 36.60 | 5.562 | 1864 |
| 5 | 1.172 | 0.877 | 0.616 | 0.327 | 3.67 | 2908 | 5.358 | 1864 |
| 6 | 1.329 | 9.890 | 6.609 | 6. 318 | 1.67 | 4308 | 5. 258 | 1896 |
| $\stackrel{7}{7}$ | 1.119 | 0.938 | 5. 685 | 0.372 | 9.3 | 8946 | 5.195 | 1600 |
| 8 | 1.24E | 0.974 | 0.693 | 0.371 | 5.16 | 3300 | 4.360 | 160 c |
| 3 | 1: 380 | 0.993 | 6. 6.61 | 1,364 | 2.77 | 3606 | 4.714 | 16 GE |
| 18 | 1.541 | 1.0163 | 6. 683 | 0,356 | 1.89 | 3940 | +.66\% | 1540 |
| 11 | 1.284 | 1.028 | 0.738 | 0.397 | 5.301 | 3004 | 4.635 | 1504 |
| 12 | 1.482 | 1.955 | 9.738 | 0.391 | 3.29 | 3391 | 4.444 | 1596 |
| 13 | 1.605 | 1. 1.68 | E. $0^{46}$ | 0.381 | 1.6 6 | 3641 | 4. 585 | 1590 |
| 14 | 1.255 | 1.144 | 0.840 | 0.458 | 16.21 | 2409 | 4.28E | 13618 |
| 15 | 1.545 | 1.201 | 0.853 | 0.456 | 4.93 | 2769 | 3.935 | 1309 |
| 16 | 1.754 | 1.227 | 0.848 | 0.445 | \%, $\mathrm{z}_{6}$ | उणघए | 3.813 | 1309 |
| 17 | 1.453 | 1.235 | 0.968 | 0.496 | 10.E3 | 2290 | 3. 985 | 1240 |
| 18 | 1.684 | 1.285 | 5.923 | 0.496 | 6.36 | 2496 | 3.769 | 1294 |
| 19 | 1. 848 | 1.325 | 0.921 | 6. 485 | 2.78 | 2898 | 3.536 | 1296 |
| 26 | 2.148 | 1.346 | 9. 9 \% 15 | (1) 4 76 | 1. $\mathrm{H}^{7}$ | 31010 | 3. 5161 | 1204 |
| 21 | 1.569 | 1.344 | 0.988 | 0.544 | 11.14 | 2604 | 3.686 | 1196 |
| $2{ }^{\circ}$ | 1. 754 | 1.492 | 1. 1007 | B. 541 | 6.30 | 2200 | 3.399 | 1190 |
| 23 | 1.935 | 1.437 | 1. $300^{\circ}$ | 1.5. 54 | 3.42 | 24615 | 3.267 | 1160 |
| 24 | 2. 265 | 1.460 | 0.09\% | Q. 516 | 1.29 | 2746 | 3.289 | 1160 |
| 25 | 1.925 | 1.542 | 1.197 | 0.595 | E. 30 | 2066 | 3.996 | 1696 |
| 25 | 2.148 | 1.58\% | 1,167 | 6. 566 | 3.29 | zild | 2.96\% | 1969 |
| 27 | 2.469 | 1.603 | 1.65 | 0.572 | 1.68 | 2464 | z.929 | 10100 |
| 26 | 2.896 | 1.688 | 1.218 | E. 6.54 | E.7E | 1890 | 2.832 | 919 |
| 2 | 2.357 | 1.75 | 1. 217 | 6, 0.44 | 3.31 | 2060 | 2.Est | 916 |
| 30 | 2.675 | 1.76 | 1.202 | 6. Ee7 | 1.54 | 200 | 2.65E | 916 |
| 31 | 2.129 | 1.805 | 1.328 | [1.725 | 10.76 | 1504 | 2.729 | 824 |
| \% | 2.234 | 1.863 | 1.3047 | Qnic7 | 7.35 |  | 2.576 | -24 |
| 33 | 2.612 | 1.930 | 1.851 | 日, \%15 | \%. 34 | 18 cm | 2.431 | 920 |
| 34 | 3.409 | 1.957 | 1.332 | 6.6.94 | 1.38 | 2004 | 2.393 | eca |

Table 6．50－ohm 5－Element Chebyshev Highpass Filter Designs
Using Standard－Value Capacitors，Capacitive Input and Output．（Continued from Page 135．）

| Filter No． | －．．－－Frequency（MHz）－．．．． |  |  |  | RC <br> （\％） | $\begin{aligned} & \mathrm{C1}, \mathrm{C5} \\ & (\mathrm{pF}) \end{aligned}$ | $\begin{gathered} \mathrm{L} 2, \mathrm{~L} 4 \\ (\mu \mathrm{H}) \end{gathered}$ | $\begin{gathered} \mathrm{C} 3 \\ (\mathrm{pF}) \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Cutoff | 3－dB | $20-\mathrm{dB}$ | 50 dB |  |  |  |  |
| 35 | 2． 567 | 2． $\mathrm{S}_{5} 7$ | 1.476 | 0．793 | 5.60 | 150 Cl | 2.317 | 750 |
| 36 | 2.752 | 2.1097 | 1.479 | 0． 7.36 | 4.16 | 1696 | 2.245 | 750 |
| 37 | 3.211 | 2.157 | 1．460 | 日． 652 | 1． 61 | 1294 | 2.190 | 756 |
| 38 | 2．691 | 2.227 | 1.619 | $0.87 \%$ | 8.32 | 1300 | 2.170 | 680 |
| 39 | 3.168 | 2.329 | 1.628 | 19．80 | 3.25 | 15614 | 2.013 | 680 |
| 49 | 2.443 | 2．352 | 1． 515 | R． 845 | 1.92 | 1506 | 1． 989 | 689 |
| 4.1 | 2.95 | 2.456 | 1． 7.7 | 8． 961 | 7.76 | 1264 | 1.955 | 609 |
| 42 | 3.275 | 2．525 | 1．709 | 0．954 | 4． 62 | 1504 | 1．86\％ | 620 |
| 43 | 3.931 | 2.587 | 1．764 | 9．920 | 1.49 | 1509 | 1.809 | 625 |
| 44 | 3.379 | 2．786 | 1.974 | 1． CE 4 | 7.05 | 1109 | 1．751 | 56.0 |
| 45 | 3．7＇1．6 | 2．811 | 1． 130 | 1． .152 | 3.98 | 120 | 1.60 | 560 |
| 46 | 4.105 | 2.852 | 1.966 | 1．0132 | 2．15 | 1364 | 1．6．49 | 569 |
| 47 | 3.693 | 3.602 | 2.167 | 1．168 | 7.13 | 1006 | 1.596 | 510 |
| 45 | 4.113 | 3.691 | 2.174 | 1．154 | 3.89 | 1196 | 1．520 | 516 |
| 49 | 4.590 | 3.136 | 2． 155 | 1．123 | 1.92 | 120 | 1.491 | 510 |
| 51 | 3.956 | 3.240 | 2.347 | 1．263 | 7.79 | 910 | 1.465 | 476 |
| 51 | $4.39 \%$ | 3，343 | 2．360 | 1.255 | 4.18 | 1096 | 1．456 | 476 |
| 52 | 4.945 | 3．441 | 2.344 | 1．22E | 2．01 | 1100 | 1．375 | 479 |
| 5 | 4.244 | 3.517 | 2.559 | 1．356 | E． 4.4 | 820 | 1．375 | 438 |
| 54 | 4.772 | 3.550 | 2．580 | 1.375 | 4.34 | 916 | 1． 291 | 43 a |
| 55 | 5.358 | 3.714 | 2.560 | 1.343 | 2.12 | 16 Ca | 1．259 | 435 |
| 54 | 4.724 | 3.893 | 2．8． 6 | 1.528 | 8．03 | 768 | 1．239 | 399 |
| 57 | 5.223 | 4.1017 | 2.244 | 1.516 | 4.54 | 220 | 1.174 | 390 |
| 58 | 5,934 | 4.997 | 2.821 | 1.479 | 2.46 | 910 | 1.142 | 390 |
| 59 | 5.014 | 4.182 | 3.651 | 1.655 | 8.93 | 686 | 1．161 | 368 |
| 60 | 5．59\％ | 4.341 | 3.881 | 1．645 | 4.83 | 7501 | 1． 1.68 | 360 |
| $E 1$ | 5.223 | 4.424 | 3.166 | 1．615 | 2.51 | 324 | 1．058 | 360 |
| 52 | 5.437 | 4.550 | 3.324 | 1．896 | 9．2\％ | 629 | 1． 1.669 | 336 |
| 63 | 6．63 | 4．720 | 3．3E1 | 1.797 | 5.26 | 659 | 1． 10.6 | 330 |
| 64 | E．7\％ | 4.825 | 3.345 | 1． 7 ¢ 1 | 2．56 | 750 | 0．976 | 336 |
| 65 | 7.702 | 4.869 | 3.297 | 1.713 | 1.14 | 820 | 0.962 | 330 |
| 65 | 5.936 | 4.988 | 3． 651 | 1.955 | 9.56 | 564 | 0.978 | 3019 |
| 67 | 6.658 | 5.187 | 3．697 | 1．976 | 5.10 | 629 | 6． 516 | 364 |
| 68 | 7.437 | 5．305 | 3.681 | 1.939 | 2．61 | E80 | 0.882 | 300 |
| $8 \%$ | 6.558 | 5.358 | 3.622 | 1.880 | 1，07 | 759 | 0.875 | 306 |
| 76 | 5.685 | 5.575 | 4.65 | 2．207 | 8.93 | 510 | 0.876 | 270 |
| 71 | 7.428 | 5.780 | 4．1．98 | 2.194 | 4.98 | 560 | 0.817 | 270 |
| $E 2$ | 3．392 | 5.966 | 4.024 | 2.146 | 2.35 | E20 | 0.792 | 276 |
| 73 | 7.336 | 6.376 | 4． 604 | 2．43 | 7.19 | 47 G | 0.752 | 240 |
| 8.4 | 8.591 | 6.546 | 4.622 | 2． 45.3 | 4.22 | 51.6 | 9．719 | 246 |
| 75 | 9．643 | 6.658 | 4.584 | 2．404 | 2． 06 | 568 | 0.702 | 240 |
| 76 | 8． 529 | 5.950 | $5-10$ | 2.708 | 7.27 | 436 | 0.696 | 220 |
| 77 | 9.436 | 7.156 | 5．041 | 2.679 | 4.66 | 470 | 0.656 | 220 |
| 78 | 10.43 | 7.257 |  | 2.627 | 2.17 | 510 | 9．E44 | 2 E |
| 79 | 9.358 | 7.637 | 5．5．1 | 2.939 | 7．38 | 390 | 日． 6.3 | 200 |
| 80 | 10.45 | 7.877 | 5．544 | 2.944 | 5.36 | 436 | 1．5．96 | 200 |
| 8. | 9.686 | 6．23c | 6.056 | 3． 304 | 16.63 | 336 | 6． 597 | 189 |
| 82 | 19．76 | 8.569 | 6.152 | 3.305 | E． 36 | 268 | 日． 5.56 | 136 |



Figure 7．Highpass lilter schematic diagram and attenuation response，capacitive input and output．
Tahle 7．50－ohm 7－Eiement Chebyshev Highpass Filter Designs Using Standard－Value Capacitors，Capacitive Input and Output． （Continued on Page 138．）

| Filter No． | Cutoff | $\begin{aligned} & \text { Frequer } \\ & 3-\mathrm{dB} \end{aligned}$ | $\begin{aligned} & (\mathrm{MHz}) \\ & 20 \mathrm{~dB} \end{aligned}$ | $50-\mathrm{dB}$ | $\begin{aligned} & \hline \overline{R C} \\ & (\%) \\ & \hline \end{aligned}$ | $\begin{gathered} \mathrm{C1}, \mathrm{C} 7 \\ (\mathrm{pF}) \end{gathered}$ | $\begin{array}{r} \mathrm{L}, \mathrm{LG} \\ (\mu \mathrm{H}) \\ \hline \end{array}$ | $\begin{gathered} \mathrm{C}, \mathrm{C5} \\ (\mathrm{pF}) \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{L4} \\ (\mu \mathrm{H}) \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1．02z | 61.826 | 5.660 | 6． 435 | 1.76 | 5100 | 6.162 | 2000 | 4.982 |
| 2 | 1.0132 | 9．980 | 10．724 | 8． 489 | E． 16 | 3960 | 5.673 | 1300 | 4.855 |
| 3 | 1.079 | 0.905 | 0.732 | 0．487 | 2.80 | 4306 | 5.554 | 1890 | 4.681 |
| 4 | 1.159 | 0.922 | E． 734 | B．482 | 1.45 | 4709 | 5．554 | 1890 | 4.449 |
| 5 | 1.086 | 0．971 | （4）86， | 0．549 | 6.84 | 3309 | 5.153 | 1600 | 4.477 |
| 5 | 1.160 | 1.002 | 0.819 | B． 550 | 4.11 | 35000 | 4.986 | 1600 | 4.216 |
| 7 | 1.232 | 1.023 | 0.824 | 日． 47 | 2.44 | 9909 | 4.930 | 1699 | 4.055 |
| 8 | 1.33 B | 1．043 | 0.625 | 0．539 | 1． 16 | 436 | 4.953 | 1605 | 3.921 |
| 9 | 1.130 | 1． 221 | 0.853 | 0.583 | S． 16 |  | 4.919 | 1506 | 4.312 |
| 10 | 1.217 | 1．061 | 0.871 | 8.587 | 4.71 | 3309 | 4.763 | 1560 | 4.096 |
| 11 | 1.299 | 1.087 | 0.879 | 0.594 | 2.71 | 3699 | 4．626 | 1500 | 3．826 |
| 12 | 1．3B6 | 1.105 | E．889 | 1．578 | 1．51 | 3590 | $4.62 ?$ | 1590 | － 713 |
| 13 | 1． 344 | 1.193 | 6．994 | 0． 676 | 6.58 | 2790 | 4.171 | 1369 | 3． 617 |
| 14 | 1.455 | 1．242 | 1．011 | 9.675 | 3.51 | 3096 | 4.629 | 1369 | 3.379 |
| 15 | 1． 567 | 1．2F9 | 1．916 | 9，\％13 | 1.92 | 35300 | 4． 6104 | 13019 | 3.244 |
| 16 | 1.413 | 1．27？ | 1． 1.66 | 0.723 | 1， 10 | 246 | 3.935 | 1200 | 3.449 |
| 17 | 1．546 | 1．335 | 1.092 | 0.734 | 4.11 | 2700 | 3.739 | 1250 | 3.162 |
| 18 | 1.677 | 1．372 | 1． 180 | 0． 327 | 2． 94 | 31515 | 3.695 | 12 ¢̆ | 3.011 |
| 19 | 1.541 | 1.393 | 1．153 |  | 8.16 | 2266 | 3.507 | 1168 | 3.162 |
| 20 | 1.649 | 1.443 | 1．136 | 6． 509 | 4，95 | 2400 | 3.458 | 1100 | 2.953 |
| 21 | 1.802 | 1.496 | 1．239 | 6． 795 | 2.32 | 2790 | 3． 388 | 1195 | 2.779 |
| ご | 1.973 | 1． 524 | 1.199 | 6，782 | 1.62 | 3 Cla | 6．412 | 1109 | E．5．14 |
| ご3 | 1.695 | 1.532 | 1.279 | 9．875 | 8.15 | 2096 | 3.279 | 1960 | 2.874 |
| 24 | 1.925 | 1.592 | 1． 357 | 0.981 | 4.71 | 2204 | 3，135 | 1965 | 2．671 |
| 25 | 1.948 | 1.631 | 1．316 | 0.877 | 2n「1 | 2496 | 3.004 | 1009 | 2.551 |
| 26 | 2.150 | 1．669 | 1．320 | 8．86く | 1．11 | 276 | ©．097 | 16 T | 2.447 |
| 27 | 1.846 | 1.674 | 1．406 | 0.959 | 8.65 | 1809 | 3．99？ | 510 | 2.644 |
| 28 | 2.094 | 1．748 | 1．436 | 6.963 | 4.74 | 2606 | 2.854 | 910 | 2．432 |
| 29 | 2.153 | 1．795 | 1．4．49 | 8． 963 | 2．58 | 2206 | 2．305 | 910 | 2． 314 |
| 36 | 2．312 | 1．827 | 1.451 | 9．951 | 1.25 | 2465 |  | 919 | 2． $2+2$ |
| 31 | 2． 6 | 1.345 | 1.547 | 1．962 | 9.25 | 1600 | 2．737 | $82 \square$ | 2.415 |
| 32 | 2． 222 | 1.9481 | 1.593 | 1． 017 | 4.78 | 1850 | $2.5 \%$ | 820 | $2 \times 153$ |
| 33 | 2．465 | 1.997 | 1． 619 | 1． $0 ¢$ | 2．43 | 2 Eat | 2． 520 | 820 | 2． 67 |
| 34 | 2．806 | 2.034 | 1．616 | 1．053 | 1.17 | 2c90 | 2． 530 | 820 | 2.019 |
| 35 | 2． 260 | 2． 043 | 1． 365 | 1．166 | 8．19 | 1509 | 2.459 | 750 | 2.155 |
| 36 | 2．37 | － 499 | 1．ア36 | 1．1．73 | 5.5 | 1564 | 2．35 ${ }^{3}$ | 750 | 2.1045 |
| 37 | 2． 599 | 2.175 | 1． $\mathrm{F}^{\prime} \mathrm{Fi} \mathrm{i}^{\prime \prime}$ | 1.169 | 2．71 | 180 C | 2.312 | 750 | 1.913 |
| 36 | 2.394 | 2．221 | 1.760 | 1．152 | 1.24 | 2495 | 2.217 | 750 | 1.842 |

Table 7．50－ohm 7－Element Chebyshev Highpass Filter Designs Using Standard－Value Capacitors，Capacitive Input and Output． （Continued from Page 137．）

| Filter <br> No． | －．．－Frequency（MHz）－．－．－ |  |  |  | $\begin{aligned} & \mathrm{RC} \\ & (\tilde{6}) \end{aligned}$ | $\begin{gathered} (\mathrm{pF}) \\ \mathrm{C}, \mathrm{C} 7 \end{gathered}$ | $\begin{gathered} \text { L2, L6 } \\ (\mu \mathrm{H}) \end{gathered}$ | $\begin{gathered} \mathrm{C} 3, \mathrm{C} 5 \\ (\mathrm{pF}) \end{gathered}$ | $\begin{gathered} \mathrm{L4} \\ (\mu \mathrm{H}) \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Cutoft | 3－dB | 20－dB | 50－dB |  |  |  |  |  |
| 39 | 2.689 | 2.343 | 1.922 | 1.295 | 4.54 | $\pm 565$ | 2． 136 | 585 | 1． 513 |
| 49 | 2.822 | 2．387 | 1.936 | 1．291 | 3.6 | 1 E6E | 2.161 | 656 | 1．754 |
| 41 | 3.165 | $2.44 i$ | 1．941 | 1．262 | 1，31 | 1896 | 2．181 | 68 | 1．E73 |
| 42 | 2．E60 | 2． 429 | 2．949 | 1．4日2 | $\because 6$ | 12¢ | 2．982 | E30 | 1．842 |
| 43 | 2．830 | 2.523 | 2.489 | 1.418 | 6． 23 | 13 C | 1．980 | 520 | 1.712 |
| 44 | 3.162 | 2.636 | 2.127 | 1.413 | 2.57 | 150 | 1.911 | 626 | 1．575 |
| 45 | 3．841 | 2．671 | 2.130 | 1． 4.1 | 1． 8. | 1600 | 1．911 | 6 cg | 1．535 |
| 46 | 2．982 | 2．711 | 2.276 | 1．557 | 8.93 | 1109 | 1.859 | 569 | 1．6\％6 |
| 47 | 3.195 | 2.816 | 2.323 | 1.572 | 5.56 | 1260 | 1．722 | 560 | 1．522 |
| 48 | 3．892 | 2．889 | 2．349 | 1．57以 | 3.38 | 1300 | 1.734 | 560 | 1．451 |
| 49 | 3.810 | 2.977 | 2.85 | 1.542 | 1.19 | 1506 | 1．732 | 56.9 | 1.373 |
| 56 | 3.269 | 2.974 | 2.491 | 1．769 | 9.91 | 1509 | 1． 596 | 519 | 1.494 |
| 51 | 3．525 | 3.104 | 2.553 | 1．726 | $5{ }_{5} 3^{31}$ | 1184 | 1．610 | 519 | 1．380 |
| 5 | 3．763 | 3.183 | 2．51 | 1．722 | 3．099 | 1260 | 1．575 | 510 | 1．312 |
| 53 | 4.008 | 3．246 | 2.589 | 1.766 | 1．7E | 1360 | 1．571 | 516 | 1．270 |
| 5 | 3.519 | 3．205 | 2．691 | 1．856 | 9．64 | 910 | 1．575 | 476 | 1.396 |
| 55 | 3.756 | 3.347 | 2.764 | 1．872 | 5.72 | 1000 | 1．491 | 475 | 1.283 |
| 56 | 4． 967 | 3.449 | 2.819 | 1.859 | 3.20 | 1109 | 1．453 | 470 | 1．213 |
| 57 | 4.355 | 3，517 | 2.810 | 1.351 | 1.74 | 1206 | 1.445 | 470 | 1.170 |
| 58 | 4.121 | 3．651 | 3.117 | 2.946 | 5.91 | 914 | 1．367 | 430 | 1.179 |
| 5 | 4，424 | 3.763 | 3． $0_{15} 5$ | 2． 144 | 3.34 | 1000 | 1．3．1 | 436 | 1．113 |
| 60 | 4.760 | 3.845 | 3.871 | 2．023 | 1．72 | 1102 | 1． 325 | 436 | 1.076 |
| 81 | 4.205 | 3.349 | 3.235 | 2.225 | 9.99 | 750 | 1.317 | 390 | 1.167 |
| $E 2$ | 4.521 | 4． 115 | 3.322 | 2，255 | 6.14 | 926 | 1.244 | 396 | 1． 6174 |
| 63 | 4．890 | 4.153 | 3.373 | 2.253 | 3.27 | 916 | 1．296 | 390 | 1.698 |
| 64 | 5． 267 | 4.242 | 3.386 | 2．236 | 1.69 | 1049 | 1． 202 | 396 | 0.969 |
| 65 | 4.864 | 4.333 | 3.592 | 2．441 | E． 46 | 7513 | 1.153 | 366 | 0.993 |
| E6 | 5． 2 E 2 | 4.469 | 3.645 | 2． 244 | 3.81 | 829 | 1.118 | 360 | 0.942 |
| E7 | 5.639 | 4．582 | 3.668 | 2.420 | 1.88 | 910 | 1.198 | 360 | 0.899 |
| 68 | 5.268 | 4.706 | 3.908 | 2.660 | 6.87 | $6 \%$ | 1．063 | 330 | 0.924 |
| 69 | 5．EEG | 4．87E | 3.976 | 2.657 | 3．8E | P兵成 | 1． 1.8 | 336 | 0． 864 |
| 78 | E． 067 | 4.931 | 4.8100 | 2．64E | 2，13 | $80^{4}$ | 1．016 | 330 | 0.829 |
| 71 | 5.860 | 5.183 | 4.362 | 2.927 | 6.76 | E20 | 0.985 | 360 | 9.833 |
| 72 | 5.220 | 5． 355 | 4.372 | 2.934 | 3.53 | E80 | 0.933 | 360 | 0.787 |
| 73 | 6． 2 jeg | ¢． 497 | 4.491 | 2．969 | 2． $\mathrm{F}_{2} 4$ | 7 Cig | 0.523 | 3 Ex | 0.752 |
| 74 | 7． 247 | 5． 576 | 4，397 | 2.867 | 1． 60 | g25 | 0.931 | 300 | 0.731 |
| 75 | 6.462 | 5.767 | 4.784 | 3.25 | 6.83 | 569 | 0.867 | 270 | 0.752 |
| 76 | 6.979 | 5.972 | 4.865 | 3.250 | 3．E3 | ES | 0.337 | 270 | 区． 303 |
| 77 | 7．496 | E． 145 | 4． 290 | 3.229 | 1．93 | 689 | 0.831 | 27. | 0.675 |
| 78 | 5.940 | 6.315 | 5.292 | 3.631 | 9.97 | 478 | 0.798 | 240 | 19．704 |
| 79 | 7．467 | 6． 551 | 5.411 | 3．665 | 5.78 | 510 | 日． 762 | 240 | 3． 6.56 |
| 80 | 7． 946 | 6.748 | 5.481 | 3．E61 | 3.27 | 56 | 9．742 | E4 | 0． 620 |
| 81 | 8．E12 | 6.983 | 5．592 | 6.619 | 1.5 | E2d | 0． 7.75 | $\underline{z}+6$ | 0.595 |
| E2 | 7.559 | E． 383 | 5.769 | 3.964 | 9.17 | 436 | 0.733 | 225 | 0．646 |
| 83 | 8.113 | 7.161 | 5.569 | 4.604 | 5.6 | 476 | 9．69？ | 220 | 0.599 |
| 34 | 8． 5 E6 | 7． 249 | 5.978 | 3.995 | 3.41 | 51.1 | 0． 6.81 | 220 | 8.570 |
| 35 | 9．20日 | 7.509 | 6.6192 | 3.957 | 1.73 | 50.9 | 9，67？ | 220 | 5． 0.548 |
| 86 | 3.293 | 7． 561 | E． 341 | 4． 558 | 9，28 | 391 | 0.667 | 299 | 0.589 |
| 87 | 3．9ES | 7.895 | E，598 | 4.411 | 5.49 | 430 | 4． 58 | 201 | 5.542 |
| 89 | 9.587 | E． 113 | E．581 | 4.51 | 3.12 | 478 | E．618 | 209 | 1． 515 |
| 8 | 10， 2 | 8.263 | E．EtS | 4.351 | 1．76 | 519 | 6． 616 | 206 | 6． 498 |
| 911 | 9.417 | E． 511 | 7． 165 | ＋． 85 | 8.10 | 而可 | 9． 590 | 180 | 9.517 |
| 9 | 18.02 | 6． 296 | 7.241 | 4.891 | 5.16 | 960 |  | 186 | 9．4Es |
| 92 | 11.79 | 9.951 | 7.221 | 1．832 | 3.84 | 436 | 1． 5.55 | 186 | $0.4 E 8$ |



Figure 8. 50-ohm 5-th degree elliptic highpass filfer designs using standard-value capacitors for C1, C3 and C5.

Table 8A. 50-ohm 5th-Degree Elliptic Highpass Fitter Designs Using Standard-Value Capacitors, Capacitive Input and Output, (Continued on Page 140.)

| Filter No. |  |  |  |  | (\%) |  | C3 |  | C2 | C4 | $\mu$ | $\begin{array}{r} \mathrm{L} 4 \\ \mu \mathrm{H})- \end{array}$ |  | F4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | B. 79 | 0.7 | 9.5 | 49.6 | 20. | 3. |  | . |  |  |  | 10. | 0.32 | D. |
| 2 | 0.93 | 0.84 | 0.63 | 41.0 | 12.9 | 3.6 | 2. | 4. | 21 | 726 | 7.09 | 9. | 0.41 | 11 |
| 3 | 0.92 | 0.88 | 0.53 | 48.1 | 9.8 Bl | 3.9 | 2. 2 | 4. | 34. | 11 | 6.86 | 2. 32 | 0.33 | 9. 51 |
| 4 | 1.02 | 0.86 | 0.60 | 42.4 | 5.92 | 4.3 | 2.2 | 5.5 | 27. | 9.34 | 6.44 | 8.18 | 0.38 | 1.58 |
| 5 | 1.04 | 0.82 | 0.48 | 50.5 | 3.73 | 4.7 | 2.2 | 5.6 | 45.6 | 16.0 | 6.36 | 7.40 | 0.30 | 9.46 |
| 6 | 1.15 | 0.86 | -. 58 | 42. | 2.27 | 5.1 | 2.2 | 5.8 | 32. | 10.7 | 6.26 | 7.77 | 0.36 | 55 |
| ? | 0.97 | 0.90 | 0.69 | 40. 8 | 18.2 | 3. | 2.6 | 3.9 | 17.6 | 5.9 | 7.5 | 9.5 | 0.45 | 9.67 |
| 8 | 0.95 | 0.85 | 6. 55 | 49.9 | 13.8 | 3.3 | 2.6 | 3.9 | 31. | 11.1 | 6.67 | 9.04 | 0.35 | 3 |
| 9 | 1.08 | 0.94 | 6. 6.5 | 41.5 | E. 67 | 3.6 | 2. 61 | 4.7 | 22. | 7.53 | 6.06 | 2.87 | 0.43 | 0.65 |
| 10 | 1.08 | 0.96 | 0.57 | 48.7 | 6.17 | 3.9 | 2.9 | 4.7 | 34.9 | 12.2 | 5.93 | 7.07 | 0.35 | 0.54 |
| 11 | 1.19 | 0.94 | 0.63 | 43.1 | 3.57 | 4.3 | 2.8 | 5.6 | 28.6 | 9.62 | 5.73 | 7.12 | 0.39 | 1 |
| 12 | 1.28 | 0.74 | 0.62 | 43.0 | 2.96 | 4.7 | 2.0 | 6.2 |  | G. 3 | 5.69 | 7. | 9. |  |
| 13 | 1.01 | 0.94 | 0.67 | 45.9 | 19.7 | 2.7 | 1.6 | 3.3 | 20. | . 24 | 5.58 | 8.40 | 4.43 |  |
| 14 | 0.98 | 0.88 | 0.47 | 61.3 | 4.7 | 3. ${ }^{\text {a }}$ | 1.6 | 3.3 | 50. | 18.4 | 6.22 | 6.94 | 0.28 | 0.45 |
| 15 | 1.14 | 0.98 | 0.61 | 59.4 | 8. 50 | 3.3 | 1.8 | 3. | 32. | 11.4 | 5.53 | 6.54 | 9.38 |  |
| 16 | 1.27 | 1.85 | 0.73 | 42.4 | 5.27 | 3.6. | 1.8 | 4.7 | 23. | ¢ | 5.23 | 6.62 | $\square_{0.46}$ | 0. |
| 17 | 1.39 1.33 | 1.01 1.05 | 0.89 0.71 | 49 | 42 | , | 1.8 | 4.7 5.1 |  |  | 5.19 5.15 | 6.07 | 0.37 |  |
| 18 | 1.33 | 1. |  |  |  |  |  |  |  |  |  |  |  |  |
| 13 | 1.02 | 0.94 | 0.57 | 56.8 | 22.7 | 2.4 | 1.5 | 2.7 | 31.7 | 11.5 | 6.35 | 7.9 | 2.35 |  |
| 20 | 1.13 | 1.01 | 0.55 | 59.3 | 13.6 | 2.7 | 1.6 | 3. | 48,9 | 15.9 | 5.41 | . 69 | a. 34 | 9.53 |
| 21 | 1.24 | 1.11 | 0.76 | 46.5 | 12.1 | 2.7 | 1.6 | 3.3 | 21.6 | 7.52 | 5.15 | 5.39 | 5.45 |  |
| 22 | 1.37 | 1.18 | 0.83 | 42.2 | 7.22 | 3.8 | 1.6 | 3.5 |  |  |  | 6.69 | 0.53 |  |
| 2 | 1.39 | 1.12 | 0.66 | 51.1 | 4.59 | 3.3 | 1.6 |  |  | 11.7 | 4, 5 ? | 5.43 | 0.40 | 0.6 |
| 25 | 1.19 |  | 0.81 | 45.4 | 21.3 | 2.2 | . 5 | . 7 | 16. | . 11 | 5.55 | F. 2 | 9. 52 | . 7 |
| $2 \varepsilon$ | 1.16 | 1.96 | 0.62 | 56.9 | 17.0 | 2.4 | 1.5 | 2.7 | 32.2 | 11.7 | 5.37 | 5. 17 | 9.38 | . 5 |
| 2 | 1.39 | 1.26 | 0.88 | 46.8 | 9.05 | 2.7 | 1.5 | 3.3 | 22.0 | 7.66 | 4.61 | 5. 65 | 0.50 | 0.71 |
| 28 | 1.45 | 1.27 | 9. 94 | 41.3 | 8.59 | 2.7 | 1.5 | 3.6 | 15.E | 5. 29 | 4.53 | S. 99 | 0.60 | 9.9 |
| 29 | 1.52 | 1.26 | 0.8 ? | 42. 7 | 5.23 | 3.0 | 1.5 | 3. | 19, 6 | 5.61 | 4.36 | 5.50 | 0.54 | 0.85 |
| 30 | 1.56 | 1. | 0.69 | 51.5 | 3.11 | 3.3 | 1.5 | 3.9 | 33 | 11.9 | 2 | 4.97 | Q. 42 | [1. 66 |

Table 日A．50－0hm 5－th Degree Eltiptic Highpass Filter Designs Using Standard－Value Capacitors，Capacitive input and Output．
（Continted from Page 139．）

| Filter F－CO No． | F－3dB <br> －（MHz |  | $\begin{aligned} & \mathrm{A}_{S} \\ & (\mathrm{~dB}) \end{aligned}$ | RC <br> （\％） |  | C3 |  | C 2 | C4 |  | $\begin{gathered} L 4 \\ (\mu H) \cdots \end{gathered}$ |  | F4 z) . . |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 31.1 .29 | 1.23 | 0.71 | 45.7 | 26.7 | 1.8 | 1.3 | 2.2 | 13.4 | 4.88 | 5.43 | 7．19 | 19：59 | 0.87 |
| 62 1．25 | 1．1．01 | 6， 5 | 61.3 | 21.3 | 2.0 | 1.3 | 2.2 | 3\％．9 | 12.1 | 5.197 | E．71 | 0.33 |  |
| 351.53 | 1.37 | 0.94 | 45.1 | 11．9 | こ，2 | 1.3 | 2．${ }^{\text {a }}$ | 17.2 | 5．00 | 4.17 | 5.19 | 6． 1.59 | 1． 613 |
| 341.84 | 1．41 | 5．9E | 45.1 | 7．91 | 2．4 | 1.3 | 3．${ }^{\text {a }}$ | 17.8 | 6．13 | 3.92 | 4.8 | 6． 60 | 日． 92 |
| 351.75 | 1．48 | 0.88 | 47.8 | 4.37 | 2.7 | 1.2 | 3.3 | 22.9 | 7.75 | 3.77 | 4．50 | 6.54 | 0.84 |
| 361.81 | 1． 4.47 | 1．6\％ | 41.4 | 4.33 | 2，${ }^{\text {a }}$ | 1． 3 | 3.6 | 16.4 | 5.47 | 3.74 | 4.76 | 0．64 | 8.97 |
| $37 \quad 1.51$ | 1． 49 | 1． 91 | 45.9 | 19.7 | 1．8 | 1.2 | 2.2 | 13.8 | 4.22 | 4.39 | 5.68 | 9．E5 | 0.97 |
| 381.47 | 1.32 | 0.76 | 6.1 .3 | 44.7 | 2.0 | 1.2 | 2.2 | 33.5 | 12.3 | 4.15 | 4．62 | 1， 4.3 | 5.57 |
| 351.61 | 1．44 | 0．9E | 48.2 | 13.9 | 2． 9 | 1.2 | 2.4 | 17． | E． 16 | 3.93 | 4.81 | 6．${ }^{\text {E }}$ | 9．93 |
| 491.75 | 1．51 | 1．00］ | 45.6 | gucr | 2.2 | 1.2 | 2.7 | 17．7 | E． 14 | 3.65 | 4.47 | 10．63 | 园，96 |
| 411.87 | 1．54 | 1.91 | 45.6 | 5.33 | 2.4 | 1.2 | 3.6 | 1E． | 6.27 | 3． 51 | 4.29 | 0．63 | 0.97 |
| 42 E ． 42 | 1.52 | 0.92 | 48.3 | 2.69 | 2.7 | 1．2 | 3.3 | 23． 4 | 8． 19 | 3.44 | 4.84 | 日． 5 E | 1．08 |
| 431.42 | 1.33 | 0． 81 | 56.9 | $2 \mathrm{E} \cdot 9$ | 1．E | 1.1 | 1.8 | 21.0 | 7.65 | 4．6E | 5.43 | 0． 51 | 回，PG |
| $44 \quad 1.65$ | 1．55 | 1.15 | 49.7 | 21.5 | 1． 6 | 1.1 | 2.9 | 10.9 | 3.76 | 4.13 | 5.45 | 4．75 | 1． 11 |
| 451.80 | 1.44 | 6． 86 | 59.2 | 15.7 | 1.8 | 1.1 | 2.9 | 27.1 | 3.92 | 3.86 | 4.36 | 0.49 | 9.77 |
| 461.76 | 1．59 | 1． 18 | 45.3 | 1．3．8 | 1.8 | 1.1 | 2.2 | 14．2 | 4.96 | 3.64 | 4.55 | \％． 7 |  |
| 471.87 | 1.61 | 1． 1.94 | 48.7 | 8.74 | $2 \cdot 6$ | 1.1 | 2.4 | $1 \overline{7} .9$ | 6.30 | 3.35 | 4．66 | E1． 65 | 0.99 |
| 482.82 | 1． 56 | 1． 1.6 | 47.1 | 5.36 | 2.2 | 1.1 | 2.7 | 18.1 | 6.23 | 3.22 | 3．83 | 6． 6.6 | 1．बF |
| 491.48 | 1．3采 | 可． 5 | 69．6 | 25.5 | 1.5 | 1.0 | 1.6 | 36.6 | 13． | 4.32 | 4．5\％ | 8.48 | 0.63 |
| 51.78 | 1．65 | 1.15 | 47.8 | 20.2 | 1.5 | 1.0 | 1.8 | 12.7 | 4.47 | 3.71 | 4．54 | 8.73 | 1．10 |
| 511.82 | 1.65 | 6.88 | 59.5 | 9.91 | 1.8 | 1.6 | 2.6 | 27．6 | 15.1 | 3.18 | 3.55 | 6，54 | 10，84 |
| 52 2．07 | 1．89 | 1．26 | 46.8 | 9.95 | 1.8 | 1.6 | 2.2 | 14．7 | 5.11 | 3.187 | 3.77 | 6． 7.5 | 1.15 |
| 53 ¢－19 | 1.91 | 1.41 | 4 C .8 | 0.59 | 1.8 | 1.0 | 2.4 | 10．4 | 3.47 | 3.02 | 3.95 | 1． 96 | 1.35 |
| 548.45 | 1.93 | 1.34 | 4 E .6 | 3.15 | 2.2 | 1.0 | 3.6 | 12.7 | 4.20 | 2.85 | 3.53 | 0.84 | 1.25 |
| 551.93 | 1.81 | 1.34 | 45.1 | 23.5 | 1.3 | 9．91 | 1.6 | 9．45 | 3.29 | 3． 56 | 4.64 | 0.87 | 1.29 |
| 562.11 | 1．90 | 1.27 | 48.8 | 13．E | 1.5 | 0.91 | 1.8 | 13.1 | 4．66 | 3.62 | 3.69 | Q．8E | 1．2 |
| 572.099 | 1.82 | 1.62 | 57.1 | 11．${ }^{\text {a }}$ | 1.6 | 0.91 | 1．8 | 21.9 | 7.94 | 2.93 | 3.33 | 6． 63 | E．93 |
| 58.2 .42 | 2． 20 | 1.28 | 47.4 | 5.69 | 1.8 | 9．91 | 2.2 | 15.1 | 5.24 | 2， 88 | 3.22 | 9.79 | 1.23 |
| 592.51 | 2.10 | 1.50 | 41.6 | 5.55 | 1.8 | 0.91 | 2.4 | 16． 8 | 3.59 | 2.65 | 3.41 | 0.94 | 1.44 |
| 602.84 | 2． 06 | 1.18 | 45.5 | 1．62 | 2.2 | 0， 91 | 2.7 | 19.9 | 5.55 | 2.60 |  | 4.72 | 1．13 |
| 612.2 | 2． 08 | 1．55 | 43.7 | 21． 6 | 1.2 | 6． 3. | 1.5 | 3.19 | 2.83 | 3.05 | 4.62 | 1． 81 | 1.49 |
| 62 2．36 | 2.12 | 1． 5 | 45.5 | 15．E | 1.3 | ［1．82 | 1．5 | 9.83 | 3.42 | 2.79 | 3.54 | 9．96 | 1.45 |
| 53 2．5e | 2.17 | 1．3F | 48.7 | 6． 49 | 1．5 | 0．82 | 1.8 | 13.5 | 4.73 | 2.51 | 3．61 | 0.87 | 1.33 |
| E4 2．69 | 2.25 | 1．5日 | 45.4 | 6． $\mathrm{G}^{5}$ | 1．E | 5．82 | 2.0 | 12．1 | 4.15 | 2.42 | 2.97 | 6． 9.9 | 1.49 |
| $65 \quad 2.89$ | 2.23 | 1．3E | 48.2 | 3.15 | 1.8 | B． 32 | 2.2 | 15．5 | 5.37 | 2.36 | 2.78 | 8.83 | 1.39 |
| 6E 2．97 | 2.35 | 1.59 | 41.8 | 3.12 | 1.8 | 11．82 | 2.4 | 11.1 | 3.71 | 2.34 | 2.94 | 0.95 | 1．52 |
| 67．2．27 | 2.12 | 1．45 | 47.6 | 22.7 | 1.1 | 0．7\％ | 1.3 | 18．1 | 3.59 | 2.43 | 3.62 | 4， 93 | 1.49 |
| $68^{\circ} 2.60$ | 2.37 | 1．70 | 44.2 | 14．7 | 1．2 | 0.75 | 1.5 | 2．48 | 2.92 | 2.51 | S． 22 | 1． 69 | 1．64 |
| 65 玉． 56 | 2．25 | 1．37 | E\％， | 11.4 | 1.3 | 6.75 | 1.5 | 14.6 | 5.24 | 2．42 | 2．92 | 8.85 | 1.31 |
| FE12．93 | 2．44 | 1． 48 | 49.2 | 5.35 | 1.5 | 0.75 | 1.8 | 13.8 | 4.82 | 2.25 | $2 \cdot 61$ | 9． 51 | 1.42 |
| 713.12 | 2．47 | 1.58 | $4 E .9$ | 3.74 | 1，E． | 0.75 | 2.0 | 12.4 | 4.25 | 2.16 | 2． 61 | 8．97 | 1.51 |
| 723.42 | 2.43 | 1，45 | 43.8 | 1.71 | 1．8 | 0.75 | 2.2 | 15.8 | 5.47 | 2.14 | 2.50 | 0.85 | 1.36 |
| 73 2．57 | 2.40 | 1．68 | $4 \overline{1} .8$ | 21.3 | 1.6 | 0.88 | 1.2 | 6．40 | 2.96 | 2.69 | 3.27 | 1．08 | 1.62 |
| 74.2 .49 | 2．2＇6 | 1．17 | 63.2 | 17．1 | 1.1 | 9.68 | 1.2 | 20.1 | 7.40 | 2． 46 | 2.73 | 0.72 | 1.12 |
| 75.9 .95 | 2．68 | 1.85 | 44.7 | 9．72 | 1.2 | 0.66 | 1.5 | 2． 77 | 3.492 | 2． 16 | 2.64 | 1.17 | 1.78 |
| 763.65 | 2.56 | 1．43 | 53.6 | 7．02 | 1.3 | 1.65 | 1.5 | 14.9 | 5.34 | 2.15 | 2． 36 | 10．91 | 1.42 |



Table 8A．50－0hm 5－th Degree Eliptic Highpass Fitter Designs Using Standard－Value Capacitors，Capacitive Input and Output． （Continued from Page 141．）

| Filter No． | $\mathrm{F}-\mathrm{CO}$ | $\begin{array}{r} \mathrm{F}-3 \mathrm{~dB} \quad \mathrm{~F}-\mathrm{A}_{\mathrm{S}} \\ -(\mathrm{MHz}) \end{array}$ | $\begin{gathered} A_{S} \\ (\mathrm{~dB}) \end{gathered}$ | $\begin{aligned} & \mathrm{RC} \\ & \text { (\%) } \end{aligned}$ |  | C3 |  | C2 | 64 |  | $14$ $(\mu \mathrm{H})$ | $\begin{gathered} \text { F2 F4 } \\ \cdots(\mathrm{MHz})- \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 123 | 5.99 | 5.343 .56 | 47.1 | 11.8 | 9， 56 | 0.33 | 4． 68 | 4.63 | 1.62 | 1.66 | 1.31 | 2.273 .46 |
| 124 | 6．72 | 5.764 .15 | 41.1 | 7． 11 | 6， 62 | 8． 33 | 6． 82 | 3.74 | 1．25 | ［． B $^{\text {a }}$ | 1.27 | 2．603．99 |
| 125 | 6.81 | 5.483 .37 | 49.0 | 4.56 | 9.68 | 0.33 | W． 82 | 6.15 | 2.15 | 13．9E | 1，13 | 2.073 .22 |
| 126 | 8.67 | 5.563 .17 | 49.3 | 1.304 | 0.62 | 0．33 | 1.0 | 7．35 | 2.54 | 0.94 | 1.69 | 1.913 .82 |
| 127 | 6.25 | 5.884 .61 | 46.4 | 21，5 | 0.43 | 6， 30 | 0． 56 | 2.45 | 9.83 | 1．12 | 1.55 | 3.054 .45 |
| 128 | 5.40 | 4.952 .54 | E4． 5 | 20．2 | 6． 0.47 | 0.80 | 6． 0.51 | 9.99 | 3.35 | 1.15 | 1.27 | 1.562 .43 |
| 125 | E． 10 | 5.592 .77 | 45.6 | $17=1$ | 0.47 | 6， 30 | 0． 56 | 4.25 | 1.48 | 1.05 | 1．30 | 2.392 .63 |
| 1.30 | 6.80 | 5.312 .77 | 61.7 | 13.4 | 0． 51 | 8．30 | 19．56 | 6.73 | 3.21 | 1． 1.1 | 1.13 | 1.692 .65 |
| 131 | 7.03 | 6.603 .59 | 47.7 | 7.64 | 0.56 | 0．30 | 0． 3.68 | 4．2E | 1．E6 | 0． 91 | 1.09 | 2.423 .73 |
| 132 | 8.68 | 6.643 .56 | 49.7 | 2.56 | 0．63 | 6.34 | 13.32 | 5.29 | 2.19 | 0.86 | 1． 5 ¢ | 2.163 .48 |
| 133 | 6.36 | 5.994 .25 | 47.3 | 23.3 | 6． 39 | 8． 27 | 9．47 | 3.15 | 1.12 | 1．06 | 1．34 | 2.744 .18 |
| 134 | E．13 | 5.632 .97 | 62.3 | 19.4 | Q． 43 | 0． 27 | 9，47 | 7.65 | 2.82 | 1.60 | 1．11 | 1.822 .84 |
| 135 | 7.34 | 5.474 .18 | 49．2＇ | 14．8 | 4． 47 | 0.27 | ［，5E | 4．33 | 1.53 | 0.86 | 1．03 | 2．614．01 |
| 136 | 8．26 | 7.188 .13 | 49．6 | 6.92 | 0． 51 | 0.27 | 达，63 | 3． $\mathrm{g}^{4}$ | 1． 96 | 8． 8.80 | 1． 64 | 3.254 .93 |
| 137 | 8.39 | 6.734 .17 | 46.4 | 4.41 | 9． 56 | 0.27 | 1．68 | 4.96 | 1.71 | 0.78 | 1.95 | 2.574 .90 |
| 1.38 | 9.36 | 7.024 .8 | $42 \cdot 7$ | 2.46 | 4.82 | 0.27 | 0．8こ | 3.79 | 1.33 | 0.77 | 9． 95 | 2.874 .47 |
| 139 | 6．35 | 5.923 .08 | 55.9 | 24.8 | 6． 35 | 1． 24 | 3． 39 | 7.06 | 2.62 | 1． 01 | 1.12 | 1.892 .34 |
| 140 | 8． 48 | 7.525 .81 | 40．4 | 13．1 | 日． 36 | 0.24 | 0.47 | 2.87 | 5． 7.7 | 8.54 | 1，15 | 3.815 .61 |
| 141 | 7． 94 | 7.184 .97 | 47.7 | 14．4 | 6． 39 | 8． 24 | 0.47 | \％．31 | 1.16 | 13．80 | 9．99 | 3.984 .68 |
| 142 | E． 49 | 7．39 4． 82 | 49.7 | 9．4E | 9.48 | 4． 24 | 0． 51 | 4：10 | 1．45 | 13.75 | 9． 89 | 2.884 .43 |
| 143 | E． 97 | 7．44 4.58 | 49.9 | $\underline{0.95}$ | 5． 47 | 3． 24 | G． 56 | 4.47 | 1.57 | 8． 71 | 0.84 | 2.824 .38 |
| 144 | 9.94 | 7.955 .51 | 41.6 | 3.32 | 0.51 | 0.24 | 6.68 | 3.16 | 1． 64 | 0.69 | 0.87 | 3.455 .29 |

Table 8B．600－ohm 5th－Degree Elliplic Highpass－Filter Designs Using Stanard－Value Capacitors，Capacitor input and Output．

| Filter <br> No． |  |  |  | $\begin{aligned} & \mathrm{A}_{\mathrm{S}} \\ & (\mathrm{~dB}) \end{aligned}$ | $\begin{aligned} & \mathrm{RC} \\ & (\%) \end{aligned}$ |  |  | $\begin{aligned} & \mathrm{C} 5 \\ & -(\mathrm{nF} \end{aligned}$ | $\begin{gathered} \mathrm{C} 2 \\ \text { nF) } \end{gathered}$ |  | $L^{L 2}(m$ | $\begin{gathered} \mathrm{L4} \\ (\mathrm{mH})^{-} \end{gathered}$ | $\begin{array}{cc} F_{2} & F_{4} \\ -(\mathrm{kHz}) & \cdots \end{array}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | E． 6.0 | 6.13 | 4.15 | 49.6 | 20．${ }^{\text {a }}$ | 33 | 22 | 39 | 395 | 128 | 11.9 | 14． 6 | 2．64 | 3.39 |
| 2 | P． 6 ？ | 6.71 | 4.35 | 48.1 | 9．86 | 39 | 22 | $4 \cdot \overrightarrow{ }$ | 349 | 11.7 | 9.88 | 12．91 | 2.75 | 4.21 |
| 3 | 8．76 | 6.81 | 4.50 | 5 | $3 \times 7$ | 47 | 2 | 56 | 456 | 164 | 9.17 | 10.7 | 2．4E | 3.85 |
| 4 | 3.46 | 7． 2 可 | 5.59 | 45.9 | 19.7 | 27 | 16 | 33 | 207 | 72.4 | 7.48 | 12.1 | 3，59 | 5.38 |
| 5 | 9.47 | S．13 | 5． 0 E | 50.4 | 8． 58 | 33 | 16 | 33 | 323 | 11.4 | 7.96 | 9．4 | 3.14 | 4.85 |
| $E$ | 18．8 | 8.39 | 5.64 | 43.4 | 3.42 | 39 | 1.8 | 47 | 853 | 125 | 7.47 | E．74 | 3． 015 | 4.82 |
| $?$ | 11.1 | Q，PE | 5.36 | 42.9 | 3.42 | 37 | 18 | 51 | 255 | 86.0 | $\overline{7}=42$ | 9.22 | 3.65 | 5.65 |
| 8 | 9.84 | 9.25 | 5.75 | 45.4 | 21.3 | 22 | 15 | ？ | 164 | 5 5．1 | 8.13 | 14．5 | $4 \times 86$ | 6.56 |
| 9 | 11．5 | 9.38 | 6.54 | 46.6 | 9.103 | 27 | 10 | 36 | 220 | 76．6 | 6.64 | 8． 13 | 4.16 | 6.38 |
| 10 | 12.1 | 19.6 | 7， 31 | 40.3 | 8.59 | 27 | 15 | 36 | 156 | 52.0 | 6.52 | 8，62 | 4.95 | 7.52 |
| 11 | 13.8 | 9.95 | 5.71 | 51.6 | 3．11 | 33 | 15 | 39 | 337 | 119 | 5.22 | 7．15 | 3.47 | 5.46 |
| 12 | 12．6 | 11.7 | 8.35 | 45 | 15.7 | 1 E | d | K2 | 135 | 40.2 | 5.32 | S． 6.6 | 5.39 | 8.07 |
| 13 | 14.6 | 12．6 | B．35 | 46.6 | 8．27 | 22 | 12 | 27 | 177 | 61.4 | 5.25 | 6.43 | 5.22 | 8.81 |
| 14 | 16.8 | 12.7 | 7．67 | 48.3 | 2．Es | 27 | 12 | 35 | 234 | S⿴囗 9 | 4.95 | 5.82 | 4.68 | 7.83 |
| 15 | 12． | 11.5 | 5． 48 | 89.6 | 25.8 | 15 | 18 | 16 | 366 | 137 | 5.21 | 6.75 | 3.34 | 5.24 |
| 16 | 14.3 | 13.7 | 9．57 | 47.8 | 20.2 | 15 | 16 | 18 | 127 | 44.7 | 5.35 | 5．68 | G． 11 | 9.21 |
| 17 | 16． 6 | 13.8 | 7.35 | 59.5 | 9.91 | 18 | 118 | 2 C | 276 | 161 | 4． | 5，12 | 4.47 | 7.01 |
| 15 | 17.8 | 15．0 | 9．${ }^{5}$ | 4 G .8 | 913 | 18 | 18 | 2 | 1.4 | 51．1． | 4.43 | 5，45 | 5.24 | 9.56 |
| 19 | 18．1 | 15.9 | 11.7 | 4 H .3 | 9．59 | 16 | 1080 | 24 | 104 | 34.7 | 4.34 | S．75 | 7.49 | 11.3 |
| 20 | 20.5 | 15.1 | 11.2 | 40.6 | 3.15 | $2 \%$ | 19 | 30 | 127 | 42.6 | 4.16 | 5.23 | 6.95 | 16.7 |
| 21 | 19.5 | $1{ }^{17} .3$ | 12．3 | 43.7 | 21.0 | 12 | E． | 158 | 81.3 | 28.8 | 4.39 | 5.79 | 8.37 | 12.4 |
| 22 | 21.6 | 18.1 | 11.6 | 48.7 | 8.49 | 15 | 8.6 | 12 | 135 | 47.3 | 3．E1 | 4.34 | 7． 21 | 11.1 |
| 23 | 24.1 | 18．6 | 11.4 | 48.2 | 3.15 | 18 | B．E | 22 | 155 | 53.7 | 3.39 | 4． 115 | 6.94 | 16.9 |
| 24 | 24.8 | 19.4 | 150 | 41．8 | \＃19 | 15 | 8， 2 | 24 | 111 | 37.1 | 苟37 | 4.24 | E． 21 | 12．7 |
| ＇25 | 21.4 | 20.0 | 14．${ }^{\text {c }}$ | 47.5 | 21．3 | 16 | $E .8$ | 128 | 84.0 | 29.6 | 3.75 | 4，71 | 6.77 | 13.5 |
| 26 | 25.4 | 23.3 | 15．5 | 44.7 | 9．7 | 13 | t． 8 | 159 | Q7．${ }^{7}$ | 36． | 3．63 | 3．80 | 9.76 | 14.8 |
| 27 | 29.0 | 22．2 | 13.1 | 49.9 | and | $1!$ | $E \cdot 8$ | 15 | 141 | 454. | 2．E2 | 3.28 | 7.95 | 12.5 |
| 23 | 26.4 | 24.7 | 17．8 | 4 E .1 | 21.7 | 8.3 | 5.6 | 16 | 63.1 | 22.1 | 3． 0.5 | 3．92 | 11．5 | 17．1 |
| 29 | 31．2 | 24.3 | 1709 | 48.6 | 91 | 1.14 | 5.6 | 125 | 59.3 | 31.4 | 二． 51 | 3.02 | 19．E | 16.4 |
| 36 | 34.9 | 27.4 | 17．6 | 46.1 | 354 | 12 | 5.5 | 159 | 93，0 | 31.9 | 3．72 | 2.80 | 10.8 | 16.8 |
| 31 | 391，6 | 28.7 | 20.4 | 47.2 | 23ッ | 6． 8 | 4． 7 | ． 25 | $55^{5}$ | 19．5 | 2．65 | 3.36 | 13.2 | 19.7 |
| $3 \%$ | ＊5．8 | 31.6 | 21.2 | 4E． 9 | 16．4 | 8.2 | 4.7 | $1{ }^{10} 6$ | 66．${ }^{1}$ | 23， | 2.13 | 2．61 | 130 | 2 c .4 |
| 33 | 40.3 | $32 \times 9$ | 19．2 | 49.7 | 3.81 | 19 | 4.7 | 129 | 93．4 | 32.7 | 1． 5 | 2.29 | 11.8 | 10.4 |
| 34 | 49．619 | 32.5 | 19.2 | 47.4 | 1． 可 $^{\text {a }}$ | 12 | 4.7 | 159 | 97.1 | 35.2 | 1.94 | 2.27 | 11．E | 18．3 |
| 35 | 37.0 | 34.8 | 25.1 | 45 | 23． | 5.6 |  | 5.94 | 43.7 | 15.3 | 2－21 | 른 6 | 15.2 | 24.2 |
| 36 | 42.8 | 37.7 | 24.5 | 48.6 | 10．है | 5.8 | 3.7 | 6.25 | 58.8 | 20.6 | 1.77 | 2.16 | 15.6 | 23.7 |
| 37 | 49.0 | 39.0 | 24.2 | $4 \mathrm{E}_{\text {，}}^{\text {E }}$ | 4．9E | 3．2 | 3. | 147 | 78.5 | 24.5 | 1.53 | 1.35 | 14.9 | 23.2 |
| 38 | 42.2 | 39.3 | ぞア | 48.5 | \％5，z | ¢ $\square_{0}$ | 3.3 | 5.6 |  | 14．4 | 1．94 | 2.48 | 17.3 | 26．9 |
| 39 | 49.7 | 44.5 | 30.6 | 47.1 | 11.8 | 5.6 | 3， 3 | 6.84 | $4 E .3$ | 16.2 | 1.58 | 1．88 | 18.9 | $2 \mathrm{EB}$. |
| 45 | 56.7 | 45.7 | 28．1 | 4.43 | 4．58 | 5.8 | 3.3 | 8.25 | 51，5 | 21.5 | 1．3E | 1． 69 | 17.3 | ご． 3 |
| 41 | 67.3 | 45.8 | 25－4 | 49.3 | 1． 5 ¢ | B．${ }^{\text {er }}$ | 3．3 | I． 1.0 | 7 | 纪以 ${ }^{\text {为 }}$ | 1.86 | 1．5．7 | 15.9 | 25.2 |
| 42 | 53.2 | 19.9 | 35.5 | 4 4 .3 | 23.3 | 3.9 |  |  |  |  | 1.53 | 1.94 | 22.8 | 34.2 |
| 43 | 51.2 | $5 \% .9$ | 34.8 | 49.2 | 14． | 4.7 | 2. | 5.6 | 43.3 | 15.3 | 1．2S | 1． 48 | 21.8 | 33.4 |
| 4.4 | 69.9 | 561 | 34.8 | 48.4 | 4.41 | 5.5 | 2.7 | E゙ィ 4 | 49 | 17．1 | 1．13 | 1．34 | 21.4 | 330 |

FILTER CHARACTERISTICS AND DESIGN FORMULAS
Band-Pass Sections
Fundamental Felations
$f_{1}=$ lower frequency limit of pass $\quad f_{2}=$ higher frequency limit of pass
a
$f_{100}=a$ frequency of very high attenuation in low-frequency attenuating band $f_{2 \infty}=$ a frequency of very high attenuation in high-frequency attenuating band

$$
\left(f_{2}^{\prime}-t_{1}\right)
$$

$R=$ load resistance
Design of Sections
band

$$
c_{1 k}=\frac{f_{1}-f_{1}}{4 \pi f_{12} R}
$$

$$
C_{2 k}=\frac{1}{\pi\left(t_{2}-f_{1}\right)^{R}}
$$

| Type | Atmuation |  |  | B. Fillers hiving ritatermelisto kectione |  | Notzion for beat T and x section |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |
| 1 |  |  |  |  | $\begin{aligned} & L_{1}=\frac{L_{-k}}{b} L_{n^{\prime}}=\frac{L_{n}}{d} \\ & L_{1}=\frac{L_{1}}{m_{3}} C_{1}=a C_{4} \\ & C_{1}^{\prime}=C_{2} \\ & C_{1}=m_{1} C_{4} \end{aligned}$ |  |
|  |  | $\xrightarrow{2 L_{1}^{2}-4 L_{1}^{2}}$ |  | $x^{1} c^{\frac{1}{2}}$ |  |  |
|  |  |  |  |  |  |  |


|  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 콥ㅋํ <br> 110 ज5NT | 年落 |  |  |  |  |
|  |  |  | $\begin{aligned} & \text { Sume drcuit as abovo } \\ & \text { for Type Y } \end{aligned}$ |  |  |  |
|  | जึ जैื 1111 ज． |  |  |  | 5 气密 |  |
|  |  |  |  | 开 |  |  |
|  | cogmudry |  |  |  |  |  |
|  |  | $=1$ |  | $\begin{aligned} & \circ \\ & \mathrm{B}^{\circ} \\ & \hline \end{aligned}$ | Ei |  |

## COMB-FILTER DESIGN

Comb filters consist of a chain of narrow-band filters which pass spectral lines over the frequency spectrum of the signal. They pass discrete frequency components and discriminate against noise. Such filters are used to separate a composite input signal into a number of channels before data processing in telemetry systems and radar. The spacing between channels may be expressed as a frequency ratio which depends on the number of channels needed to coverone octave, or " $n$." Thus $f / f_{c}=2^{n}$, where $f_{c}$ is the reference, $f$ is the unknown frequency of the adjacent channel, and $n$ is any positive or negative real number. For $n= \pm 1$, $f$ equals $2 f_{c}$ and $1 / 2 f_{c}$. These values are the center frequencies of channels, one octave away from the reference frequency.

The nomogram solves for positive or negative iractional values of $n$. The frequency scales, $f_{c}$ and $f$, are normalized so that the nomogram can be used for any frequency by shifting the decimal point. The ratio scale, $n$, has a decimal range as well as fractional values.

To use the nomogram, place a straight-edge from the octave fraction or decimal on the $n$ scale to the reference frequency on the $f_{c}$ scale. Read the center frequency of the next channel on the $f$ scale. Hold the $n$-scale value as a pivol point and shift the straight-edge to the same frequency on the $f_{c}$ scale as the first answer. Fead the next bandpass center frequency on the /scale. Continue the process until all center frequencies are obtained. For negative $n$ values, divide the relerence frequency by two to obtain the lower octave. After this step, proceed as for a positive $n$ value.

FOR EXAMPLE: Calculate the center frequencies for $1 / 3$ octave filters, starting at 100 Hz (see illustration).
Set the straight-edge from $1 / 3$ or 0.33 on the $n$ scale to the one (for 100 Hz ) on the $f_{c}$ scale and read 1.26 on the $f$ scale; the center frequency of the next channel bandpass filter is 126 Hz . Fivot at $1 / 3$ on the $n$ scale and shift the straightedge to 126 on the $f_{c}$ scale. Read 160 Hz on the $f$ scale. When $1,260 \mathrm{~Hz}$ on the $f$ scale and 1,000 Hz on $f_{c}$ is reached, shift back to the lower portion of the $f_{c}$ scale and continue.


Pulse-forming networks supply high-voltage pulses to magnetrons and lasers. This nomogram relates the pulse width and characteristic impedance to the network's inductances and capacitances. It is based on the formulas:

$$
\begin{aligned}
Z_{0}=\sqrt{\frac{L}{C}} ; P_{w} & =2 n \sqrt{L C} \\
n & =\frac{P_{w}}{2 r}
\end{aligned}
$$

where $Z_{0}=$ characteristic impedance
$i=$ inductance per section
$C=$ capacitance per section
$n=$ number of sections
$P_{w}=$ pulse width
$r=$ rise time
FOR EXAMPLE: Designa PFN that delivers a $4-\mathrm{kV}, 500-\mu \mathrm{sec}$ pulse with a $25-\mu \mathrm{sec}$ rise time into a 1 -ohm load: The numbers of sections ( $\mathrm{P}_{\mathrm{w}} / 2 r$ ) is 10 . Connecting 1 ohm to $500 \mu \mathrm{sec}$ on the lelt and right scales yields $250 \mu \mathrm{~F}$ and $250 \mu \mathrm{H}$ as total capacitive $\mathrm{C}_{N}$ and total inductance $L_{N}$. Dividing by 10 gives $25 \mu \mathrm{~F}$ and $25 \mu \mathrm{H}$ per section. The two end inductances are 1.15 the value of each section or $2.875 \mu \mathrm{H}$.


A pulse applied to the input of a delay line is continuously delayed by a predetermined amount as it travels along the line. The artificial or lumped parameter type of delay line consists of a series of low pass LC filters. The delay for $n$ sections is given by the formula

$$
t=n \sqrt{L C}
$$

$$
\begin{aligned}
\text { where } t & =\text { time delay in microseconds } & L & =\text { inductance in microhenries } \\
n & =\text { number of sections } & C & =\text { capacitance in microfarad }
\end{aligned}
$$

The characteristic impedance $Z_{0}$ must be matched to reduce reflections within the delay line and is given by the formula

$$
z_{0}=\sqrt{L C}
$$

where $Z_{0}$ is in ohms
The cutoff frequency of each section must be higher than the operating frequency $f_{c}=\frac{1}{\pi \sqrt{L C}}$
where $f_{c}$ is the cutoff frequency in megahertz
FOR EXAMPLE: Determine the parameters for a delay line with a $1.5-\mu \mathrm{sec}$ delay and an $f_{0}$ of 5 MHz . Pivot around 5 MHz on scale 2 and select standard values of $L$ and $C$ on scales $\boldsymbol{I}$ and 4. ( $120 \mu \mathrm{H}$ and 33 pF ) The cutoff frequency on scale 2 corresponds to the time delay per section shown on scale 3-in this case $0.063 \mu \mathrm{sec} /$ section. The time delay per section aligned with the required total delay ( $1.5 \mu \mathrm{sec}$ ) on scale 5 shows the total number of sections required as 24 on scale 7. The characteristic impedance of the line is found to be 1,900 ohms as shown on scale 6 by aligning $C(33 \mathrm{pF})$ on scale 5 , with the previously selected value of $L(120 \mu \mathrm{H})$ on scale 8 .


This nomogram solves for the delay per foot as well as the lotal delay of a coaxial cable when the relative dielectric constant of the insulation is known. The nomogram is based on the relationship

$$
T=1.108 \sqrt{E} \text { nsec } / \mathrm{t}
$$

The relative dielectric constant and delay per foot are plotted on the left-hand index and can be related directly. The chart gives the approximate ranges of dielectric constants of commonly used insulating materiais. Some dielectric properties are a function of composition, frequency, and temperature, and the values shown should be used accordingly.

FOR EXAMPLE: A 4-ft cable with a polystyrene dielectric will produce a total delay of about 6.3 to 6.5 nsec .

DIELECTRAC CONSTANTSDIELECTRAC CONSTANTS
Bakelite ${ }^{1}$........................................................... 95
Fluasinated eitylena propylente ..... 2.2
itrodiated polyethrice. ..... 2.1
Luelto. ..... 2.7
Maqnagiviun axidy $^{\text {. }}$ ..... 4.9
Nyion. ..... 1.0
Polyathylens ..... $2.25-2.32$
Polysiyrene ..... 2.4-2.6
Polyleitrofluarsathylent. ..... 2.0.2. 3
Polyurelhane ..... 6.4.7.6
Polyvinylethloide (nsmel qid) ..... 7.0
Rubber (malural), ..... 2.4-4.6
Rubber (silitione) ..... 2.9-3.7
if Tw Union Coblida Corp
2.TMarent

VOLTAGE MULTIPLIER CFRCUITS
Circuit diagrams are given and the minimum voltage ratings of the capacitors are shown as related to $V_{m}$. The minimum PIV of the diodes is $2 V_{m}$.



FUll-wave voltage tripler



FULL-WAVE VOLTAGE OUADFUPLER


HALF-WAVE VOLTAGE OUADRUPLER


## POWER TRANSISTOR AND DIODE REQUIREMENTS FOR SWITCHING POWER SUPPLIES

This tabulation shows the transfer function, switching transistor currents and voltages, diode currents and voltages as well as voltage and current waveforms for ten different converter circuit configurations used in switching power supplies.

The advantages and disadvantages of each circuit configuration are also given.


|  |  |  |
| :---: | :---: | :---: |
|  | $\stackrel{\text { (®) }}{\text { FLreack }}$ |  |
|  |  | $\frac{V_{0}}{V_{1 H}}=\frac{w_{2}}{N_{1}}\left(\frac{1}{T}\right)$ |
|  |  |  |
|  | $v_{\text {cro }}>v_{\text {UH }}+\left(\frac{\mathrm{HE}}{\mathrm{Hz}}\right) \mathrm{v}_{\text {cut }}$ | $v_{\text {ceo }}>v_{\text {w }}\left(1+\frac{\text { mid }}{43}\right)$ |
|  | $I_{\text {chi }}=I_{\text {mt }}$ | $\begin{aligned} & I_{\text {CR1 }}=\frac{\hat{I}_{\text {man }}}{Z}\left(\frac{T}{T}\right) \\ & I_{\text {Chz }}=I_{\text {mL }}\left(\frac{T}{T}\right) \\ & I_{\text {Ch3 }}=I_{\text {ma }}\left(\frac{T-T}{T}\right) \\ & \hline \end{aligned}$ |
|  | $v_{\text {PH }}+\gamma_{\text {IN }}\left(\frac{\mathrm{N}_{2}}{\mathrm{~N}^{\prime}}\right)$ | $\left.\begin{array}{l} v_{C N 1} \cdot v_{1 H}\left(1+\frac{N B}{N 1}\right) \\ v_{C H 2}+v_{A H}\left(\frac{N 2}{N 3}\right) \\ v_{C A 3} \cdot v_{1 H}\left(\frac{N 2}{N 1}\right) \end{array}\right\} v_{\text {AH }}$ |
|  |  |  |
|  | shate. NuLTPIE CuTputs the possber gulector cumafint recuceo dy tumas ratio of trans ifotmer low pahts conit. Isolation. | Simple, melitile outputs are possible. collectra cuarent hequceo br ratio of $\frac{\mathrm{Ne}}{\mathrm{Ni}}$ Low output ripple. |
|  |  | POOA TRAKETORMER UTLLIZATION. PGOA TRAKSIEIT RESDOMSE. parts count mitm. thansformer desicn is critical. |

AHD CURRENT RATINGS EE INCREMSED TO $125 \%$ OF THE REQUIRED MAXIMUM.

 TO T2S\% OF THE REOUIRED MAXIMUM.

|  |  |  |
| :---: | :---: | :---: |
| ( -PUSH-PULL | ćun tooost - - buck invertinch | Cux (with TAMMsFormert |
| $\frac{\mathrm{V}_{0}}{\mathrm{~V}_{1 \mathrm{~W}}} \times 2 \frac{\mathrm{~N} 2}{\mathrm{NT}}\left(\frac{\mathrm{T}}{\mathrm{T}}\right)$ | $\left.\frac{V_{0}}{V_{1 M}} \cdot\left(\frac{r}{T-r}\right) \quad 1-1\right)$ | $\frac{Y_{0}}{v_{\text {m }}}=\frac{T}{T-2}, 0 \cdot \frac{1}{T}, 0 \leq 0 \leq 1$ |
| $I_{C \text { max }} \times \frac{N / 2}{N I}\left(I_{\text {RG }}+\frac{\Delta I_{\text {Ll }}}{2}\right)+\dot{I}_{\text {mag }}$ | $I_{6 \text { Max }}+I_{1}+I_{2}=I_{1}\left(\frac{T}{7}\right)$ |  |
|  |  |  |
| $\begin{aligned} & I_{C F 1}+\frac{I_{m L}}{2} \\ & I_{C A 2}+\frac{I_{R L}}{2} \end{aligned}$ | $\begin{aligned} & I_{G G_{1}} \cdot I_{1}+I_{2} \\ & I_{1}+I_{E} \cdot I_{1}\left(\frac{T}{T}\right) \end{aligned}$ | $\mathrm{I}_{\mathrm{CHI}} \cdot 1.5 \mathbf{1}_{\mathrm{HLL}}$ for 0.4 .33 <br>  <br>  |
|  | $V_{0}$ * 1 | $\begin{array}{r} 1.5 v_{\text {IN }} \text { FDR }=-33 \\ 2 v_{\text {WI }} \text { FCR } 0=.50 \\ 25 v_{\text {IN }} \text { FOR } D=.60 \end{array}$ |
|  |  |  |
|  CDELECTOR CUMAENT REDUCED AS A FUNGTION OF $\frac{\mathrm{HZ}}{\mathrm{Ni}} .6000 \mathrm{AT}$ LOW wilues OF $\mathrm{V}_{\mathrm{IH}}$. | COHTINUCUS INPUT AMO OUTPUT CURAENT, MIGHEST EFFICIENCT, LOW RIPPLE. SNALLEST MUMBER OF SwICHINC COMPOREMTS. Smichinc losses cit in half, dive cimeut referezeeo to emond Hightist ofgratime frcouency. |  LDW RIPME, SWLLLEST NUMEER OF SWITCHING COWPONENTS, 5 WITCHANG cossts ow, orive current meferenceo To groumo mighest OPERATHAC FREOUENCY. |
| Choss comillition of ol ca possicle miti Parts COUNT, TRANSFORMEI DCSHEN CRTTICNL. PODR DYMAMC AANCE. POCF TRANSENI RESPONSE. | HLGH COLLECTOR CURREHT, CI HAS MIGH RIPPLE <br>  FOR QLI POWER OUTPUT LIMITED, |  desige chifical. power output is limited. |

(From General Electric Application Note 200.87, "Power Transistor Applications for Switching Regulators and Motor Control," copynighted by and reprinted with permission of General Electric Company.)

The percent regulation of a power supply is found by the change in output voltage between Full Load and No Load voltage as given by the formula:

$$
\text { \% regulation }=\frac{\text { No Load Voltage }- \text { Full Load Voltage }}{\text { Full Load Voltage }} \times 100 .
$$

## FOR EXAMPLE:

1. What is percent regulation if No Load Voltage is 500 V and Fufl Load Voltage is 492 V ? The difference is 8 V. Answer: Connecting 492 and 8 gives a regulation of about $1.6 \%$.
2. For $0.04 \%$ regulation what is maximum allowable change in output voltage if required Full Load Voltage is 15 V . Answer, 0.006 V .


## POWER LOSS DUE TO IMPEDANCE MISMATCH

This chart shows the power loss resulting from inequality in the absolute magnitude of two impedances connected so as to transfer power from one to the other. The figures on the curves are the number of degrees of algebraic phase difference between the two impedances.

FOR EXAMPLE: Find the resulting power loss when a loudspeaker with an impedance of 10 ohms and a phase angle of $60^{\circ}$ is fed from a generator with a $100-\mathrm{hm}$ internal impedance. The impedance mismatch ratio is 10:1, and at the $60^{\circ}$ line the loss due to mismatch is read as 5.7 dB .


A bridge consists essentially of four arms connected in series and so arranged, that when an electromotive force is applied across one pair of opposite junctions, the response of a detecting and /or indicating device connected between the outer pair of junctions may be zeroed by adjusting one or more of the elements of the arms of the bridge. Seven commonly used bridge circuits and their balance equations are shown.


This nomogram is used to find the eflective resistance of resistors connected in parallel or the capacitance of capacitors connected in series. The range of the nomogram may be extended by multiplying the three scales by the same factor $10^{n}$, where $n$ may be positive or negative.

FOR EXAMPLE; (1) The effective resistance of a 150 k and 120 k resistor in paraliel is 67 k . (2) A $6.3 \mu \mathrm{f}$ and $5.6 \mu \mathrm{f}$ capacitor connected in series present an effectlve capacitance of $3 \mu \mathrm{~F}$.

(From "Parallet-Resistance Charl," EDN, September 14, 1966 by permission of EDN.)

## Section 4

# Active Components and Circuits 

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| MANE OF DEvick | CIMCUIT <br> SYMDOE． | COMMONLY USED Jいइetmon SCHEMATIC． | ELECTRLCAL MIARACTEAUSTICS | MA．OR APかもCATIONS | $\begin{aligned} & \text { MOLGHIY } \\ & \text { ASALOCOUS } \\ & \text { TO: } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Oroda <br> or <br> Reetiliur |  |  |  | nect）fiention <br> Bockink <br> Geiteling <br> sterfing | Cherek ，alve <br> Diode tube <br> Gas alloble |
| Avalenthe （Zener） Drocte |  |  | Constopt voltage characieribicic In negative quadrant | Fegulation <br> Relerence <br> Clipping | V －fl lide |
| Iategrated Voltoge Aegetator 4VA） |  |  | Programmed to dichired $\mathrm{V}_{21}$ by ine residtury | Slater volunge regulator <br> Reference element <br> Error mokitfier <br> Level zensing <br> Level shifting | Avalanche Diade |
| Tunnel Diode | POSATFE ELECTRODE SEGATIVE EI．ECTRODE | POSITIVF． Electrode： <br> NEGATIVE EJ，YCTRODF |  <br> Diatilay magntue Pdalatince athen current exeusede reak fiolnt curreal $\mathbf{L}_{\mathrm{p}}$ | Wha converter <br> 1－ARicelteults <br> Mucrosive cireulis <br> lievel mennlig | None |
| Back <br> Ulode | ANODE： <br> CATHODE |  | Simider ctaracterfstics 10 conventhona！diode etcepe rery fow farmard voltane drap | Micromave maixers and Iow poser cosciflatars | None |


| NAME OF DFVICE | circutr sYmbor. | COMMONI.Y USED sunctron schematic | El.ECTRJCAL ctaracterustica |  | Mandor <br> APPLICATIONS | notronly <br> ana logerth T0: |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Thyrector |  |  |  | Fiaptaly increasing cargeal abowe rated voltugn in eñher cirrection | Trazaient voltage suppresilen zod arre suppresalon | Thyrste <br> Tvo nualanche diodes In inverse-serieq connection |
| $\begin{aligned} & \text { q-p-п } \\ & \text { Trnnululer } \end{aligned}$ |  |  |  | Constank enflector tusrent for glven base Jrive | Amplitizatico <br> Swelceking <br> Oxillartom | Pentexic Tuther |
| $\begin{aligned} & p-n-11 \\ & \text { Tranulkior } \end{aligned}$ |  |  |  | Complement to n-p-n transisfur <br> neciom (-) | Amplitication <br> 5wetching <br> Osciltationt | None |
| Phata「ransiator |  |  |  | theident leyht pecto 25 base curtent of U.e photn transivtar | Tape reaklers <br> Cand readers <br> Prozition bemas <br> Tachometere | None |
| Unijumetion Translskur ( HJT 7 |  |  |  | Unijumettion eatilict Dlocks umis its rohtige reacter $\mathrm{V}_{1} \mathrm{p}$. 1amen comeliets | tateryal turaing Osciatation fiswl leycetor SCH Trleget | Nuns |


| KAME OH DE.VICK: | ctitelit stislag. |  JUNC7H5* SCIF:NATATIS | F.L.ECTRKCAL, ©HARACTEIELSTICS | MASOR AP"LICATHONS |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Complementary <br> Unijutsetion <br> 'riansistot <br> (CLEST) |  |  | Functional cimplement to CJS | ling suablity strices <br> Ghitallators and theel de-kedors | Nuse |
| Progrimathatile <br> (Jut)westion <br> Trangletor IPUT) | CATIMODE |  | Programmed by two Peblstora for ${ }^{\prime} p$ p 'p, $1_{y}$. Function equivalent to normal UJT. | I. ow cost timers sud aseillators <br> Laug perbext llmers <br>  <br> Luvel derfectar | UJT |
| Silicen <br> Controlied Restifier (5CR) |  |  |  | Pawece mwitchalk <br> lithate condiol <br> laveriers <br> Choppers | Gay thyratrolt or Iysutron |
| Complementary <br> Sllison <br> Controlles <br> Fiectuber <br> (CSCl? | ANODE <br> CATHODE |  | $\xrightarrow{\text { 4NOOL }}$ | Bing countera <br> Lurw speed logle <br> Litmindeiver | Nent |
| Ligte Activated SCR" (LAECR) | CATHOD: |  | Ojerates stmilar to SCR, except can nisa be trigatered inta condubition by light falling on Junctions | Felay Replacement <br> Porltion eontrol: <br> Phoremeletris applicativna <br> Sluxe flashea | Nooe |


| NAME OF DEvice | circurt <br> SYMBOL | COMMONEY LSED JURETMOs SCHEMATLC | Finictrical．Cit | ARACTERISTICS | MASOR <br> APIMICATIONS | ROUGHLY ANALOCOHS 70： |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Stleon <br> Controlled 5 witch ${ }^{\prime}$ ［5CS |  |  |  | Orerates similar to SCf except tata misn be trugtuered an ly a nerative sulynal mot ancode－gnte．Also severat other specializet maxles of uperation | Logic appleations <br> Counter is <br> Nixde 小rlver＇s <br> Lamp divers | Conpplemestars armsistor pair |
| Silletan <br> Unitateral <br> Switeh <br> （SUS） | CATHODE | Ancoet <br> CATJROUE： |  | Simifiar to SCS lxat aener atdded to noode pate to tripger device Into eon－ duethon at $\sim$ 白 volts．Can albo be triegered by neghtive pulse the gate lead． | Switching Clrevilts <br> Comature SCR Trlater Oacellator | Envelley ${ }^{\text {or }}$ A－layer dfunde： |
| Silleon <br> BElateral <br> Switeh <br> ［SDBS | ANOGE 1 |  |  | Symimetrical bilateral veradon oll the Sl ＇S．Breaks down in both directions as suss does in torwiand． | Switehtar Clreuta Countera TRIAE Plase Contral | Two laterse Ehuchleg difores |
| Truct | ANODE 1 | 9んで <br> ANODE I |  | Operates slsuilitr Io SCR except can be stickered into conilugkan in ahher dirndidun by $\{+1$ ar $\{-\}$ taie alymal | AC awthehlng <br> Phase control <br> golay ruplacement | Two SCA＇s 5：finterwe parullel |
| Dise <br> Friges |  |  |  | When wolky reghter tricgur lavel tinbout 3k volth），abruptly swhethes down about 10 volta． | ```Trhae and SER itignt Omelitalor``` | Neont lamp |

Table 1: General Semiconductor Symbols

| $I, i$ | region of a device which is intrinsic and in which neither holes not electrons <br> predominate |
| :--- | :--- |
| $N_{i}, n$ | region of a device where electrons are the majority carriers |
| $N F$ | noise figure |

Table 2: Signal Diode and Rectifier Diode Symbols

| $V_{\text {(BA) }}$ or $V_{\text {(BA) }}$ | reverse breakdown voltage, dc |
| :---: | :---: |
| $v_{(B R)}$ or $v_{\text {(GRIR }}$ | reverse breakdown voltage, instantaneous total value |
| $I_{F}$ | torward cursent. dc |
| /fiav) | forward current. average value |
| $i_{\text {F }}$ | forward current, instantaneous total value |
| $I_{1}$ | forward current, rms value of alternating component |
| /FiRMS) | forward current, rms total value |
| /fm | forward current, maximum (Deak) total vafue |
| $t_{\text {FM }}$ (rop) | forward current, repetitive, maximum (peak), total value |
| ${ }^{\text {I }}$ M M(wiga) | forward current, maximum (peak), total value of surge |
| \% | output current, average rectified |
| $f_{\text {A }}$ | reverse current, do |
| $i_{\text {\% }}$ | reverse current, instantaneous total value |
| $J_{\text {R(AV) }}$ | reverse current, average value |
| $/_{\text {RM }}$ | reverse current, maximum \{peak) total value |
| $t_{\text {r }}$ | reverse current, ims value of alternating component |
| /R(RMS) | reverse current, ims total value |
| $L_{c}$ | conversion loss (microwave diodes) |
| $P_{F}$ | forward power dissipation, dc |
| $P_{\text {F }}($ AV) | forward power dissipation, average value |
| $P_{\text {FM }}$ | forward power dissipation, maximum (peak) total value |
| $\rho_{\text {F }}$ | forward power dissipation, instantaneous total value |


| $P_{\text {A }}$ | reverse power dissipation, dc |
| :---: | :---: |
| $P_{\text {R(AV) }}$ | reverse power dissipation, average value |
| $\rho_{\text {RM }}$ | reverse pawer dissipation, maximum (peak) total value |
| $\rho_{R}$ | reverse power dissipation, instantaneous total value |
| $V_{F}$ | forward voltage drop, dc |
| $V_{F}$ | forward voltage drop, instantaneous total value |
| $V_{\text {Flav }}$ | forward voltage drop, average value |
| $V_{\text {FM }}$ | forward voltage drop, maximum (peak) total value |
| $V_{\text {fiRMS }}$ | forward voltage drop, total rms value |
| $V_{1}$ | forward voltage drop, rms value of alternating component |
| $V_{R}$ | reverse voltage, $d c$ |
| $V^{\prime}$ | reverse voltage, instantaneous total value |
| $V_{\text {R(AV) }}$ | reverse voltage, average value |
| $V_{\text {RM }}$ | reverse voltage, maximum (peak) total value |
| $V_{\text {RM }}$ (wivg) | working peak reverse voltage, maximum (peak) total value |
| $V_{\text {RM }}$ (ripl ${ }^{\text {a }}$ | repetitive peak reverse voltage, maximum (peak) total value |
| $V_{\text {fiminoticep }}$ | nonrepetitive peak reverse voltage, maximum (peak) total value |
| $V_{\text {f(RMS })}$ | reverse voltage, total rms value |
| $V$, | reverse voitage, rms value of aiternating component |

Table 3: Transistor Symbols

| $B V_{\text {CBO }}$ | obsolete-see $V_{\text {Igricao }}$ |
| :---: | :---: |
| $8 V_{\text {ceo }}$ | obsolete-see $V_{\text {(briceo }}$ |
| $B V_{\text {CER }}$ | obsolete-see $V_{\text {(BAICEA }}$ |
| $B V_{\text {ces }}$ | obsolete-see $V_{\text {(ar)ces }}$ |
| $B V_{\text {cex }}$ | obsalete-see $V_{\text {(raricex }}$ |
| $8 V_{\text {Ebo }}$ |  |
| $8 V_{\text {¢ }}$ | obsolete-see $V_{\text {(talR }}$ |
| $C_{\text {ibo }}$ | open-circuit input capacitance, common base |
| $C_{i b s}$ | short-circuit input capacitance, common base |
| Cioo | open-circuit input capacitance, common emitter |
| $C_{\text {ies }}$ | short-circuit input capacitance, common emitter |
| $C_{060}$ | open-circuit output capasitance, common base |
| $C_{\text {obs }}$ | short-circuit output capacitance, common base |
| $C_{\text {O®O }}$ | open-circuit output capacitance, common emitter |
| $C_{\text {oss }}$ | short-circuit output capacitance, common emitter |
| $f_{\text {hfb }}$ | small-signal short-circuit forward current transfer ratio cutoff frequency (common base) |
| forc | small-signal short-circuit forward current transfer ratio cutofi frequency (common collector) |
| $f_{\text {hfe }}$ | small-signal short-circuit forward current transfer ratio cutoff frequency (common emitter) |
| $f_{\text {max }}$ | maximum frequency of oscillation |
| $f_{\text {T }}$ | frequency at which small-signal forward current transfer ratio (common emitter) extrapolates to unity |
| $g_{\text {ME }}$ | static transconductance (common emitter) |
| $g_{\text {me }}$ | small-signal transconductance (common emitter) |
| $G_{\text {PB }}$ | large-signal average power gain (common base) |
| $G_{\text {pb }}$ | small-signal average power gain (common base) |
| $G_{P C}$ | large-signal average power gain (common collector) |
| $G_{p c}$ | small-signal average power gain (common collector) |
| $G_{\text {PE }}$ | large-signal average power gain (common emitter) |
| $G_{\text {po }}$ | small-signal average power gain (common emitter) |

$h_{\text {fo }} \quad$ small-signal short-circuit forward current transfer ratio (common base)
$h_{\mathrm{FC}}$
$h_{\mathrm{it}} \quad$ small-signal short-circuit forward current transfer ratio (common collector)
$h_{\text {FE }}$
$h_{\text {fo }}$
$h_{18}$
$h_{16}$ small-signal short-circuit input impedance (common base)
$h_{\text {IC }} \quad$ static input resistance (common collector)
$h_{\text {ic }} \quad$ small-signal short-circuit input impedance (common collector)
$h_{\text {IE }} \quad$ static input resistance (common emitter)
$h_{\text {in }} \quad$ small-signal short-circuit input impedance (common emitter)
$h_{\text {ob }}$ small-signal open-circuit output admittance (common base)
$h_{o c} \quad$ small-signal open-circuit output admittance (common coltector)
$h_{0} \quad$ small-signal open-circuit output admittance (common emitter)
$h_{r}$
$h_{r c} \quad s m a l l-s i g n a l$ open-circuit revarse voltage transfer ratio (common collector)
$h_{r e} \quad s m a l l-s i g n a l$ open-circuit revarse voltage transfer ratio fcommon emitter)
/B base current, dc
Ib base current, rms value of aiternating component
保

## leev

leex
tces
loss
/E

1. emitter current, rms value of alternating component
tebo
$P_{\text {EE }}$
$\rho_{\text {BE }}$
$P_{\mathrm{CE}}$
PCB power input (instantaneous total) to the collector (common base)
$P_{\text {Ce }} \quad$ power input (dc) to the collector (common emitter)
$\rho_{\mathrm{CE}} \quad$ power input finstantaneous total) to the collector (common emitter
$P_{E B} \quad$ power input (dc) to the emitter (common base)
$\rho_{\text {EB }} \quad$ power input (instantaneous totall) to the emitter (common base)
$P_{\text {旧 }} \quad$ large-signal input power (common base)
$D_{i b} \quad$ small-signal input power (common base)
Pic large-signal input power (common collector)
$p_{\mathrm{is}} \quad$ smald-signal input power (common collector)
$P_{I E} \quad$ large-signal input power (common emitter)
$\rho_{\text {io }} \quad$ small-signal input power (common emitter)
$P_{\text {os }} \quad$ large-signal output power \{common base\}
$p_{\text {ob }}$ small-signal output power (common base)
Poc large.signal output power (common collector)
$p_{\text {oc }} \quad$ small-signal output power (common collector)
Poe large-signal output power (common emitter)

| $\rho_{\text {of }}$ | small-signal output power (cammon emitter) |
| :---: | :---: |
| $\boldsymbol{P}_{\text {T }}$ | total nonreactive power input (dc) to all terminals |
| $\rho_{T}$ | nonreactive power input (instantaneous total) to all terminals |
| $R_{B}$ | external base resistance |
| $R_{c}$ | external collector resistance |
| $r_{\text {CEist) }}$ | collector-to-emitter saturation resistance |
| $\boldsymbol{R}_{\mathbf{E}}$ | external emitter resistance |
| Fei $\mathrm{h}_{1+}$ ) | real part of the small-signal short-circuit input impadance (common emitter) |
| $V$ (ericbo | breakdown voltage, collector-to-base, emitter open |
| $V$ (ba)ceo | breakdown voltage, collector-to-emitter, base open |
| $V$ (bricef | breakdown voltage, collector-to-emitter, with specified resistance between base and emitter |
| $V_{\text {(batces }}$ | breakdown voltage, collector-to-emitter, with base short-circuited to emitter |
| $V$ tearcex <br> $V_{\text {ibaligeo }}$ | breakdown voltage, collector-to-emitter, with specified circuit between base and emitter breakdown voltage, drain-to-gate, saurce open |
|  | breakdown voltage, emitter-to-base, collector open |
| $V_{\text {(BA) }}$ | breakdown valtage, reverse |
| $V_{B B}$ | base supply voltage |
| $V_{\text {BC }}$ | base-to-collector voltage. dc |
| $V_{\text {bc }}$ | base-to-collector voltage, rms value of alternating component |
| $v_{\text {bc }}$ | base-to-collector voltage, instantaneous value of ac component |
| $V_{\text {ge }}$ | base-to-emitter voltage, dc |
| $V_{\text {b }}$ | base-to-emitter voltage, rms value of alternating component |
| $v_{\text {b* }}$ | base-to-emitter voltage, instantaneous vatue of ac component |
| $V_{\text {CB }}$ | collector-to base voltage, dc |
| $V_{c b}$ | collector-to-base voltage, ims vatue of alternating component |
| $V_{\text {col }}$ | collector-to-base voltage, instantaneous value of ac component |
| $V_{\text {ca(1) }}$ | dc open-circuit voltage (floaking potential) between the collector and base, with the emitter biased with respect to the base |
| $V_{\text {cc }}$ | collector supply vaitage, dc |
| $V_{\text {CE }}$ | collector-to-emitter voltage, de |
| $V_{c e}$ | collector-to-emitter voltage, rms value of alternating component |
| $v_{\text {ce }}$ | collector-to emitter voltage, instantaneous value of ac component |
| $V_{\text {cef }}$ fil | dc open-circuit voltage (flozting potential) between the collector and emitter, with the base biased with respect to the emitter |
| $V_{\text {CEO }}$ | collector-to-emitter voitage, dc, with base open |
| $V_{\text {CEO }}$ (av) | collector-to-emitter (breakdown) sustaining voltage with base open |
| $V_{\text {CER }}$ | collector-to-emitter voltage, dc with specified resistor between base emitter |
| $V_{\text {CER }}$ (wis) | collector-to-emitter (breakdown) sustaining voltage with specified resistor betweer base and emitter |
| $V_{\text {CES }}$ | collector-to-emitter voltage, dc with base short circuited to emiter |
| $V_{\text {cestsua) }}$ | collector-to-emitter (breakdown) sustaining voltage with base short-circuited to emitter |
| $V_{\text {CEX }}$ | collector-to-emitter voltage, dc with specified circuit between base and emitter |
| $V_{\text {CEX (ws) }}$ | collector-to-emitter (breakdown) sustaining voltage with specified circuit between base and emitter |
| $V_{\text {cetat) }}$ | collector-to-emitter ssturation voltage, dc |
| $V_{\text {e }}$ | ernitter-to base voltage, dc |
| $V_{\text {E日 } \text { dfl }^{\text {d }} \text { ) }}$ | dc open-circuit vollage floating potentiall between the emitter and base, with the collector biased with respect to the base |
| $V_{\text {ob }}$ | emitter-to-base voltage, rms value of alternating component |
| $v_{\infty}$ | emitter-to-base voltage, instantaneous value of ac component |
| $V_{E C}$ | amitter-to-collector voltage, dc |

```
VEc(f|) dc open-circuit voltage (floating potential) between the emitter and collector, with the
    bose biased with respect to the collector
V ec emitter.to-collector voltage, rms value of alternating component
Vece emitter-to-collector voltage, instantaneous value of ac component
V EE emitter supply voitage
V rt reach-through valtage
```

Table 4: Tunnel Diode Symbols
$t_{1}$ inflection point current
$f_{p}$ peak point current
Iv valley point current
$f_{i}$ dynamic resistance at inflection point
$V_{\text {Pp }}$ projected peak point voltage
(forward voltage point (greater than the peak voltage), at which the current
is equal to the peak current]
$V_{1}$ inflection point voltage
$V_{\mathrm{p}}$ peak point voltage
$V_{V}$ valley point voltage

## Typical Characteristics



| Characteristic | $\begin{aligned} & \text { Vacuum } \\ & \text { Tube } \end{aligned}$ | Small-Signal Transistor | High.Power Transistor | Junction Fet | Mosfet |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Input impedance | High | a | Very low | High | Very high |
| Output impedance | High | * | Low/moderate | High | High |
| Noise | Low | Low | Moderate | Low | Unpredictable |
| Warm-up time | Long | Short | Short | Short | Short |
| Power consumption | Large | Small | Moderate | Very Small | Very smali |
| Aging | Appreciable | Low | Low | Low | Moderate |
| Retiability | Poor | Excellent | Very good | Excellent | Very good |
| Overload sensitivity | Excellent | Good | Fair | Good | Poor |
| Size | Large | Small | Moderate | Small | Smat |

almpedances depend on circuit arrangement:

For common base
For common emitter
For common collector

Mnput Impedance
Low (10's of ohms) Medium (kilohms) High ( 100 's of kilohms)

Output impedance
High (megohms)
Medium ( 10 's of kilohms)
Low (100's of ohms)

## SUMMARY OF INTEGRATED CIRCUIT PROPERTIES

This table compares pertinent characteristics of present day and future ICs.

| Properthes | Curtent vechnologies |  |  |  |  |  |  |  | Future (1985-1900) sos Gpe |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 76 | LSTLL | ECL | 12. | PMOS | Hmos | BULK CNOS | chos/505 |  |  |
| Relative process maturily $(1.10)$ | $\begin{array}{r} 10 \\ (8)^{*} \\ \hline \end{array}$ | $\begin{gathered} 9 \\ (4105)^{\prime} \end{gathered}$ | $\begin{array}{ccc} 8 & 10 & 9 \\ (3 & 10 & 5) \\ \hline \end{array}$ | 4 | 10 | 9 | 6 | 4 | 2 | 1 |
| Process complaxity (No. processing steps) | 18 to 22t | 18 to $23 \dagger$ | 15 to 23\% | 13 to 17 | 8 to 14 | 9 to 15 | 14 to 17 | 14 to 20 | 14 to 20 | 16 |
| Logic complezity $\{$ No. components. 2-Input gale) | 12 | 12 | 8 | 3 to 4 | 3 | 3 | 4 | 4 | 3104 | 2 |
| Packing Density (gales/mm? | 10 to 20 | 20 to 40 | 151020 | 7510150 | 75 to 150 | 10010200 | 401090 | 100 to 500 | 20010500 | 300 to 1000 |
| Propagation delay, ns tiypical values | 8 to 30 (10) | $\begin{gathered} 2 \text { to } 10 \\ (5) \end{gathered}$ | $\begin{gathered} 0.7 \text { to } 2 \\ 12)^{2} \end{gathered}$ | 7 ta 50 (20) | $\begin{aligned} & 30 \text { to } 200 \\ & (100) \end{aligned}$ | $4 \text { to } 25$ (15) | 10 ta 35 (20) | 4 to 20 (10) | 0.2 to 0.4 (0.3) | $\begin{gathered} 0.05 \text { to } 0.1 \\ (0.07) \end{gathered}$ |
| Speecr-pawer protuct (p.l) | 3010150 | 10 to 60 | 151080 | 0.2102 .0 | 50 to 500 | 51050 | 2 to 40 | 0.5 to 30 | 0.110 .0 .2 | 0.01 to 0.1 |
| Typical supply voltages (volls) | +5.0 | +5.0 | -5.2 | $\begin{gathered} +0.810 \\ +1.0 \end{gathered}$ | -15 to +20 | +5.0 | $+10.0$ | +10.0 | +2.0 | *1.2 |
| Signal swing (volis) | 0.2 to 3.4 | 0.2153 .4 | -0.6 to -1.7 | 0.2 to 0.8 | 0.0 to -15.0 | 0.2 to 3.4 | 0.0 to 10.0 | 0.0 to 10.0 | 0.0 to 2.0 | 0.0100 .8 |
| Guaranteed nousp margin (volls\| | 0.3100 .4 | 0.3 to 0.4 | 0.125 | $<0.1$ | 1102 | 0.51020 | 3.5 to 4.5 | 3.5104 .5 | 0.2100 .8 | 0.2 to 0.3 |
| Neulron hardness capabillity ( $\mathrm{n} / \mathrm{cm}^{3}$ ) | 0.2 to 108 | 0.2 to 1014 | $\begin{aligned} & 0.510 \\ & 2 \times 10^{15} \end{aligned}$ | $\begin{array}{r} 105 \\ \times 1018 \\ \hline \end{array}$ | $\begin{gathered} >10^{15} \mathrm{lo} \\ 10^{10} \end{gathered}$ | $\begin{gathered} >10.5915 \\ 1014 \end{gathered}$ | $\begin{gathered} 310^{13} \text { to } \\ 10^{\prime!} \end{gathered}$ | $\begin{gathered} >10^{15} \text { to } \\ 10^{12} \\ \hline \end{gathered}$ | $\begin{gathered} >10^{44} \mathrm{Jo} \\ 10^{14} \\ \hline \end{gathered}$ | $>10^{12}$ |
| Tolal dose (a) hardmess capabisty \{rads\} | 100 to 104 | $10^{4}$ to to ${ }^{\circ}$ | $\begin{gathered} 10 \% 10 \\ 100^{2} \\ \hline \end{gathered}$ | $\begin{gathered} 109 \text { to } \\ 100^{\circ} \\ \hline \end{gathered}$ | 10 F | $\begin{gathered} 1505 \times \\ 10^{4} \\ \hline \end{gathered}$ | $\begin{gathered} 10 \% \\ 100^{\circ} \\ \hline \end{gathered}$ | $\begin{gathered} 10510 \\ 100^{1} \\ \hline \end{gathered}$ | 104 to 104 | $>107$ |
| Dose rati (i) or photocutrent hardiness capabutiy trads/s) | $\left\lvert\, \begin{array}{cc} 0.5 \text { to } \\ 1016 \end{array}\right.$ | 0.2 ta $10{ }^{04}$ | 0.2 to 104\% | $\begin{gathered} 0.7104 \\ \times \quad 1014 \end{gathered}$ | $\begin{array}{r} 0.110 \\ \$ \times 10^{01} \end{array}$ | $\begin{gathered} 0.1 t a \\ 5 \times 10^{9} \end{gathered}$ | $\begin{array}{cc} 0.510 \\ 2 \times 10 \end{array}$ | 0.2 to 1011 | 0.5 to $10^{11}$ | 31019 |

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## ANALOGY BETWEEN THE THREE BASIC JUNCTION

## TRANSISTDR CIRCUITS AND THEIR GQUIVALENT ELECTRON TUBE CIRCUITS

A transistor can be operated with the input signal applied to the base and the output taken from the collector (common emitter), with the input signal applied to the emiller and the oulput taken from the collector (common base), or with the input signal applied to the base and the oulput taken from the emitter (common collector or emitter follower). The performance characteristics of these three connections correspond roughly to the three tube connections shown below, with the exception that the input impedance is generally lower in the transistor circuit. General characteristics of these three connections are given in the table.

| Common Emitter | Common Base | Common Collector |
| :--- | :--- | :--- |
| Large current gain | Approximate unity current gain | Large current gain |
| Large voltage gain | Large voltage gain | Approximate unity voltage gain |
| Highest power gain | Intermediate power gain | Lowest power gain |
| Low input resistance | Very low input resistance | High input resistance |
| High output resistance | Very high output resistance | Low output resistance |
| Analogous to grounded cathode | Analogous to grounded grid | Analogous to cathode follower generally |



| Parameter | Common | Common Emitter | Common Collector | Definition |
| :---: | :---: | :---: | :---: | :---: |
| $z$ | $\begin{aligned} & z_{11}, z_{11 b}, \text { or } z_{b b} \\ & z_{12}, z_{12 b}, \text { or } z_{b b} \end{aligned}$ | $\begin{aligned} & z_{11 e} \text { or } z_{i e} \\ & z_{12 e} \text { or } z_{r e} \end{aligned}$ | $\begin{aligned} & z_{11 c} \text { or } z_{i c} \\ & z_{12 c} \text { or } z_{r c} \end{aligned}$ | Input impedance with open-circuit output Reverse transfer impedance with opencircuit input |
|  | $z_{21}, z_{21 b}$, or $z_{f b}$ | $z_{21 e}$ or $z_{f e}$ | $z_{21}{ }_{c}$ or $z_{f C}$ | Forward transfer impedance with opencircuit output |
|  | $z_{22}, z_{22 b}$ or $z_{\text {ob }}$ | $z_{22 e}$ or $z_{0 e}$ | $z_{22 c}$ or $z_{D c}$ | Output impedance with open-circuit input |
| $y$ | $Y_{11}, Y_{11}$, or $Y_{i b}$ | $\gamma_{11 e}$ or $\gamma_{i e}$ | $\gamma_{11}$ c or $y_{i c}$ | Input admittance with short-circuit output |
|  | $Y_{12}, Y_{12 b}$, or $V_{r b}$ | $y_{12 e}$ or $Y_{r e}$ | $Y_{12} c$ or $Y_{r c}$ | Reverse transfer admittance with shortcircuit input |
|  | $V_{21}, V_{21 b}$, or $V_{f b}$ | $y_{21 e}$ or $\gamma_{f e}$ | $y_{21 c}$ or $y_{f c}$ | Forward transfer admittance with shortcircuit output |
|  | V22, $\mathrm{Y}_{22}$, or Yob | $Y 22 e$ or Yoe | $Y_{22 c}$ or $y_{o c}$ | Output admittance with short-circuit input |
| $h$ | $h_{11}, h_{11 b}$, or $h_{j b}$ $h_{12}, h_{12 b}$, or $h_{r b}$ | $h_{11 e}$ or $h_{i e}$ $h_{12 e}$ or $h_{r e}$ | $\begin{aligned} & h_{11 c} \text { or } h_{i c} \\ & h_{12 c} \text { or } h_{r} \end{aligned}$ | Input impedance with short-circuit output Reverse open-circuit voltage amplification factor |
|  | $h_{21}, h_{21 b}$, or $h_{f b}$ | $h_{21 e}$ or $h_{f e}$ | $h_{21 c}$ or $h_{f c}$ | Forward short-circuit current amplification factor |
|  | $h_{22}, h_{22 b}$, or $h_{0 b}$ | $h_{22 e}$ or $h_{\text {Oe }}$ | $h_{22 c}$ or $h_{o c}$ | Output admittance with open-circuit input |
| Not $\hat{*} h_{11}=1 / y_{11}$ and $h_{22}=1 / z_{22}$. |  |  |  |  |

## Typical Transistor Parameters

| Common 8ase | Common Emitter | Common Collector |
| :--- | :--- | :--- |
| $h_{11}=39$ ohms | $h_{11}=2,000$ ohms | $h_{11}=2,000$ ohms |
| $h_{12}=380 \times 10^{-6}$ | $h_{12}=-600 \times 10^{-6}$ | $h_{12}=1$ |
| $h_{21}=-0.98$ | $h_{21}=50$ | $h_{21}=-51$ |
| $h_{22}=0.49 \mu$ mho | $h_{22}=25 \mu$ mhos | $h_{22}=25 \mu$ mhos |



Common-base configuration (a) and hybrid equivalent citcuit (b).


Common-emitter configuration (a) and bybrid equivalent circuit (b).


Common-eollector coneguration (a) and hybrid equivalent oircuit (b).


## TRANSISTOR PARAMETER CONVERSION TABLES

(A) Common-base $h$ parameters in terms of common-emitter, common-collector, and $T$ parameters.
(B) Common-collector $h$ parameters in terms of common-emitter, common-base, and T parameters.
(C) Common-emitter $h$ parameters in terms of common-base, common-collector, and T parameters.
(D) T parameters in terms of common-emitter, common-base, and common-collector parameters.

| $\begin{aligned} & \hline \begin{array}{c} n \\ \text { neram } \\ \text { sive } \end{array} \\ & \hline \end{aligned}$ | Commor emittr | Commanan egltectos | 1 enomatent critull |
| :---: | :---: | :---: | :---: |
| $\int h_{16}$ |  |  | $r_{*} * 11-\mathrm{or} r_{8}$ |
| $n n_{0}$ |  |  | $\frac{i_{0}}{i_{c}+i_{b}} \equiv \frac{i_{0}}{t_{c}}$ |
| (A) nio |  |  | - |
| $n_{0}$ | $\frac{n_{\infty}}{11+n_{i v} 11-A_{A_{t}} 1+n_{*} h_{0 *}} \geq \frac{A_{\infty}}{1+n_{p_{t}}}$ | $\frac{h_{f s}}{h_{k} h_{o r}-h_{t_{c}} n_{t r}} \geqslant \frac{n_{o c}}{h_{t_{c}}}$ | $\frac{1}{x_{c}+x_{0}}=\frac{1}{e_{4}}$ |
| $\begin{gathered} \pi \\ \text { ournm } \\ \text { for } \end{gathered}$ | Sommen emiter | Comman bave | 1 dquwilent ercuis |
| $\int n_{c}$ | $\cdots$ | $\frac{n_{0}}{\left(1+n_{+0} H 1-h_{\infty}\right)-n_{\Delta 0} n_{\Delta}} \geq \frac{n_{\Delta}}{1+n_{\Delta 0}}$ |  |
| $n_{r c}$ | $1 n_{r e}$ | $\frac{1+h_{0}}{\left(1+h_{g}\right)\left(1-h_{c t}\right)+h_{n 0} h_{t}}=1$ | $\frac{r_{c}-\mu_{c}}{r_{f}+r_{c}-m_{c}}=1-\frac{r_{e}}{(1-a) r_{c}}$ |
|  | $\left.11+h_{4 *}\right\}$ | $\frac{n_{t o}-1}{\left(1-n_{s p}, 11-n_{t}\right)+n_{a t} n_{b}}=\frac{1}{1+n_{t_{0}}}$ | $\frac{x_{c}}{x_{s}+t_{c}-z t_{c}}=\frac{-1}{1-a}$ |
| $n_{\text {oc }}$ | Sor |  | $\frac{1}{r_{1}+r_{c}-a r_{c}} \geqslant \frac{1}{11-a!r_{c}}$ |
| $\begin{gathered} n \\ \text { poram } \\ \text { nom } \end{gathered}$ | Common bere | Camman remestor | Temamaleat ertent |
|  | $\frac{h_{b}}{\left(1+h_{t b}\right)\left(1-h_{s b}\right)+h_{\text {ob }} h_{b}}=\frac{h_{t b}}{1+h_{\text {d }}}$ | $h_{\text {c }}$ | $r_{b}+\frac{r_{b} r_{c}}{r_{a}+r_{c}-a r_{c}} \geqslant r_{b}+\frac{r_{d}}{1-\alpha}$ |
| $c_{1} 0 n_{r T}$ |  | $1 \mathrm{~h}_{\boldsymbol{\tau}}$ | $\frac{r_{\phi}}{r_{f}+r_{f}-\Delta r_{c}} \cong \frac{r_{g}}{[1-a] r_{c}}$ |
| (c) $n^{\prime}$ |  | $-\left[11+h_{k}{ }^{\prime}\right.$ | $\frac{\sigma_{c}-r_{f}}{r_{q}+r_{c}-r_{c}} \geqslant \frac{0}{1-a}$ |
| ( $\mathrm{bor}^{\text {or }}$ |  | Hor | $\frac{1}{r_{*} \cdot r_{c} s_{c}}=\frac{1}{[1-\alpha]_{\varepsilon}}$ |
| $\begin{gathered} r \\ \text { counin } \\ \text { tir } \end{gathered}$ | Comman memilier | Commomever | Commen colisctor |
| [0 |  | nib |  |
| \% | $\frac{n_{r_{t}}, 1}{n_{o k}}$ | $\frac{1 n_{\text {op }}}{n_{00}}$ | $\frac{n_{c_{c}}}{n_{\alpha c}}$ |
| \|D| $\{$ * | $\frac{n_{i f}}{n_{\infty}}$ |  | $\frac{1 n_{64}}{n_{04}}$ |
| \% | $n_{*} \frac{n_{7}\left[1+n_{n_{0}}\right)}{n_{0+}}$ | $\frac{n_{\phi}}{n_{\infty \phi}}$ | $n_{*} \cdot \frac{n_{k-1} 11 n_{\tau-1}}{n_{\infty}}$ |
| ( | $\frac{n_{t e} \cdot n_{t e}}{1+n_{n_{t}}}$ | $\frac{n_{\text {to }} \cdot h_{n}}{n_{n}}$ | $\frac{t_{r r}+r_{r c}}{n_{r c}}$ |

(E) Input impedance and output impedance in terms of $h$ and $T$ parameters.
(F) Insertion power gain and transducer power gain in terms of $h$ parameters.
(G) Current gain and voltage gain in terms of $h$ and $T$ parameters.
(H) Available power gain and operating power gain in terms of $h$ parameters.

(I) $Z$ parameters in terms of $h$ parameters.
(J) $Y$ parameters in terms of $h$ parameters.
(K) Common emitter $z$ parameters in terms of common collector and common base $z$ parameters and $T$ parameters.
(L) Common emitter y parameters in terms of common collector and common base y parameters and T parameters.


| $x$ persmeter | Common caliector | Common base | $T$ equivelent-citcuit |
| :---: | :---: | :---: | :---: |
| $z_{11 \mathrm{l}}$ | $z_{11}-z_{12}-z_{21}+z_{22}$ | $z_{11}$ | $r_{t}+r_{b}$ |
| $z_{120}$ | $z_{22}-z_{12}$ | $z_{11}-z_{12}$ | $r_{t}$ |
| $z_{218}$ | $z_{22}-z_{21}$ | $z_{11}-z_{21}$ | $r_{s}-a_{c}$ |
| I22* | $z_{22}$ | $z_{11}-z_{12}-z_{21}+z_{72}$ | $r_{e}+r_{\text {c }}(1-a)$ |
| $v$ Paramater | Common collector | Common bare | Tequivalent-circuit |
| V110 | r's | $y_{11}+y_{12}+v_{21} y_{22}$ | $\frac{r_{g}+r_{\mathrm{g}}(1-a)}{\Delta}$ |
| $V_{120}$ | $-\left(y_{11}+y_{12}\right)$ | $-\left(r_{12}+y_{22}\right)$ | $\cdot \frac{r_{0}}{\Delta}$ |
| $\gamma^{21 \%}$ | $\left.-\left(y_{11}\right)+y_{21}\right)$ | $-\left(r_{21}+y_{22}\right)$ | $\frac{.}{r_{e}-8 r_{c}}$ |
| $V_{220}$ | $y_{11}+y_{12}+y_{21}+y_{22}$ | 122 | $\frac{r_{0}+r_{6}}{\Delta}$ |

(M) Common base $\mathbf{z}$ parameters in terms of common emitter and common collector $\mathbf{z}$ parameters and $\mathbf{T}$ parameters.
(N) Common base y parameters in terms of common emitter and common collector $y$ parameters and $T$ parameters.
(O) Common collector z parameters in terms of common emitter and common base z parameters and T parameters.
(P) Common collector y parameters in terms of common emitter and common base y parameters and T parameters.
(Q) Input impedance, output impedance, voltage gain, and current gain in terms of $z$ and $y$ parameters.

| 7 aramelel | Common erimiter | Comman collectar | T*quryalent ancuil |
| :---: | :---: | :---: | :---: |
| F110 | 311 | $>_{11} \quad x_{12} \quad x_{21} * z_{27}$ | $r_{2}+r_{6}$ |
| 2120 | $l_{11} \quad 17$ | ${ }_{14} \mathrm{IF}_{21}$ | fob |
| ${ }^{2} 216$ | $z_{11} \quad{ }_{21}$ | $\begin{array}{lll}11 & z_{12}\end{array}$ | $r_{B}+8 r_{c}$ |
| -2720 | $\begin{array}{llll}11 & 312 & 81\end{array}$ | 711 | $r_{b}+r_{c}$ |
| y permaner | Camman amilet | Common collector | T-equivaliont cifeuh |
| $\int_{110}$ | $V_{11}+V_{17}+V_{21}+V_{22}$ | 122 | $\frac{r_{b}+r_{c}}{\Delta}$ |
| $\gamma_{123}$ | ( $\mathrm{y}_{12}$ ' $\mathrm{y}_{22}$ ) | $\left.\underline{V} 21+V_{22}\right\}$ | $\frac{\pi}{\Delta}$ |
| ${ }^{1} 714$ | $\mid y_{21}+1 / 221$ | $\left(y_{12}+y_{22}\right)^{\prime}$ | $\frac{r_{b}+a r_{c}}{\Delta}$ |
| Y220 | V7 | $V_{11}+V_{12}+V_{21}+V_{22}$ | $\frac{r_{p}+r_{b}}{\Delta}$ |


$\bar{\Delta}=r_{e} f_{b}+r_{c} \mid r_{e}+r_{b}\{1 \quad 1]$

| Parament | lingut impedante | Outhut imperance | Voltage gain | Qurtunt puin |
| :---: | :---: | :---: | :---: | :---: |
|  | $\frac{\Delta z+1_{11} z_{L}}{t_{22}+z_{1}}$ | $\frac{\Delta z+y_{22} Z_{1}}{Z_{11}+Z_{q}}$ | $\frac{I_{21} Z_{t}}{\Delta z+z_{11} Z_{t}}$ | $\frac{-21}{z_{22}+z_{L}}$ |
|  | $\frac{r_{\partial z}+r_{L}}{\Delta r+r_{1}, r_{L}}$ | $\frac{Y_{11}+Y_{y}}{\Delta y+y_{22} Y_{y}}$ | $\frac{Y_{2 t}}{\gamma_{22}+Y_{2}}$ | $\frac{V_{31} Y_{L}}{\Delta Y+Y_{11} Y_{L}}$ |

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## MULTIVBRATOR DESIGN CURVES

The accompanying curves permit an easy and rapid determination of the frequency of oscillation of a symmetrical-astable (free-running) multivibrator, and the pulse duration ( $1_{p}$ ) of a monostable (one-shot) multivibrator. The pulse duration of the astable muitivibrator output also can be read from the curve.

The expressions on which the curves are based are derived readily. The expression for the voltage at the base of the "off" transistor is

$$
e_{b}=E_{c c}\left(1-2 \varepsilon^{-\nu A} c\right)+V_{b e}
$$

where $V_{b e}$ is the base-to-emitter voltage of an "on" transistor. The above equation assumes that base-to-emitter breakdown is prevented by using transistors whose base-to-emitter breakdown voltage is greater than $E_{\text {cc }}$ volts, or by connecting a diode in either the base or emitter lead.

The "off" transistor tums on when $e_{b}=V_{b 0}$, or $\epsilon^{-U R C}=1 / 2$ where $t$ is the "off" time ( $t$ ) at the end of which time $e_{b}=V_{b e}$. Solving the equation yields $t_{p}=0.69$ RC. The curves in graph (A) are plots of this equation. For the monostable multivibrator, $t_{p}$ is the pulse duration. The period of the symmetrical-astable multivibrator is equal to $2 t_{p}$.
${ }^{\circ}$ Graph (B) is a family of curves of frequency of the symmetrical-astable multivibrator versus capacitance Cfor various values of resistance $R$. Since the period of the output wave is $2 t_{\rho}$, the equation for frequency is given as $f=1 / 1.38 \mathrm{RC}$, from which the curves were plotted.

FOR EXAMPLE: Find the value of $C$ required to generate a frequency of 500 Hz from a free-running multivibrator, or a 1 msec pulse from a monostable. In both cases the value of $R$ is limited to 100,000 ohms by the beta of the transistor selected. The curves indicated a value of $0.0145 \mu \mathrm{~F}$ for the capacitor.


## OPERATIONAL AMPLIFIERS

An operational amplifier is essentially a very high gain dc amplifier whose open-loop gain is generally high enough when compared with the closed-loop gain so that the closed-loop characteristics depend solely on the feedback etement. Circuit applications for which operational amplifiers can be used are illustrated below.

Summing


Differentiotion


$$
e_{0}=-R_{F} C_{1}\left(\frac{d e_{1}}{d t}\right)
$$

tage Gain (Muitiplication)

$e_{0}=-\left(\frac{R_{F}}{R_{1}}\right) e_{1}$

Scoling


$$
e_{0}=-R_{F}\left(\frac{e_{1}}{R_{1}}+\frac{e_{2}}{R_{2}}+\frac{e_{3}}{R_{3}}+\ldots\right)
$$



$$
e_{0}=-\frac{1}{C} \int_{9}^{t}\left(\frac{e_{1}}{R_{1}}+\frac{e_{2}}{R_{2}}+\frac{e_{3}}{R_{3}}\right) d 1
$$

Subtraction

$e_{0}=\frac{R_{F}}{R_{1}}\left(e_{2}-e_{1}\right)$


Current Constont Source
(Flooting Lood)


Voltage Source



High-impedance Low-voltage Voltmeter



Modulator-Demodulator (Holf-Wove)


Floating Lood


Automotic Goin Control Amplifier


D/A Converter
COMPLEMENTARY SWITCHES


Second-Order Tronsfer Function Amplifier

$\frac{e_{0}}{e_{i}}=\frac{1}{\left(R_{1} R_{2} C_{1} C_{2}\right) s^{2}+C_{1}\left(2 R_{2}+R_{1}\right) s+1}$

Adjustable Log(0 to - $180^{\circ}$ ) Amplifier


Second-order Low-pass Active Filter (Two Fole)


$$
=\frac{1}{\left(\frac{s}{w_{n}}\right)^{2}+\frac{25 s}{w_{n}}+1}
$$

## Second-Order High-Pass Active Filter






Squore-wove Multivibrotor
Erystol Oscillotor (Square Wove)


Common-mode gain Ratio of output voltage over input voltage applied to ( + ) and ( - ) terminal in parallel. Common-mode rejection ratio (CMRR) Ratio of an op amp's open-loop gain to its common-mode gain. Differential-input voltage range Fange of vollages that may be applied between input terminals without forcing the op amp to operate outside its specifications.
Differential Input Impedance ( $Z_{\text {in }}$ diff) Impedance measured between $(+)$ and ( - ) input terminals.
Drift, input voltage Change in output voltage divided by open-loop gain, as a function of temperature or time.
Input voltage offset Dc potential required at the differential input to produce an output voltage of zero.
input bias current Input current required by $(+)$ and ( - ) inputs for normal operation.
Input offset current Difference between $(+)$ and $(-)$ input bias currents.
Offset Measure of unbalance between halves of a symmetrical circuit,
Open-loop bandwidth Without feedback, frequency at which amplifier gain falls 3 dB below its low-frequency value.
Open-loop voltage gain ( $A_{\text {wol }}$ ) Ditterential gain of an op amp with no external feedback.
Slew rate Maximum rate at which output voltage can change with time; usually given in volls per microsecond.

| First Letter | Second Letter | Third, Fourth, and Fifth |
| :---: | :---: | :---: |
| Character |  |  |

The third letter-if there ts one-indicates industrial device and is a $Y$. If there is no third letter, the device is for consumer or entertainment use. The digits that follow the letters for industrial units indicale how many devices of that particular type have been registered. The diglts start at 10 and go up to 99 . When 99 is reached-i.e., after 89 devices-the last letter changes from $a Y$ to an $X$ and the numbering begins anew, working back towards $A$. There is no $Z$. For consumer devices, the numbers that follow the two letters start with 100, allowing registration of 899 similar devices.

FOR EXAMPLE: The designation BLY 80 means the device uses silicon (B) is for high if power use (L), and is used in industrial applications, $(\mathrm{Y}$ ); the 80 means that it is the 71 st device of its type to be registered with Pro Electron.


CHARACTERISTICS OF DISPLAYS USED IN ELECTRONIC EQUIPMENT

| Display Jechnologr | Averaga Viewing Angle | Typrat Current Requitrament | Typica! Votage Fioquirement | Typical Oprerating Temperatures | Relatrue Brightness | Ourability | Colors avalable (basic light source) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Light emiting dicdes | Med bright (washout in sunlight) | $\begin{aligned} & 150^{\circ} \\ & \text { (magnilying } \\ & \text { lens culs } \\ & \text { down angle) } \end{aligned}$ | $51010$ $\mathrm{mA}$ | 2105 V | -40 1085 ${ }^{\circ} \mathrm{C}$ | Rugged, no oreakable parts | Rad, orenga yellow, green |
| Liquid crystal dısptays | Highcontrast. no luthinance | 90 to $150^{\circ}$ | $5010500$ | 3 to 7 V | $\begin{gathered} -10 \\ 1065^{\circ} \mathrm{C} \end{gathered}$ | Glass construction | Black on whito (or reverse) |
| Gas chischarge | Brght | $100^{\circ}$ | $\frac{150 \mathrm{~mA}}{2 \mathrm{~A}} 10$ | 13510250 V | 0 to $70^{\circ} \mathrm{C}$ | Gas.hlied glass construction | Orange |
| 1rcandescant | Vary bright | $150^{\circ}$ | $101017$ $\mathrm{mA}$ | 3105 V | $\begin{gathered} -55 \\ 10-100^{\circ} \mathrm{C} \end{gathered}$ | Glass and filaments construction subject to shock | White. Filterable to most colors |
| Vacuum ftuorescent | Bright | $100^{2}$ | $\begin{gathered} 400 \text { to } 650 \\ \mathrm{~mA} \end{gathered}$ | 30 to 50V | $\begin{gathered} -10 \\ 1055^{\circ} \mathrm{C} \end{gathered}$ | Vacuum-tubo device. glass consiruction | Bright-green Nierable to many colors |
| (Frem Electronic Products, June, 1982. courtesy of Electronic Products.) |  |  |  |  |  |  |  |

## DEFINITIONS OF INTEGRATED CIRCUITS, LOGIC, AND MICROELECTRONICS TERMS

Abrading equipment. This type of equipment fires a gas propelled stream of finely graded abrasive particles through a precise nozzle against the work surface. When linked to abrading equipment, it can cut intricate palterns in silicon semiconductors.
Abrasiva trimming Trimming a film resistor to its nominal value by notching the resistor surface with a fine adjusted stream of abrasive material such as aluminum oxide.
Access time Time required in a computer to move intormation from memory to the computing mechanism.
Activating A treatment which renders nonconductive material receptive to electroless deposition.
Active elements Those components in a circuit which have gain or which direct current flow: diodes, transistors, SCA's, atc.
Active substrate A substrate for an integrated component in which parts display transistance. Examples are single crystals of semiconductor materials, within which transistors and dlodes are tormed.
A.D. converter Analog-to-digital converter; a circuit which accepts information in a continuously varying ac or dc current or voltage and whose output is the same information in digital form.
Adder Switching circuits which combine binary blts to generate the SUM and CARRY of these bits. Takes the bits from the two binary numbers to be added (ADDEND and AUGEND) plus the CARRY from the preceding less significant bit and generales the SUM and the CAARY.
Address Noun: a location, either name or number, where information is stored in a computer. Verb: to select or piek out the location of a stored information set for access.
Alloy junction A junction produced by alloying one or more impurity metals to a semiconductor. A small button of impurity metal is placed at each desired location on the semiconductor wafer, heated above its melting point, and cooled. The impurity metal alloys with the semiconductor material to form a $p$ or $n$ region, depending on the impurlty used.
Alternate print in screen printing, one squeegee print stroke per substrate in alternate directions.
Alumina Aluminum oxide $\left(\mathrm{A1}_{2} \mathrm{O}_{3}\right)$ used as a ceramic substrate material.
Align To put inko proper relative position, agreement, or coordination when placing parts of a photomask together or placing a photomask over an etched pattern in the oxide on a semiconductor wafer.
Alignment The accuracy of coordination or relalive position of images on a semiconductor oxide coating and on the photomask, or any other images placed in relation to those.
"AND" A boolean logic expression used to identity the logic operation wherein given two or more variables, all must be logical " 1 " for the result to be logical "1." The AND function is graphically represented by the dot (*) symbol.
Angle of attack in screen printing, angle at which the squeegee blade attacks the screen surface.
Anticipated carry adder A parallel ADDER in which each stage is capable of looking back at all ADDEND and AUGEND bits of less significant stages and deciding whether the less significant bits provide a " 0 " or a"1" CARAY IN. Having determined the CARAY IN it comblnes it with its own ADDEND and AUGEND to give the SUM for that bit or stage. Also called FAST ADDER or look ahead CARRY ADDER.
Arrays Integrated circuits designed to perform near or actual subsyslem operations. They are characterized by high complexity and component density. Each array package replaces a number of conventional I/Cs. Arrays are classified as medium-scale or larger-scale according to function performed. They can be monolithic or fabricaled on a silicon wafer with interconnections between circuits.
Artwork The original pattern or configuration produced at an enlarged ratio, from which a circuit product is made, using a tochnique of photographic reduction to achieve microelectric scale; layouts and photographic films created to produce thick film screens and thin film masks.
As-fired Description of properties of ceramic substrates (smoothness) or thick film resistors (values) as they emerge Irom furnace processing, before any trimming or polishing.
Asynchronous inputs Those terminals in a flip-flop which can affect the output state of the flip-flop independent of the clock. Called Set, Preset, Reset or DC Set and Reset, or clear.
Back bonding Bonding active chips to the substrate using the back of the chip, leaving the face with its circuitry face up. The opposite is face down bonding.
Backfill Filling an evacuated hybrid circuit package with dry inert gas prior to hermetric sealing of the package.
Bake-aut Elevated temperature process which evaporates unwanted gases and moisture before final sealing of a hybrid circuit package.
Ball bond Type of thermocompression bond wherein a ball shaped end interconnect wire is flattened against a metalized pad.
Basic logic diagram A logic diagram that depicts logic functions with no reference to physical implementations. It consiats primarily of logic symbols and is used to depict all logic relationships as simply and understandably as possible. Nonloglc functions are not normally shown.
Beam leads A generic term describing a system in which flat, metalic leads extend beyond the edges of a chip component, much the same as wooden beams extend from a root overhang. These are used to interconnect the component to film circuitry.
Beryllia Berylium oxide ceramics (BeO) significant in that they have high thermal conductivily characteristics.
Binders Substances added to unfired substrates and thick firm compounds to add strength.

Binary coded decimal (BCD) A binary numbering system for coding decimai numbers in groups of 4 bits. The binary value of these 4 -bit groups ranges from 0000 to 1001 and codes the decimal digits " 0 " through 9 . To count to 9 takes 4 bits; to count to 99 takes two groups of 4 bits; to count to 999 takes three groups of 4 bits.
Binary logic Digital logic elements which operate with two distinct states. The two states are variously called true and false, high and low, on and off, or " 1 " and " 0 ." In computers they are represented by two different voltage levels. The level which is more positive (or less negative) than the other is called the high level, the other the low level. If the true (" 1 ") level is the most positive voltage, such logic is referred to as positive true or positive logic.
distable element Another name for flip-flop. A circuit in which the output has two stable states (output levels " 0 " or " 1 ") and can be caused to go to elther of these states by input signals, but remains in that state permanently after the input signals are removed. This differentiates the bistable element from a gate also having two output states but which requires the retention of the input signals to stay in a given state. The characteristic of two stable states also differentiates it from a monostable element which keeps returning to a specific state, and an astable element which keeps changing from one state to the other.
Bit A synonym for binary numeral. Also refers to a single binary numeral in a binary word.
Bleeding In photomasking, poor edge definition or acuity caused by spread of image onto adjacent areas.
Blister A lump or raised section of a conductor or resistor caused by out-gassing of the binder or vehicle during firing.
Boat A container for materials to be evaporated or fired.
Bond liftoff The failure mode whereby the bonded lead separates from the surface to which it was bonded.
Bond-to-bond distance The dislance measured from the bonding site on the dia to the bond impression on the post, substrate land, or fingers which musl be bridged by a bonding wire or ribbon.
Bond-to-chip distance In beam lead bonding, the distance from the heel of the bond to the component.
Bonding pad A metalized area at the end of a thin metalic strip or on a semiconductor to which a connection is made. Also called Bonding Island.
Bonding ribbon and tape Bonding ribbon and tape are used in the manufacture of high-volume ICs such as memory devices and consumer products. Wire conneclions between I /O pads on the circuit die and the lead frame are replaced by a piece of tape with finely etched fingers that are patterned to fit exactly onto the pads.
Bonding wire Fine gold or aluminum wire lor making electrical connections in hybrid circuits between various bonding pads on the semiconductor device substrate and device terminals or substrate lands.
Boolean algebra The mathematics of logic which uses alphabetic symbois to represent logical variables and " 1 " and " 0 " to represent states. There are three basic logic operations in this algebra: AND, OR, and NOT. (Also see NAND, NOR, Invert which are combinations of the three basic operations.)
Bubble memories In general, magnetic bubble memory systems conslst of a film deposited on a garnet subsirate. Data is stored in magnetic domains (bubbles) which are formed on the film by the application of a perpendicular magnetic field.
Buffer A circuit element, which is used to isolate between stages or handis a large lanout or to convert input and output circuits for signal level compatibility.
Bump chip A chip that has on its termination pads a bump of solder or other bondlng material that is used to bond the chip to external coniacts.
Gump contact A large area contact used for alloying directly to the substrate of a chip, for mounting or interconnecting purposes.
Buriad layer A heavily doped ( $\mathrm{N}+$ ) region directly under the N doped epltaxial colleclor region of transistors in a monolithic Integrated circuit used 10 lower the series collector resistance.
Burf-in Operation of electronic components otten at elevated temperature, prior to their ultimale application in order to stabilize their characteristics and to identily their early failures.
Aurn-in, dynamic High temp test with device(s) subject to actual or simulated operating conditions.
Burn-in, static High tomp lest with device(s) subjected to unvarying voltage rather than to operating conditions: either forward or reverse bias.
Camber In screen printing, a slight rise or curve in the surface of the substrate.
Carriage Mechanism on a screen printer to which the workholder is attached, which conveys the substrate to and from the print position.
Carriers Holders for electronic parts and devices which facilitate handling durlng processing, production, imprinting, or testing operations and protect such parts under transport.
Ceramic Non-metallic and inorganic material (e.g., alumina, beryllia, or steatite) used in microelectric substrates and component parts.
Cermet A combination of ceramic and metal powders used for thin and thick film resistors.
Chip A single substrate on which all the active and passive circuit elements have been fabricated using one or all of the semiconductor techniques of diffusion, passivation, masking, photoresist, and epitaxial growth. A chip is not ready for use until packaged and provided with external connectors. The term is also applied to discrete capacitors and resistors which are small enough to be bonded to substrates by hybrid techniques.
Chip and wire A hybrid technology exclusively employing face-up-bonded chip devices interconnected to the substrate conventionally, i.e., by flying wires.
Chip architecture The design or structure of an IC chip, incorporating arithmetic logic unit, registers, and control-bus pathway configuration.

Chip capacitors Discrete devices which introduce capacitance into an electronic circuit, made in tiny wedge or rectangular shapes to be fired onto hybrid circuits.
Chip component An unpackaged circuit element (active or passive) for use in hybrid microelectronics. Besides ICs, the term includes diodes, transistors, resistors, and capacitors.
Chip-outs Semiconductor die defects where fragments of silicon on the face have been chipped off in processing. ieaving an active junction exposed.
circuit The interconnection of a number of devices in one or more closed paths to perform a desired electrical or electronic function.
Clean room A work station or processing area in which steps are taken (e.g., air filtering) to protect incomplete circuits from dust and contamination.
Clear An asynchronous input. Also called Resel. To restore a memory element or flip-flop to a "standard" state, forcing the Q terminal to logic " 0 ."
Clearance The shortest distance between the outer edges of images applied in sequence.
Clock A pulse generator which controls the timing of computer switching circuits and memory stages end regulales the speed at which the computer central processor operates. It serves to synchronize all operations in a digital system.
Clock input That terminal on a flip-flop whose condition or change of condition controls the admission of data into a flip-flop through the synchronous inputs and thereby controls the output state of the flip-flop. The clock signal performs iwo functions:
(1) It permits data signals to enter the flip-flop; (2) after entry, it directs the flip-flop to change state accordingly.

CML (Current Mode Logic) Logic in which transistors operale in the unsaturated mode as distinguished from most other logic typas which operate in the saturation region. This logic has very fast switching speeds and low logic swings. Also called ECL or MECL.
CMOS Complementary metat-oxide semiconductor. Device formed by the combination of a PMOS and an NMOS (P-type and N-type channel semiconductors).
Co-fire To place circuits onto an unfired ceramic and fire both circuits and ceramic simultaneously.
Collector junction The semiconductor junction in a transistor berween the collector and base regions.
Collocator Device used to collect substrates from a screen printer and deposit them, in rows, onto a conveyor/dryer or furnace belt.
Compliant bond A bond which uses an elastically and /or plastically deformable member 10 import the required energy to the lead.
Component A packaged functional unit consisting of one or more circuits made up of devices, which (in furn) may be part of an operating system or subsystem. A part of, or division of, the whole assembly or equipment.
Component part A lerm sometimes used to denote a passive device.
Component placement equipment Automatic systems for sorting and placing components onto hybrid circuit substrates: consisting of indexing-conveyor, sorter, placement heads, missing component detector, programmable electro-pneumatic control, and options to handie special requirements.
Condiryer Process equipment designed to receive screen printed substrates and dry the ink on the substrate while conveying them away.
Contact printing Print mode in screen printing wherein entire substrale contacts bottom surlace of screen during print cycle. Necessary when using metal masks.
Contaminant An impurity or foreign substance present in a material that affects one or more properties of the material.
Cosmetic defect A variation from the conventional appearance of an item, such as a slight change in color: not necessarily detrimental to performance.
Corrosion In semiconductors, a defect in or on the aluminum metalization, usually a white crystalline growth.
Counter A devico capable of changing slates in a specified sequence upon receiving appropriate input signals. The output of the counter indicates the number of pulses which have been applied. (See also Dlvider.) A counter is made from flip-flops and some gates. The output of all flip-flops are accessible to indicate the exact count at all times.
Counter, binary An interconnection of flip-flops heving a signal input so arranged to enable binary counting. Each lime a pulse appears at the input, the counter changes state and tabulates the number of input pulses for readout in binary form. It has a $2^{n}$ possible counts where $n$ is the number of flip-flops.
Counter, ring A special form of counter sometimes called a Johnson or shift counter which has very simple wiring and is fast. It forms a loop or circuits of interconnected flip-flops so arranged that only one is "0" and thet as input signals are received, the positioning of the " 0 " state moved in sequence from one flip-flop to another around the loop undif they are all " 0 ," then the first one goes to " 1 " and this moves in sequence from one tlip-flop to another untif all are " 1 ." It has $2 \times n$ possibla counts where $n$ is the number of flip-flops.
Cover fay, cover coat Outer layer(s) of insulating material applied over the conductive pattern on the surface of the substrate.
Crazing Minute cracks on or near the surface of materials such as ceramic.
Data Term used to donote facts, numbers, letters, symbols, binary bits presented as voltage levels in a computer. In a binary system data can only be "0" or "1."
DCTL (Direct-Coupled Transistor Logic) Logic employing only transistors as active circuit elements.
Debug To remove malfunctions from a system or device.

Decimal A system of numerical representation which uses ten numerals $0,1,2,3, \ldots, 9$. Each numeral is called a digit. A number system to the radix 10 .
Defect Any deviation from the normally accepted characteristics of a product or component.
Delay The slowing up of the propagation of a pulse either intentionally, such as to prevent inputs from changing while clock pulses are present, or unintentionally as caused by transistor rise and fall time pulse response effects.
Detailed logic diagram A diagram that depicts all logic functions and also shows nonlogic functions, socket locations, pin numbers, test points, and other physical elements necessary to describe the physical and electrical aspects of the logic. The detailed logic diagram is used primarily to facilitate the rapid diagnosis and localization of equipment malfunctions. It also is used to verily the physical consistency of the logic and to prepare fabrication instructions. The symbols are connected by lines that represent signal paths.
Detritus Fragments of material produced during resistor trimming which remain in the trimmed area.
Device The physical realization of an individual electrical element in a physical independent body which cannot be further reduced or divided without destroying ils stated function. This term is commonly applied to active devices. Examples are translstors, pnpn slruclures, iunnel diodes, resistors, capacitors, and inductors.
Dlamond powders, grits, and compounds These materials are used mainly as abrasives for processes such as lapping and polishing, abrasives in abrasive trimming, of to create the cutting surface of slicing equipment.
Die A tiny plece of semiconductor malerial, broken from a semiconductor slice, on which one or more active electronic components are formed. (Sometimes called ohip).
Die bonding Attaching the semiconductor chip to the substrate, with an epoxy, eutectic, or solder alloy.
Dielectric isolation The use of silicon dioxide barriers created during silicon IC processing to provide isolation between components on a chip.
Diffusion A process, used in the production of semiconduclors, which introduces minute amounts of impurltes into a substrate material such as silicon or germanlum and permits the impurity to spread into the substrate. The process is very dependent on temperature and time.
Diffusion and oxidation systems Equipment in which non-conductive materials are made semiconductive by diffusing controlled amounts of selected impurities into the surface and the surface of silicon is oxidized selectively to provide a protective or insulative layer. Diffusion and oxidation are accomplished by exposing the silicon wafer to specific atmospheres in a high temperature furnace.
Diffusion depth testing A diffusion depth tester determines to what depth diffused impurities have been implanted into a wafer under ion implantation.
Digital circuit A circuit which operates in the manner of a switch, that is, it is either "on" or "off." More correctly should be called a binary circuit.
Diode A device permitting current to flow in one direction only. Diodes are used in logic circuits to control the passage or nonpassage of a signal from one element to another.
Discrate Having an individual identity. Fabricated prior to installation, and /or separately packaged, not part of an integrated circuit.
DIP Dual in-line package.
Discrete circuits Electronic circuits built of separate, individually manufactured, tested, and assembled diodes, resistors, trensistors, capacitors, and other specific electronic components.
Discrete component A circuit component having an individual idenlity. such as a transistor, capecitor, or resistor.
Divider (Frequency) Acounter which has a gating structure added which provides anoutput pulse after receiving a specified number of input pulses. The outputs of all flip-flops are not accessible.
Dopants Selected impurities introduced into semiconductor substrates in controlied amounts, the etoms of which form negative (n-type) and positive ( $p$-type) conductive regions. Phosphorus, arsenic, and antimony are n-type dopants for silicon; boron, aluminum, gallium, end indium are p-type dopants for silicon.
Doping Addition of controlled impurities to a non-conduclive material to achieve the desired semiconductor characteristic, accomplished through thermal diffusion or ion implantation.
Dot "AND" Externally connecting separate circuits or functions so that the combinetion of their outputs results in an "AND" function. The point at which the seperate circuits are wired together will be a " 1 " if all circuits feeding into this point are " 1 " (also called WIRED "OR").
Dot "OR" Externally connecting separale circuits or functions, so that the combination of their outputs results in an "OR" function. The point at which the separate circuits are wired together will be a " 1 " if eny of the circuits feeding into this point are "1."
Driver Ant element which is coupled to the output stage of a circuit in order to increase its power or current handling capability or fanout; for example, a clock driver is used to supply the current necessary for a clock line.
OTL (Diode-Transistor Logic) Logic employing diodes with transistors used only as inverting amplifiers.
Dual-in-line package (DIP)) Carrier in which a semiconductor integrated circuil is assembled and sealed. Package consists of a plastic or ceremic body with two rows of seven verticel leads which are inserted into a circult boand and secured by soldering.
Durometer An instrument for measuring the hardness of the squeegee meterial for screen printing.
ECL Emitter-coupled logic; a type of current mode logic in which the circuits are coupled with one another through emitter followers at the input or output of the logic circuit.

Ejection Wipe off or removal of the printed part from the workholder, in screen printing.
Electrical element The concept in uncombined form of the individual buifding blocks from which electric circuits are synthesized.
Electron beam bonding Process using a stream of electrons to heat and bond two conductors within a vacuum.
Electron beam lithography Lithography in which the radiation sensitive film or resist is placed in the vacuum chamber of a scanning beam electron microscope and exposed by an electron beam under digital computer control.
Electron beam welding Process in which welder gererates a stream of electrons traveling at up to $60 \%$ of the speed of light, focuses it to a small, precisely conirolled spot in a vacuum, and converts the kinetic energy into extremely high temperature on impact with the workpiece.
Emitter The region of transistor from which charge carriers (minority carriers in the base) are injected into the base.
Enable To permit an action or the acceptance or recognition of data by applying appropriate signais (generally a logic "f" in a positive logic) to the appropriate input. (See Inhibit.)
Encapsulate To embed electronic components or other entities in a protective coating, usually done when the plastic encapsulant is in fluid state so that it will set in solid form as an envelope around the work.
Entrapment The damaging admission and trapping of air, flux, and fumes, caused by contamination and plating process defects.
Epitaxial Pertaining to a single-crystal layer on a crystalline substrate, and having the same crystalline orientation as the substrate: e.g. silicon etoms condensed from vapor phase onto a sillcon-wafer substrate.
Epitaxial growth A process of growing layers of material on a selected substrate. Usually silicon is grown in a silicon substrale. Silicon and other semiconductor materials may be grown on a substrate with compatible crystalography, such as sapphire (silicon-on-sapphire).
Epitaxial layer A precisely doped, thin layer of silicon grown on a p-doped thick wafer and into which n-type semiconductor junctions are diffused.
EPROM Electricelly programmable read only memory.
Etch factor The ratio of depth of etch to the amount of undercut.
Exclusive " 0 " A logical function whose output is " 1 " if either of the two variables is " 1 " but whose output is " 0 " if both inputs are " 1 " or both are " 0 ."
Exposure The act of subjecting photosensitive surfaces or matter to radiant energy such as light to produce an Image.
Evaporation and sputtering materials Metals used for evaporation charges and sputtering targets, including: chromium and Ils alloys, for (1) a thin adhesive layer on IC substrates to allow better deposition of gold or other metal, (2) resistor material, and
(3) vacuum deposition in mask production; aluminum and certain Al alloys, for first layer deposition in MOS technology; molybdenum, as a conductor or adhesive layer for IC fabrication; and titanium, as an intermediate adhesive layer for beam-lead interconnection.
Evaporation saurces Boats and tilaments used as heat sources for vacuum evaporation to form thin film layers on substrates. The process is trequently done by resistively heating the evaporant in a ceramic crucible or by self-heating or boats constructed of tungsten, molybdenum, or tantalium.
Extrinsic properties Properties introduced into a semiconductor by impurities with a crystal.
Extrinsic semiconductor The resulling semiconductor produced when impurities are introduced into an otherwise nonsemiconductor crystal. The electrical properties depend upen the impurities.
Face bonding Process of bonding semiconductor chlp so that its circuitry side feces the substrate. Flipchip and beam lead bonding are two common methods. (Opposite of back bonding.)
Fall time A measure of the time required for the output voltage of a circuit to change from a high voltage level to a low voltage level once a level change has started. Current could also be used as the reference, that is, from a high current to a low current level.
Fanint The number of inputs available to a specific logic stage of function.
Fanout The number of input stages that can be driven by a circuit output.
Fast ADDER (See Anticipated CARFY ADDER.)
FEB (Functional Electronic Block) Another name for a monolithic integrated circuit of thick-film circuit.
Fbedback When parl of the output of a circuit is channeled back to an input, it is said to have feedback. When part of the output of an amplifier is routed back to augment the inpul signal, the amplifier has positive feedback or if this rechanneling is employed to diminish the input it is called negative feedback.
FET Field effect transistor; semiconductor device in which resistance between source and drain terminals is modulated by a fiald applied to the third (gate) terminel.
Filtu conductor Electrically conductive material formed by deposition on a substrate.
Film microcircuit Thin or thick film network forming an electrical interconnection of numerous devices.
Film resistor A device whose resislive material is a film on an insulator substrate; resistance value is determined by trimming.
Final seal The hybrid microelectronic packaging step which encloses the circuit so that further intemel processing cannot be periormed without disassembly.
Flatpack Subassembly composed of two or more stages made up of integrated circuits and thin film components mounted
on a ceramic substrate. This semiconductor network is enclosed in a shallow rectangular package with the connecting leads projacting Ifom edges of the package.
Flip-chip A generic term describing a semiconductor device having all terminations on one side of the form of bump contacts. After the surface of the chip has been passivated or otherwise treated, it is flipped over for attaching to a matching substrate.
flip-flop (storage element) A circuit having two stable states and the capability of changing from one state to another with the application of a control signal and remaining in that stale after removal of signals. (See Bistable element.)
Flip-flop, "D" D stands for delay. A flip-flop whose output is a function of the input which appeared one pulse earier; for example, if a " 1 " appeared at the input, the output after the next clock pulse will be a " 1. "
Flip-flop, " $J$ - $K$ " A flip-flop having two inputs designated J and $K$. At the application of a clock puise, a" 1 " an the " $J$ " inpul and a " 0 " on the " $K$ " input will set tha flip-flop to the " 1 " state; $a$ " 1 " on the " $K$ " input and a " 0 " on the " J " input will raset it to the " 0 " state; and " 1 " s " simultaneously on boih inputs will cause it to change state regardless of the previous state. $\mathrm{J}=0$ and $\mathrm{K}=0$ will prevent change.
Flip-flop, "R-S" A flip-flop consisting of two cross-coupled NAND gates having two inputs designated "R" and "S." A " 1 " on the " $S$ " input and " 0 " on the " $R$ " input will reset (clear) the flip-flop to the " 0 " state, and " 1 " on the " $R$ " input and " 0 " on the " $S$ " input will set it to the "4." It is assumed that "O's" will never appear simultaneously at both inputs. If both inputs have " 1 's" it will stay as it was. " 1 " is considered nonactivating. A similar circuit can be formed with NOR gates.
Flip-flop, "R-S-T" A flip-llop having three inputs, "R," "S," and "T." This unit works as the "R-S" flip-flop except that the "T" input is used to cause the flip-flop to change stales.
Flip-tlop, "t" A flip-flop having only one input. A pulse appearing on the input will cause the flip-flop to change slates. Used in ripple counters.
Fleating squeegee This squeegee, as opposed to a rigid squeegee, has the ability to produce a rocking movement on the horizontal plane in screen printing.
Flood stroke Return stroke of squeegee in screen printing which redistributes ink back over the pattern. Provides for proper ink control, and is especially useful for thixotropic inks. (See "Print Stroke".)
Fluid flow masking A gold electro-plating lechnique in which the work to be plated is the cathode and current flows through the fluid stream of plating material, allowing control of deposit at the point of contact between the streart and the workpiece.
Furnaces, diftusion and firing Systems designed for enclosed elevated tempereture processing of solid state devices and systerns, ingaseous atmospheres. Diffusion furnaces are operated at temperatures from 1,000 to $1300^{\circ} \mathrm{C}$ to achieve doping of semiconductor substrates, by one of a number of processes. Oxidation is a process that puts a protective layer of silicon oxide on the wafer and is used either as an insulator or to mask out certain areas when doping. Deposition systems, of which there are three (liquid, gaseous, solid), are used to deposit impurities on the silicon wafer. Other systems include a drive-in system used to ditfuse impurities into the wafer to e specified level, and enalloy system which is used in a final step of the metallization process. Firing furnaces are used for the curing of multilayer ceramics for integrated electronics and for the firing of thick film materials on microcircuits.
Furnace, screen printing Process equipment designed to cure substrates after screen printing and drying.
FULL ADDER See Adder.
Gate 1. A circuit having an output and a multiplicity of inputs designed so that the output is energized only when a certain combination of pulses is present at the inputs. An AND-gate dellvers an output pulse only when every input is energized simultaneously in a specified manner. An OR-gate dellivers an output pulse when any one or more of the pulses meet the specified conditions. 2. An electrods in a field effect transistor. 3. A circuit that admits and amplities or passes a signal only when a gating (triggering) pulse is present. 4. A circuit in which one signal serves to switch another signal on and oft.

## Gate definitions below assume positive logic

Gate, AND All inputs must have " 1 " level signals at the input to produce a " 1 " level output.
Gate, NAND All inputs must have " 1 " level signals at the input to produce a " 0 " level output.
Gate, NOR Any one input or more than one input having e"1" level signal will produce a " 0 " level output.
Gate, OR Any one input or more than one input having a "1" level signal will produce a " 1 " level output.
Gates (decision elements) A circuit having two or more inputs and one output. The output depends upon the combination of
logic signals et the input.
Germanium polycrystalline A prime raw malerial for making crystal ingots.
Glassivation A deposited layer of glass on top of a metallized wafer or chip; primarliy a protective layer.
Giazed substrate Ceramic substrete with a gless coating to effect a smooth and nonporous surface.
Green ceramic Unfired ceremic material.
Green substrate Unfired material in substrate form. Normally substrates are printed after firing. Under special clrcumstances, however, green (unfired) substrates are printed.
Half ADDER A switching circuit which combines binary bits to generate the SUM and the CARRY. It can only take in the two binary bits to be added and generate the SUM and CARRY (see also ADDER).
Halt shift register Another name for cerlain lypes of flip-flops when used in a shift register. It takes two of these to make one stage in a shift register.

Header Base of a hybrid circuit package, holding the leads.
High See Binary logic.
High temperature reverse bias Burn-in type lest of diodes and transistors conducted with the junctions reverse blased to effect any failure due to ion migration in bonds of dissimilar melals
Hole A mobile vacancy or electron deficiency in the valence structure of a semiconductor. It is equivalent to a positive charge.
HTRG High temperature reverse bias.
Hybrid A method of manufacturing integrated circuils by using a combination of monolithic, thin-film and thick-film techniques.
IC Integrated circuit.
IC sacket Female contact which provides pluggable electrical engagement on its inner surface for integrated circuit components to achieve interfacing to a PCB.
Image/pattern The printed screen or design on the substrate atter screen printing.
Inhibit To prevent an action, of acceptance of data, by spplying an eppropriate signal to the appropriate input (generally a logie "0" in positive logic). (Seo Enable.)
ink In hybrid technology the conduclive paste used on thick film materials to form the printed conductor pattern. Ususlly contalns metals, metal oxide, glass frit, and solvent.
Input/oulput Interface circults or devices offering access between external circuits and the central processing unit or mamory.
Integrated circuit (ElA definition) (1) "The physical realization of a number of electrical elements inseparably associated on or within a continuous body of semiconductor malerial to perform the functions of a circuit." (See Slice and Chip.) (2) Electronic circuits or systems consisting of an inlerconnected array of extremely small active and passive elements, inseparably associated on or within a continuous substrate or body. Other names are intagrated electrontic circuit, integratad electronio system, and integrated microcircult.
Integrated injaction logie Integrated circuit logic which uses bipolar fransistor gates. Makes possible lerge scale Integratlon on slilicen for logic artays and other analog and digital applications.
Inverter A circuit whose output is always in the opposite state from the input. This is also called a NOT circuil. (A teeter-toher is a mechanical inverter.)
//0 Input/output.
Ion Implantation Precise and reproducible methed of doping semiconductors to achieve e desired characteristic. Ions of the parlicular dopant are energized and accelerated to the point where they can be driven in a focused beam directly into the sillton wafer. This technique assures unlionm, accuralely controlled depth of implentation and ionic diffusion in the waker,
lon milling ton milling is a VLSI production technique that pertorms many of the seme type of tesks that more tradiklonal wet chemical and plasma etching processes do.
ISHM The International Society for Hybrid Microelectronics.
Isolation diffusion In MIC technology, the diftusion step which generates back-to-back functions to isolate active devices from one another.
Josephson thfect The tunneling of electron pairs through a thin insulating bartier between two superconducting materials. Junctlon A joining of two different semiconductors or of semiconductor and metal. Alloy, diffused, electrochemical, and grown are the four junction types.
Kerf The slit or channel cut in a resistor during trimming by laser beam of abrasive jet.
Laminar flow A directed stream of filtered air moved constantly across a clean work station, usually parallel to the workbench surface.
Land area in image Closed spaces in the screen which result in open spaces on the printed image in screen printing.
Lapping Grinding and polishing such products as semiconductor blanks in order to obtain precise thicknesses or exiremely smooth, flat, polishing surfaces.
Large-scale integration (LSI) Usually denoles arrays of integrated circuits on a single substrate that comprise 100 or more Individual actlve circult functions or gates.
Laser bonding A process which forms a metal-to-metal fastened union, using a laser heat source to join conductors.
Laser trim The adjustment (upward) of a tilm resistor vahte by applying heat from a focusod laser source to remove material.
Laser welding Process in which thermal energy rebased by a laser impinging upon the surface of a metal is conducted into the bulk of the metal work-piece by themmal conduction, bonding component leads to highly conductive materials such as copper printed circuitry.
Lead frame The metal pat of a solid state device package which achleves electrical connection between the die and other parts of the systems of which the IC is a component. Large scale integrated circuits are welded onto lead frames in such a way that leads are available to facilitake making connections to and from the various solid state devices to the packages.
Leadless inverted device (LID) A shaped, metallized ceramic form used as an intermediate carrier for the semiconductor chip devices, especially adapted for attachment to conductor lands of a thick or thin film network by reflow solder bonding.
Leak detectors Applied only to hernetic devices, fine leak detectors are used to detect defects in sealing that are too small to be detected by gross-leak methods. Devices are placed in a bomb pressurized with a mixture of gases.

Life aging Bum-in test which moderates the elevation of temperature and extends the time period in order to test overall device quality as opposed to infant mortality.
Linear circuit A circuit whose output is an amplified version of its input, or whose output is a predetermined variation of its input.
Logic A mathematical arrangement using aymbols to represent relationships and quantities, handled in a microelectronic network of switching circuits or gates, which perform certain functions; also, the type of gate structure used in part of a data processing system.
Logic diagram A picture representation for the logical functions of AND, OR, NAND, NOR, NOT,
Logic function A combinational, storage, delay, or sequential function expressing a relationship between variable signal input(s) to a system or device and the resultant output(s).
Logic swing The voltage difference between the two logic levels " 1 " and " 0. ."
Logic symbol The graphic representation of the aggregate of all the parts implementing a logic function.
Low See Binary logic.
LSI Large scale integration.
Magnetic integrated circuit The physical realization of one or more magnetic elements inseparably associaled to perform all, or at leest a major portion, of its intended function.
Masks, microelectronic Thin metals or other materials with an open pattern designed to mask off or shield selected portions of semiconductors or other surfaces during deposition processes. There also are photomasks or optical masks for contact or projection printing of wafers-these may use an extremely flat glass substrate with iron oxide, chrome, or ernulsion coaling. There also are thick film screen masks.
Medium scale integration (MSI) The physical realization of a microelectronic circuit fabricated from a single semiconductor integrated circuit having circuitry equivalent to more than 10 individual gates or active circuit functions.
Memory The semi-permanent storage of numbers, in digital form, in a circuit or system. With reference to computers, the term also describes the storage capability or location and which receives and holds information for later use. Also, the storage arrangement, such as RAM or other type.
Matallization The selective deposition of metal film on a substrate to form conductive interconnection between IC elements and points for connections with the outside world.
Malal-oxide-semiconductor (MOS) A metal over silicon oxide over silicon errangement which produces clrcuit components such as trensistors. Electrical characteristics are similar to vacuum tubes.
MIC Monolithic integrated circuit.
Microbond The realization of a very small fastened joint between conductors or between a conductor and a microelectronic chip device.
Microcircuit The physical realization of a hybrid or monolithie interconnected array of very small active and passive electronic elements.
Microelectronics The entire spectrum of electronic erl dealing with the labrication of sophisticated, practical systems using miniaturized electronic components. Microelectronics has developed along two basic technologies-monolithic integrated circuits and hybrid integrated circuits.
Microminiaturization The process of packaging an assembly ol mictominialure active and passive electronic elements, replacing an assembly of much larger and different parts.
Micromodule A microcircuil constructed of a number of components (e.g., microwafers) and encapsulated to form a block that is still only a lraction of an inch in any dimension.
Microprohe An extremely sharp and small exploring tool head attached to a positioning handle, used for testing microelectronic circuits by establishing ohmic contact.
Microprocessor An IC package incorporating logic, memory, control, computer, and /or interface circuits, the whole of which is designed to handle certain functions.
Microwave integrated circuit The physical realization of an electronic circuit operating at frequencies above one gigahertz and fabricated by microelectronic techniques. Either hybrid or monolithic integrated circuit technology may be utilized.
Minority carrler The less-predominant carrier in a semiconductor. Electrons are the minority in p-type; holes are the minority in n-type semiconductors.
Mobility. The ease with which charge carriers can move through a semiconductor. Generally electornics and holes do not have equal mobility in a glven semiconductor. Mobility is higher in germanium than in silicon.
Module A packaging unit dlsplaying regularity and separable repetition. It may or may not be separable fromother modules after initial assembly. Usualiy all major dimensions are in accordance with a prescribed set of dimensions.
Molecular beam epitaxy equipment This equipment is used for growing epitaxial thin films under UHV conditions by directing beams of atoms or molecules created by thermal or electron beam evaporation onto clean, heated substrates.
Molecular electronics Simply, electronics on a molecular scale, dealing with the production of complex circuitry in semiconductor devices with integral elements processed by growing multi-zoned crystals in a furnace for the ultimate performance of electrical functions.
Monolithic Refers to the single silicon substrate in which an integrated circuit is constructed. (See Integrated circuit.) Monolithic integrated circuit The physical raalization of electronic clrcuits or sub-systems irom a number of extremely small
circuit elements inseparably associated on or within a continuous body or a thin film of semiconductor material.
Morphology, integrated The structural characterizetion of an electronic component In which the identity of the current or signal modifying areas, patterns, or volumes has become lost in the integration of electronic materials, in contrast to an assembly of devices performing the same function.
Morphology, translational The structural characterization of an electronic component in which the areas or patterns of resistive, conductive, dielectric, and active materials in or on the surface of the structure can be identified in a one-to-one correspondence with devices assembled to perform an equivalent function.
MOS Metal-oxide-semiconductor. A technology for producing transistors that incorporates metal over oxide over silicon layers. Electrical characteristics are similar to vacuum tubes.
MSI Medium scale integration.
MTNS Metal thick nitride semiconductor, which is similar to an MTOS device except that a thick sllican nitride or silicon nitride-oxide layer is used instead of just plain oxide.
MTOS Metal thick oxide semiconductor, where the oxide outside tha desired active gate area is made much thicker in order to reduce problems with unwanted parasitic elfects.
Multichip Integrated circuit Hybrid Integrated circult which includes two or more SIC. MSI, or LSI chips.
Multilayer dialettric A compound Including glass and ceramie which is applied as an insulating barrier between conductors for multi-layer and crossover work.
"NAND" A Boolean loglc operation which yields a logic " 0 " output when all logic input signais are logic "1,"
Negative logic Logle In which the more negative voltage represents the "1" state; the less negative voltage represents the " 0 " state. (See Binary logic.)
Network A collection of elements, such as resistors, coils, capacitors, and sources of energy, connected together to form several Interrelated circuits.
NMOS N-channel MOS circuits, using currents made up of negative charges and producing devices at least twice as fast as PMOS.
Noble metal paste A soft, moist, smooth compound made up partially of precious metals such as gold, platinum, ruthenium, or others classed as noble metals, providing conductors in film circuitry.
Noble systern Thick film system using conductors of gold, platinum, and possibly palladium silver, or certain alloys of these precious metals.
Noise immunity A measure of the insensitivity of a logic circuit to triggering or reaction to spurious or undesirable electrical signals or noise, largely determined by the signal swing of the logic. Noise can be either of two directions, positive or negative.
Nan-noble system Thick film system using conductors of copper, tungsten, nickel, molybdenum, and other non-noble metals.
"KOR" A Boolean logic operation which yields a logic " 0 " output with one or more true " 1 " input signals.
"NOT" A Boolean logic operation indicating negation, not " 1 ." Actually an inverter. If inputs is " 1 " output is NOT " 1 " but " 0 ." If the input is " 0 " output is NOT " 0 " but " 1 ," Graphically represented by a bar over a Boolean symbol such as A. A means "when A is not 1 ."
$n$-Region The zone in a semiconductor in which electron density is greater than hole density.
n-type Semiconductor material whose impurities produce free electrons in the compound, leading to conduction.
n-type semiconductor An extrinsic semiconductor in which electron density exceeds hole density. An electron donor type.
Off-contact printing Print mode wherein screen printer's squeegee stretches screen to touch the substrate and deposit ink. Usually $0.010^{\prime \prime}$ snap-oll is used. Allows thicker ink deposition.
Offset The change in input voltage required to produce a zero output voitage in a linear amplifier circuit. In digital circuits it is the dc voltage on which a signal is impressed.
One ("1") See Binary Logic.
"0R" A Boolean logic operation used to Identify the logic operatlon wherein two or more true " 1 " inputs only add to one true " 1 " output. Only one input needs to be "true" to produce a "true" output. The graphical symbol for "OA" is a plus sign ( + ).
Overglaze A glass compound in low-melting, vitreous form, used as a coating to passivate thick film resistors and offer mechanical protection.
Overiap The contact area between a film resistor and film conductor.
Packaging The process of physically locating, connecting, and protecting devices or components.
Packaging density The number of devices or equivalent devices per unit volume in a working system or subsysiem. Pad In IC technology, the bonding area.
Parallsl gap welding Type of resistance welding wherein electrodes contact the work from one side only, Mechanism by which bonding occurs is virtually always fuslon. Process is wall sulted to welding component leads to planar suriaces such as IC leads to PC conductors.
Parallelity Relationship of screento work-holder and print head in screen printing. Each should be paraliel to one another in order to print acourataly.
Parameter Any specific characteristic of a device. When considered together, all the parameters of a device describe its operational and physical characteristics.
Paralle! This refers to the technique for handling a binary data word which has more than one bit. All bits are acted upon simultaneously. It is like the line of a football team. Upon a signal all line men act. (See also Serial.)

Parallel Adder A conventional tachnique for adding where the two multibit numbers are presented and added simultaneously (parallel). A ripple adder is still a parallel adder; the carry is rippled from the least significant to the most significant bit. Another type of parallel adder is the "Look Ahead," or "Anticipated Carry" adder. (See Ripple ADDER and Fast ADDER.) Parallel operation The organization of data manipulation within computer circuitry where all the digits of a word are transmitted simultaneously on separate lines in order to speed up operation, as opposed to serial operation.
Particle impact noise detection (PIND) PIND testing equipmenl detects any loose foreign particles that may be present in a hermetic package. The package is placed on a shaker table where it is in intimata contact with an acoustic transducer that drives an ultrasonic amplifier.
Parts handling Devices used to load and unload substrates during screen prinling and drying operations.
Passivation The growth of an insulating layer on the surface ol a semiconductor to provide electrical stability by isolating the transisfor surface from electrical and chemical conditions in the environment. II reduces reverse-current leakage, Increases breakdown voltages, and improves the power-dissipation rating.
Passive alements Resistors, inductors, or capacitors, elements without gain.
Passlve substrate A substrate tor an integrated component which may serve as physical support and thermal link to a thickor thin-film integrated circuit, but which exhibits no transisiance. Examples of passive subsirates are giass, ceramic, and similar materlals.
Paste Synonymous with "composition" and "ink" when relating to screenable, thick tilm materials.
Pattem/imare The open area in the screen through which the ink penetrates to become the printed image on the substrate. In screen printing.
Photmask A square, flat glass substrate, coated with a photographic emulsion or a very thin layer of metal, on which appear several hundred circuit patterns (each containing thousands of images). The patterns are exposed onto semiconductor wafers.
Photoresists and processing materials These are light sensltive materiels that are deposited as a uniform film on a wafer or substrate. The exposure of specific pettern is periormed through masking operalions.
Pishole A minute hole through a layer or pattern.
Planar process Fabrication of MICs and semiconductor devices using silicon dioxide as a masking agent and producing components on a single plane.
Platen Plate which holds substrate during screen printing.
Plating The deposition of a metal layer on a substrate surface by electrolytical or centain chemical means. The materials include gold, copper, solder, etc. The functions of the metal plate vary, inciuding corrosion protection, solderabillty enhancement, etch resist, bonding for lead frames, and electrical connection, emong others.
PMOS P-channel MOS: refers to the oldest type of MOS circuit where the electrical current is a flow of positive charges.
Polishing A mechanical finishing operation conducted upon solid state substrates to achieve smoothness and desired surface qualities. See Lapping.
Porcelainize To coat and fire a metal with glass material, forming a hybrid circuit substrate.
Positive lagic Logic in which the more positive voltage represents the "1" stage. (See Binary logic.)
Presat An input like the Set input and which works in parallel with the Set
Probing A term used to describe electrical testing that employs very finely-tipped probes applied sequentially to each of the finished dice of a wafer.
PROM Programmable read-only memory; a ROM which requires a progremming operation.
Propagation delay A measure of the time required for a change in logic level to be Iransmilted ihrough an element or a chain of elements.
Propagation time The time necessary for a unit of binary informalion (high voltage or low) to be transmitted or passed from one physical point in a system or subsystam to another. For example, from input of a device to output.
p-type semiconductor An extrinsic semiconductor in which the hole density exceeds the conduction electron density. An electron acoeptor type.
Print stroke Stroke of the squeegee in screen printing at which time ink is forced through the pattern on the screen.
Print-print Squeegee prints in both directions per substrate in screen printing process.
Printer Process unit designed to accept, hold, and screen print a substrate in order thal ink may be applied with extremely accurate and repeatable registration.
Pulse a signal of very short duration.
Pupla plague Defect-causing formation of gold-aluminum chemical compounds often produced when goid and aluminum are bonded. Purple in color, britte, subject 10 degenerative failure, and sometimes compounded by inclusion of silicon.
Qouput The reference oulput of a flip-flop. When this output is " 1 " the flip-flop is said to be in the " 1 " state; when it is " 0 " the output is said to be in the "O" state. (See also State and Sel.)
Goutput The second oulput of a lijp-flop. It is always opposite in logic level to the O output.
RAM Random access memory; a type of memory which offers access to storage locelions within it by means of $X$ and $Y$ coordinates.
RCTL (Resistor-Capacitor-Transistor-Logic) Same as RTL except that capacilors are used to enhance switching speed. Register A device which can store information, usually that contained in a small subset or word of the total within a digital computer system.

Registration The degree of proper alignment of a circuit pattern on the substrate.
Resist Material such as ink, paint, or metaliic plating, used to protect the desired portions of the printed conductive pattern from the action of the etchant, solder, or plating.
Reset Also called clear. Similar to Set except it is the input through which the $Q$ output can be made to go to " 0 ."
Rigid squeegee Firm mounting of the screen printer squeegee blade and holder. Squeegee adjustment is more critical. Ripple The transmission of data serially. It is a serial reaction analogous to a bucket brigade or a row of falling dominoes. Ripple ADDER A binary adding system similar to the system most people used to add decimal numbers-that is, add the "units" column, get the carry, add it to the "10's" column, get the carry, add it to the "100's" column, and so on. Again it is necessary to wait for the signal to propagate through all columns aven though all columns ere present at once (parallel). Note that the carry is rippled.
Ripple counter A binary counting system in which fllp-flops are connected in series. When the first flip-flop changes it effects the second which effects the third and so on. If there are ten in a row, the signal must go sequentially from the first flip-flop to the tenth.
Risers In a multilayer substrate, the conductive paths that vertically connect various levels.
Rotary (theta) motion Angular (rotary) adjustment of image to substrate. Allows registration in angularity in addition to "X" and " $Y$ " in screen printing. (Also called Theta motion.)
Rise time A measure of the time required for the output voltage of a state to go from a low voltage level ("0") to a high voltage level ("1") once a level change has been started.
ROM Read-only memory; a random access storage in which the data pattern is unchangeable after manufacture.
RTL (Resistor-Transistor-Logic) Logic is performed by resistors. Transistors are used to produce an inverted output.
Sapphire substrates Materials which provide a uniform dielectric constant, controlled orientation, thermal conductivity, and the single crystal suriace desired for SOS, hybrid IC, and other microcircuit systems. The material may be grown directly in ribbons, tubes, filaments. and sheets.
Screen Tensioned mesh material with an open pattern through which ink penetrates to place an image on the substrate. Screen is above and parallel to the substrate during screen printing.
Screen printing, thick film The art of depositing conductive, resistive, and insulating materials on a dielectric base. This deposition is made through selected open areas in screens with inks or pastes forced through the open areas of the screen by squeegee motion onto the substrate base. In some cases, masks instead of conventional mesh screens may be used.
Scribing Scratching a tooled line or laser path on a brittle substrate to allow a wafer to be cleft or broken along the line, producing IC chips when all brakes are completed.
Scribing machines and tools Equipment used to separate wafers into individual devices, chips, or dice. This has been done by crude techniques similar to glass cutting, but is now accomplished by more etficient methods, using truncated pyramid diamond scribers, automated machines, conical tools, or lasers.
SEM Standard electronic module; a subassembly configuration format which meets a particular U.S. Navy set of specifications. This abbreviation is also used for scanning electron microscope.
Semiconductor The name applied to materlals which exhlbit relatively high reslstance in a pure state but much lower resistance when minute amounts of impuritles are added. The word is commonly used to describe elactronic devices made from semiconductor materials.
Semiconductor devices Devices in which the characterlstic distinguishing electron conduction takes place within a semiconductor, ranging from the single unit transistor to multiple unit devices such as the semiconductor rectifier. Other devices are diodes, photocells, thermistors, and thyristors.
Semiconductor integrated circuit (SIC) The physical realization of a number of electric elements inseparably assoclated on or within a continuous body of semiconductor material to periorm the function of a circult.
Serial The technique for handling a binary data word which has more than one blt. The blts are acted upon one at a time, It is like a parade going by a revlew point.
Serial operation The organization of data manipulation within computer circuitry where the digits of a word are transmilted one at a time along a single line. The serlal mode of operation is slower than parallel operation, but utlizes less complex circuitry.
Set An input on a filp-flop not controlled by the clock (see Asynchronous inpuis), and used to effect the Q output. It is this input through which signals can be entered to get the Q output to go to " 1 ." Note it cannot get $Q$ to go to " 0 ."
Shear tester Shear testers are used to determine the integrity of a material or to test the adherance between two attached items. It is used for testing eutectic and epoxy die-bond strengths, and for adherance testing a gold-wire ball bonds, gold and solder chip bumps, external lead frames, coined and welded gold electrical contacts, thick film plating, and more.
Shift The process of moving data from one place to another. Generally many bits are moving at once. Shifting is done synchronously and by command of the clock. An 8 -bit word can be shifted sequentially (serially)-that is, the 1 st bit goes out, 2nd bit takes 1 st bit's place, 3rd bit takes 2 nd bit's place, and so on, in the manner of a bucket brigade. Generally referred to as shifting left or right. If takes 8 clock pulses to shift an 8-bit word or all bits of a word can be shiffed simultaneously. This is called parallel load or parallel shiff.
Shift register An arrangement of circuits, specifically flip-flops, which is used to shift serially or in paraliel. Binary words are generally parallel loaded and then held temporarily or serially shifted out.

SIC Semiconductor integrated circuit.
Silicon A brittle, gray, crystalline chemical alement which, in its pure state, serves as a semiconductor substrate in microelectronics. It is naturally found in compounds such as silicon dioxide.
Silicon gate A type of MOS in which the gate is made of silicon instead of metal. It is faster and denser than the metal-gate MOS.
Silicon nitride A compound of silicon and nitrogen deposited on the surface of silicon monolithic ICs to impar greater stability.
Silicon oxide Silicon monoxide or dioxide or a mixture, the latter of which can be deposited on a silicon IC as insulation between metallization layers.
Single print One squeegee print stroke and flood return per substrate, in screen printing.
Skewing Refers to time delay or offset betwean any two signais in relation to each other,
Slewing rate Rata at which the output can be driven from limit to limit over the dynamic range.
Slice A single wafer cut from a silicon ingot forming a thin substrate on which all active and passive elements for multiple integrated circults have been fabricated utlizing semiconductor epltaxial growth, diffusion, passivation, masking, photo resist, and matallization technologies. A completed slice generally contains hundreds of individual circuits. (see Chip.)
Small scaie Integration A circuit of under 10 gates, generally invoiving one metallization level implementing one circuit function in monolithic allicon.
Snap-off Distance from top of substrate in screen printing to boHom surface of screen. Squeegee must stretch screen this far to meet the substrate and deposit ink. Set by "Z" mot|on adjustments.
Snapstrate Scored large area substrate which, after screen printing, may be snapped or broken apart into smaller sized substrates.
Snugger Device for automatically positioning and holding the substrate in proper position during the print cycie, in screen printing.
Solder systems for bonding and walding Processors for ceramic hybrid microcircuits, substrates, lead frames, microassemblies, flat packs, wire memory arrays, ceramic headers, and magnet wire, where solder normally has been pretinned on the substrate or individual components, or solder pastes provide solder without the need for pretinning operations. Temperature controlled preheat, refiow, and cooling stages are involved, with reflow being almost instantaneous.
Solid state The electronic properties of crystalline materials (usually semiconductor in type). The interaction of light, heat, magnetic fields, and electric currents in these crystalline materials are involved in solid state devices. Less power is required to operate solid state devices and a greater variety of effects can be obtained. (2) Technology utilizing solid semiconductors in place of vacuum tubes for amplification, rectification, and switching.
S0S Silicon-on-sapphire transistor device. Silicon is grown on a passive insulating base (sapphire) and then selectively etched awey to form a solid state device.
Sputtering A method of depositing a thin film of material onto a substrate. The substrate is placed in a large demountable vacuum chamber having a cathode mada of the metal or ceramic to be sputtered. The chamber is then operated so as to bombard the cathode with positive ions. As a result, small particles of the material fall uniformly on the substrate.
Sputtering targets These are usually in the form of simple circular or rectangular plates, comprised of a variety of materials, and bombarded by gas ions that transfer their momentum to particles of the target, ejecting them into the vacuum chamber that houses the operation. These particles are then deposited in a thin film on strategically located substrates.
SSI Small scale integration.
Squeegee Hard, flexible blade with a precision edge which, with applied pressure, forces or pushes ink through the screen in screen printing.
Squeegee pressure Downward force exeried upon the screen and substrate by the squeegee during screen printing.
Squeegee speed Rate of speed at which the squeegee is driven across the screen during screen printing.
Stability The specific ability of electronic circuits or other devices to withstand use and environmental stresses without changing. Also continued operation according to specifications despite adverse conditions.
State This refers to the condition of an input or output of a circuit as to whether it is a logic " 1 " or a logic " 0 ." The state of a circuit (gate or flip-flop) refers to its output. The flip-flop is said to be in the "1" state when its Q output is "1." A gate is in the " 1 " state when its output is "1."
Static in burn-in, the quallty of a test wherein the device is subject to elther forward or reverse bias applled to appropriate terminals; voltages are unvarying throughout test.
Steatite Ceramic material composed mainly of a silicate of magnesium, used as a circuit substrate.
Step To use the step-and-repeat methed.
Substrate The physical material upon which an electronic circuit is fabricated. Used primarily for mechanical support but may serve a useful thermal or electrical function. Also, a material on whose surface an adhesive substance is spread for bonding or coating, or any material which provides a supporting surface for other materials.
Subsystom A part or division of a system which in ltself has the properties of a system.
Surface diffuslon The high temperature Injection of atoms into the surtace layer of a semiconductor material to form the Junctions. Usually a gaseous diffusion process.

Synchronous Operation of a switching network by a clock pulse generator. All circuits in the network switch simultaneously. All actions take place synchronously with the clock.
Synchronous inputs Those terminals on a flip-flop through which data can be entered but only upon command of the clock. These inputs do not have direct control of the output such as those of a gate but only when the clock permits and commands. Called JK inputs or ac set and reset inputs.
System A group of integrated circuits or other components interconnected to perform a single function or number of related functions. If further interconnected into a large system, the individual elements are referred to as subsystems.
Taper testers A taper tester is used to test one aspect of the dimensional integrity of wafers. Taper results when the two faces of the water under test are not parallel.
TCR Temperature coefficient of resistance.
Temperature coofficient of resistance The amount of change in the resistance of a material per dagree of temperature rise. Themal compression bonding Process of diffusion bonding in which two prepared surfaces are brought into intimale conlact, and plastic deformation is induced by the combined effects ol pressure and temperature, which in furn resulis in atom movement causing the development of a crystal lattice bridging the gap between facing surfaces and resulting in bonding.
Thermistor A semiconductor device, the electrical resistance of which varies with the lemperature. Its temperalure coefficient of resistance is high, nonlinear, and usually negative.
Thick film Conductive, resistive, and/or capacitive passive network deposited on a substrate using a metallic or resistive film which is more than five microns in thickness.
Thick film hybrid integrated circuits The physical realization of a hybrid integrated circuit fabrication on a thick film network. Thick film resistor, conductor, and diefectric compositions The principle materials for making thick film circuits, available in paste form and consisting of mixtures of melal, oxide, and glass powders.
Thin film Conductive, resistive, and /or capacitive passive network deposited on a substrate using a metalic or resistive film which is less than five microns in thickness.
Thin film deposition, chemical vapor type The CVD technique involves a decomposition and reaction between gases on the surface of a heated substrate such that a solld layer is nucleated and grown. Metals are generally derived from the decomposition of the metal halides. Insulators may be formed by reacting motal halides with oxygen (oxides), ammonia (nitrides), diborane (borides), etc.
Thin fim deposition, evaporation type Popular technique for depositing thin film in vacuum, accomplished by heating the source material in a low pressure chamber so that it vaporizes and then condenses onto all cooler surfaces in line-of-sight from the source.
Thin film deposition, sputtering type Evaporation producad by ion bombardment of the source material, known as cathodesputtering.
Thin film deposition materials, conductors and resistors Metals such as aluminum, gold, chromium, nickel, platinum, tungsten, alloys, and cermets deposited as electrical conductors and resistors on silicon or other substrates.
Thin film deposition materials, inorganic dielectrics Film compounds produced by various vacuum evaporation processes and deposited on substrates to periorm electrical functions. Examples include silicon monoxide, $\mathrm{ZnS}, \mathrm{CaF}, \mathrm{SiO}_{2}, \mathrm{Al}_{2} \mathrm{O}_{3}$, $\mathrm{Si}_{3} \mathrm{~N}_{4}$, and other chemical compounds.
Thin film depositien materials, organic dielectrics Insulating film compounds produced when organic vapors are heated under conditions in which polymerization and deposition occur. Examples are parylene, butadene, acrolein, and divinyl benzene.
Thin film deposition materials, semiconductors Polycrystelline films deposited by vacuum or flash evaporation to produce high purity single crystal silicon or other semiconductor substances.
Thin film hybrid integrated circuits The physical reatization of a hybrid integrated circuit fabricated on a thin film network. Thin fikn integrated circuit The physical realization of a number of electric elements entirely in the form of thin films deposited in a pattemed relationship on a struclural supporting materlal.
Toggle To switch between two states as in a flip-flop.
Tooling Vacuum holes, grooves, and locating pins on the tool plate surface dedicated to a certain size substrate in order to position and hold the substrate during the print cycle of screen printing.
TO package Can-type tC chip configuration, an outgrowth of the original TO transistor package. Most common are the TO-5, TO-18, and TO-47. The IC chip is mounted within the package, interconnected to terminals on the can, and then hermetically sealed. TO stands for transistor outline.
Transistance The characteristic of an electric element which controls voltages or current so as to accomplish gain or switching action in a circuit. Examples of the physical realization of transistance occur in transistors, diodes, saturable reactors, limitors, and relays.
Transistor An active semlconductor device having three or more electrodes, and capable of performing almost all the functions of tubes, including rectification and amplification, Germanium and sillcon are the main materials used, with impurities introduced to determine the conductivity type ( $n$-type as an excess of free electrons, p-type, a deficiency).
Transistor testers Equipment and instruments which detect or measure leakage current, breakdown voltage, gain, or saturation voliage. Some testers are computer operated.
Trigger A timing pulse used to initiate the transmission of logic signals through the appropriate circuit signal paths.

Trimming Removal of film resistor material in order to increase the resistance to a certain value. Two types of equipment are used for this purpose. The air abrasive jet trimming system (AWT) depends on a precisely controlled stream of abraslve particles to carve away small portions of a thick film resistor. Laser syslems are ofien used for both thick and thin fllms. With lasers, the material is burned away.
Truth table A chart which labulates and summarizes all the combinations of possible statos of the inputs and outputs of a circulit It tabulates what will happen at the output for a given input combination.
$T L$, $T^{2} L$ (Transistor-Transistor-Logic) A logic syslem which evolved from DTL wherein the multiple diode cluster is replaced by a multiple-emitter transistor. A circuit which has a multiple emitter inpul and an active pullup network.
Turm-on time The ime required for an output to turn on (sink current, to ground oulput, to go to $0-\mathrm{V}$ ). It is the propagation time of an appropriate input signal to cause the output to go to 0 V .
Turn-off time Same as Turn-on time except the output stops sinking current, goes off and /or goes to a high voltage level (logic "1").
Ultrasonic bond A contact area where two materials are joined by means of ultrasonic energy and pressure.
Ulitrasonic wire honder Equipment unit which fastens fine wire onto substrate by use of ultrasonic energy.
Unit under test (UUT) Any system, set subsystem, assembly, or subassembly undergoing testing.
UV curing Polymerizing, hardening, or cross linking a low molecular weight resinous materlal in a wet coating or ink, using ultraviolet light as an energy system.
VLSI Very large scale integration.
Vaculum evaporation The creation of thin films by vaporizing the film substance and allowing ils deposition onto a substrate through mask openings.
Varistor A two-electrode semiconductor device with a voltage-dependent nonlinear resistance which falls significantly as the voltage is increased.
Via A vertical conductor or conductive path forming the interconnection between multi-Hayer hybrid circuit layers.
Wafer and die sorters. Equipment which automates the testing and sorling of semiconductor devices from wafer form.
Wafer handling equipment Equipment used for processing silicon wafers using methods which include batch processing in a common carrier, air bearing single wafer processing, and a combination of batch and single wafer processing.
Waters Slices of semiconductor crystal materials used as substrates for monolithic ICs, diodes, and tyansistors.
Wet-process benches These are benches or stations used for water processing. Because of the hazardous materials (acids) that are used, they should be designed with personnel safety and contemination control foremost.
Wire hond The fastened union point between a conductor or terminal and the semiconductor die.
Wire, semiconductor lead Fine wire used to connect semiconductor chips to substrete petterns, packages, other chips, etc. Usually made from an aluminum alloy or gold.
Wired "OR" Externally connected separate circuits or functions amranged so that the combination of their outpute results in an "AND" function. The point at which separate circuits are wired together will be an "O" if any one of the separate outputs is an
"O." The same as a dot "AND."
Word A group of bits treated as an entity in a computer.
$X$ axis The horizontal or lett-to-right direction in a two-dimensional system of coordinates.
$\mathrm{X} \times \mathrm{X} \quad$ Signifies one direction followed in a step-and-repeat method.
" $X$ ' motion Registration adjustment left and right of the screen pattem to the substrate, in screen printing.
$Y$ axis The vertical direction, perpendicular to the $X$ axis, in a two-dimensional system of coordinates, $Y$ - $Y$ signifies one direction followed in a step-and-repeat method.
" Y " motion Registration adjustment front to rear of the screen pattern to the substrale, in screen printing.
Zener diode A p-n junction two-terminal, single junction semiconductor device reverse biased into the breakdown region and providing high impedances under less than breakdown voltage but conduction with no impedance above breakdown voltage level.
Zero ("0") See Binary logic.
"Z' motion Vertical adjustment of screen-substrate distance. Used for setting snap-off and leveling in screen printing.
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## CLASSIFICATION OF AMPUFIERS

The definitions of class A, B, or C operation apply to vacuum tubes as well as to transistor circuits. Bias voltage on the emitter junction of a transistor determines collector current jusi as grid voltage determines plate current in a vacuum tube.

Class A allows for $360^{\circ}$ operation of a sine wave.
Class B operation is with zero bias (cutoff) and allows $180^{\circ}$ conduction.
Class $C$ operation is with bias beyond culoff which allows less than $180^{\circ}$ conduction.
Class AB operation allows small-signal class A operation, and large-signal class B operation.
The above classes of operation are defined and illustrated for transistors and vacuum tubes.

| Class | Bias Setting | Input-signal Voltage Swing | Plate or Collector Current Flow | Pertormance Charactoristic |
| :---: | :---: | :---: | :---: | :---: |
| $\mathrm{A}_{1}$ | Center point of characteristic curve | Contined to linear portion of characteristic curve | Complete cycle | Undistorted output. High gain. Low power conversion efficiency. (25\% maximum) |
| $A_{2}$ | Above center point of characleristic curve | Extends into upper (saturation) bend of characteristic curve | Complete cycle | Almost undistorted output. Lower gain but higher efficiency than class $\mathrm{A}_{1}$. |
| $\mathrm{AB}_{1}$ | Below center point of characteristic curve | Extends into lower (cutolf) bend of characteristic curve | Cuts of for a small portion of negative haif-cycle | In push-pull operation output is practically undis. lorted. Lower gain but higher efficiency than class $A_{2}$. |
| $\mathrm{AB}_{2}$ | Center point of characteristic curve | Extends into lower (cutoff) and upper (saturation) bends of characteristic curve | Cuts of for small portion of negative half-cycle | Sllght harmonic distortion in push-pull operation. Lower gain but higher efficiency than class $A B_{1}$ |
| $\mathrm{E}_{1}$ | Near lower bend of characteristic curve | Extends boyond lower (cutoft) bend of characteristic curve | Cuts of for greater part of negative hall-cycle | Little harmonic distortion in push-pull operation. Gain less than class $A B_{2}$. Maximum efficiency 78.5\%, |
| $B_{2}$ | Near lower bend of characleristic curve | Exlends into lower (cutoff) and upper (saturation) bend of characteristic curve | Cuts off for greater part of negative half-cycle and small portion of positive haif-cycle | Some harmonic distortion in push-pull operation. Lower gain but higher efficiency than class $\mathrm{B}_{1}$. |
| C | Beyond lower bend of characteristic curve | Extends well beyond lower (cutoff) and uppor saturation) bends of characteristic curve | Cuts off all of negative and part of positive halfcycles | Considerable harmonic distortion. Low galn. High power conversion efficiency ( $80 \%$ maximum). |
| Subscript 1 demotes that no grid current flows during any part of the cycle. Subscripl 2 denotes that grid current flows at least for a portion of the cycle. In class C amplifiers, grid current always flows, and a subscript is therefore unnecassary. |  |  |  |  |

TRANSISTORS


VACUUM TUBES


## RISETIME OF CASCADED AMPLIFIERS

Two cascaded amplifying devices will have an overall risetime given by:

$$
T_{f_{1}}=\sqrt{T_{r_{1}}^{2}+T_{r_{2}}^{2}}
$$

where $T_{r_{1}}, T_{r_{2}}$, and $T_{r_{1}}$ are the first stage, second slage, and total risetimes respectively.
The above relation is presented in the accompanying graph.
FOR EXAMPLE: A system incorporaling two cascaded amplifiers having risetimes of $100 \mu \mathrm{sec}$ and $25 \mu \mathrm{sec}$ (a ratio of 4:1), would have an overall risetime of $103 \mu \mathrm{sec}$.

NOTE: The Y -axis is the percentage increase in the risetime above the risetime of the slower of two cascaded devices.

Where $A_{1} A_{2} \cdots A_{n}$ are amplifiers with zero output impedance and infinite input impedance

$$
e_{n}=\text { square wave of frequency } F
$$

Then for TILTS of $10 \%$ or less

$$
\% \text { TiLT }{ }_{1}=\pi \frac{F_{1}}{F} \times 100 \text { where } F_{1}=\frac{1}{2 \pi R_{1} C_{1}}
$$

TILTS of 10\% magnitude or less are additive. Thus

$$
\% \mathrm{TILT}_{2}=\pi\left(\frac{F_{1}}{F}+\frac{F_{2}}{F}\right) \times 100
$$

where

$$
F_{2}=\frac{1}{2 \pi R_{2} C_{2}}
$$

and

$$
\% \mathrm{~T}_{\mathrm{TL}}^{n},\left(\frac{F_{1}}{F}+\frac{F_{2}}{F}+\cdots \frac{F_{n}}{F}\right) \times 100
$$

By definition

$$
\% \text { TILT }=\frac{V_{1}-V_{2}}{V / 2} \times 100 \approx \pi \frac{F_{1}}{F} \times 100
$$

where

$$
\begin{aligned}
& F=\text { Frequency of applied wave } \boldsymbol{\theta}_{\text {in }} \\
& F_{1}=\frac{1}{2 \pi \mathrm{RC}} \begin{array}{l}
\text { - cutoff of high pass network }(\mathbf{3} \mathrm{dB}) \\
\mathrm{C} \text { in farads } \mathbf{R} \text { in ohms }
\end{array}
\end{aligned}
$$


(From Electronics and Communications, December, 1968.)

In negative-feedback amplifier considerations, $\beta$ (expressed as a percentage) has a negative value. A line across the $\beta$ and $\mu$ scales will intersect the center scale to indicate resulting change in gain. It also indicates amount (in decibels) by which input must be increased to maintain original output. Original amplification may be expressed as voltage ratio or in decibels by using appropriate scale at right.

FOR EXAMPLE: For a $\beta$ of $10 \%$ and an amplifier $\mu$ of 30 , the nomogram yields a change in $\mu$ of 0.25 .

(Reprinted with permission from International Telephone and Telegraph Corporation

This nomogram determines the available power from the output of class B vacuum tube or transistor push-pull stage operating under the following conditions: The output is a sine wave, the collector or plate swing is twice the supply voltage, and the available output power is determined by the formula

$$
P=\frac{(\sqrt{2} V)^{2}}{z}
$$

FOR EXAMPLE: A transistor amplifier with a $12-\mathrm{V}$ supply and a collector-to-collector impedance of 400 ohms could produce 720 mW of undistorted output power.


## CATHODE FOLLOWER NOMOGRAM

A cathode follower is useful for properly terminating transmission lines and coaxial cables. It provides high $Z_{\text {in }}$ and low $Z_{\text {out }}$ good frequency and phase response, ground common to the input and output, reduced input capacitance, power gain and in-phase input and oulput. To match a transmission line, $R_{0}$ should equal the impedance of the line (A). If $R_{0}$ is less, add a series resistor ( B ), if $R_{0}$ is greater use a resistor ( C ) so that $R=R_{0} Z_{0} /\left(R_{0}-Z_{0}\right)$.

FOR EXAMPLE: To drive a 52 -ohm line using a tube with a $g_{m}$ of 5,000 requires an $R_{0}$ of 70 ohms . To provide proper cathode bias, determine the required cathode resistance from the tube manual or by calculation, and subtract $R_{0}$ to determine $R_{\kappa}$. Assuming that 220 ohms is required for proper bias, the $R_{k}$ is 150 ohms and $R_{0}$ is 70 ohms. If fixed bias is used, $R_{\kappa}$ is not needed.



This nomogram shows the reduction in the gain of an amplifier as a result of negative feedback that is introduced if the cathode resistor is not bypassed.

FOR EXAMPLE: What will be the gain of an amplifier that has an initial stage gain of 20, a cathode resistor of 22 K , and a dynamic plate load resistor of 220 K if the cathode bypass capacitor is removed. The ratio of $R_{L}$ to $A_{K}$ is 10 , thus the resultant "actual" stage gain is 7.

The range of the nomogram can be extended by multiplying all three scales by the same power of 10 .


EUROPEAN TUBE NUMBERING SYSTEM

## Receiving and Amplifying Tubes

| First Letter | Second and Subsequent Letter | Numbers |
| :---: | :---: | :---: |
| Type of Filament or Heater | Electrode StructureClass of Tube | Type of Base |
| A 4 V ac (parallel) <br> C 200 mA heater <br> D $0.5-1.5 \mathrm{~V}$ dc <br> E 6.3 V ac (parallel) <br> G 5 V heater <br> H $12.6 \vee 150 \mathrm{~mA}$ heater (parallel) <br> K 2 V dc (parallel) <br> M 2.5 V <br> O no filament <br> P 300 mA heater <br> (series) <br> U 100 mA heater (series) <br> Z code cathode | A Single diode <br> B Dual diode <br> C Triode, small-signal <br> D Triode, large-signal <br> E Tetrode, small-signal <br> F Pentode, small-signal <br> H Hexode or heptode <br> K Octode, pentagrid converter <br> L. Pentode or tetrode, large-signal <br> M Electron-beam indicator <br> N Thyratron <br> P Secondary emission tube <br> Q Nonode ( 9 electrodes) <br> T Miscellaneous <br> X Gas-filled full-wave rectifier <br> Y Vacuum hali-wave rectifier <br> Z Vacuum full-wave rectifier <br> Two or more of these letters may be combined. Thus ac indicates a diode and a triode in one envelope. | 1 Base indicated by second number <br> 2 Locial <br> 3 Octal <br> 4 European rim-lock <br> 5 Miscellaneous special bases <br> 6,7 Subminiature tube <br> 8 Nine-pin miniature (noval) <br> 9 Seven-pin miniature <br> Second and third digits differentiale between tubes that have the same general description but diflerent characteristics. If the first number is a 1 , then the second number indicates the type of base. |

## FOR EXAMPLE:

Type ECH81 Triode-heptode oscillator converter, with noval socket and 6.3 V heater
Type EL34 Power pentode with octal base and 6.3-V heater
Type GZ34 Full-wave rectifier with octal base and 5 -V heater
NOTE: For special tubes (ruggedized, long-life, etc.), the numbers are placed between the letters. For example: E80F, E90CC, E80CF.

Transmitting Tubes

| First Letter | Second Letter | Third Lelter | Numbers |
| :---: | :---: | :---: | :---: |
| Tube Type | Filament | Cooling Type | Characteristic |
| D Rectifier | A Tungsten, directly heated | G Mercury filled | No uniform |
| M Triode | B Thoriated tungsten, directly heated | L Forced air | notation |
| P Pentode | C Oxide coated, directly heated | W Water cooled | used |
| Q Tetrode | E Heater/cathode | X Xenon filled |  |
| T Triode |  |  |  |

FOR EXAMPLE: Type QQE-04-20 Dual tetrode with indirectly heated cathode

SOUD-STATE SENSING TECHNOLOGIES
This table summarizes the characteristics of solid-state sensors of position, temperature, level, pressure, and speed.

| Sensing Technique | - Actuation | Actuator | Construction | Advantages | Disadvantages |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Hall effect | Proximity | Electromagnet or permanent magnet | Integrated circuit only | Not rate sensitive, fast signal conditioning, simpla | Requires magnet actuator, cannot achieve fine resolution |
| Hall ellect vane | Interrupted | Ferrous material | IC. permanent magnel | Integral design, not rate sensitive, low cost, signal conditioning | Megnet atraclion mode of actuation, cannot achleve fine resolution |
| Eddy current | Proximity | Ferrous or | Coil, IC and nonferrous | All-metal detector, in- | Cannot achieve fine resdiscrete com- |
| olution |  |  | material ponents | discrete comcontaminated, high frequency | tegral unit, not easily |
| Opt-electronic | Interrupted or reflective | Any opaque material | IC, LED, and components | Detects any opaque material, good resolution | Easily contaminated ambient light sensitive |
| Piezoelectric | Impact | Any hard material | Crysla | No stand-by power, potentially lowest cost device | Pulse output, requires impact |
| Piezo-resistance | Pressure or flexing | Gaseous or mechanical | 16 | Detection without mechanical linkage | Complex, difficult construction, expensive for accuracy |
| Variable reluctance (Magnetic) pickup | Proximity | Ferrous | Coil, magnet, IC and discrete components | Fine resolution, integral unit, high speed detection | Cannot sense zero speed, hard signal conditioning, small operate point, complex |
| Capacitance | Touch or proximity | Any material | IC and sensing capacitor | Detects any low dielectric material | False triggering, moisture and temperature sensitive, complex |
| Sonic | Audio beam interrupted or reflected | Any material | Transmitter, receiver, IC and discretes | Large sensing gap, detects any material | Triggered by random noise, not precise, nondirectional |

## SEMMCONDUCTOR MEMORIES

This family tree illustrates the interrelationship of the various types of volatile and nonvolatile semiconductor memories.


VOICE INPUT/OUTPUT FAMILY TREE
Electronic voice input/output capability endows machines with the human qualities of hearing (speech recognition) and speaking (speech output). This family tree highlights some of the current applications of voice input/output equipment.


The cascade noise figure of two noise sources is given by the equation

$$
F_{T}=F_{1}+\frac{\left(F_{2}-1\right)}{G_{1}}
$$

where $F_{1}, F_{2}$, and $F_{T}$ are the first-stage, second-stage, and overall noise figures respecively, and $G$ is the gain of the first stage-all expressed as power ratios. The nomogram has all scales calibrated in decibels. To use the nomogram connect $F_{2}$ and $G$ and note the intersect point on the turning scale. That point is then connected to $F_{T}$ or $F$, depending on which of these figures is given. Two ranges (high and low) are given for all three " $F$ " scales and they must be used together. Only one " $G$ " scate is necessary.

FOR EXAMPLE: A first-stage noise figure of 3 dB , a second-stage noise figure of 7 dB , and a first-stage gain of 8 dB , results in an overall noise figure of 4.2 dB .


## Section 5

# Mathematical Data, Formulas, Symbols 

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## RELIABUUTY CHARTS

This chant refates syslem MTBF (Mean-Time-Between-Failures) with the number of components per sysiem and the component MTBF.

FOR EXAMPLE: A system using 10,000 components with a component MTBF of 30 years will have a system MTBF of 1 day.


This chart relates system reliability in percent with the numberof serial parts, that is, the critical parts that must function in order for the system to perform ils function.

FOR EXAMPLE: 10,000 critical parts with a $99.99 \%$ parts reliability provide a system reliability of only $37 \%$.


## RELIABILITY NOMOGRAM

Reliability is a dependent function of operating time and failure rate. It is generally given as a percentage or a decimal that states the probability that an equipment will perform its function satisfactorily during a mission. Reliability is based on the formula

$$
P_{0}=e^{-t T}=e^{-\lambda t}
$$

where

$$
\begin{aligned}
T & =1 / \lambda & t & =\text { operating time in hours } \\
P_{0} & =\text { probability of success, i.e., rellability } & T & =\text { mean time between failures } \\
e & =\text { base of natural logarithm } & \lambda & =\text { failure rate (\% per } 1,000 \mathrm{hr})
\end{aligned}
$$

FOR EXAMPLE: A circuit that has a falure rate of $100 \% / 1,000 \mathrm{hr}$ (an hourly failure rate of 0.001 or an MTBF of 1,000 ) has a reliability of $99.8 \%$ when operated for 2 hr . That means that the circuit will not operate properly an average of 2 times out of 1,000 operations, or out of 1,000 circuits an average of 2 will fail in 2 hr .

NOTE: An equipment or circuit with an MTBF of one hour will have a reliability of only $33.788 \%$ ( $100 / e$ ) when operated for one hour.

NOTE: For more detailed treatment of MTBF see the latest edition of M/L-Hanabook-217.


## RELIABILITY—REDUNDANCY NDMOGRAM

For certain critical applications, such as manned space flights, the required reliability is often greater than what can be achieved with a single system. Under these conditions it is necessary to resort to redundancy where two or more identical systems are paralleled. The required redundancy is based on the following equation:

$$
P_{N}=1-\left(1-P_{0}\right)^{N}
$$

## where

$P_{N}=$ probability of success of $N$ paralleled systems
$P_{0}=$ probability of success of one system
$N=$ number of paralleled systems
FOR EXAMPLE: A subsystem for a two-week moon exploration flight has a special reliability of $99.99 \%$ and a MTBF of $2,000 \mathrm{hr}$. What is the required redundancy? On reliability nomogram (A) connect 2,000 on the $T$ scale with 336 (2 weeks) on the $t$ scale to determine subsystern reliability to be 0.845 . On redundancy nomogram connect 0.845 on the $P_{o}$ scale with 0.9999 on the $P_{N}$ scale to determine that a redundancy of five is required.


This graph is used to determine the minimum MTBF for a given confidence level. To use the chart, determine the actual number of Operating Hours, the Observed Failures, and the required Confidence Level. Read across from "Observed Failures" to "Confidence Level" and then down to obtaln the "Divisor." Divide the number of Operating Hours by the "Divisor." The result is the minimum MTBF for the stated Confidence Level.

FOR EXAMPLE: During $\mathbf{2 , 0 0 0}$ hours of operation there were 8 failures. What is MTBF stated with a confidence levet of $90 \%$ ? Reading across 8 to the $90 \%$ curve shows the divisor to be 13. Dividing 2,000 by 13 yields approximately 154 . Thus, it can be said that the MTBF (minimum) is 154 hours with a confidence of $90 \%$. If, in the above example, a confidence level of $70 \%$ had been required, then it could be said that the MTBF was 194 hours with a contidence level of $70 \%$.


The shaft angle corresponding to an integral binary fraction is required wherever shaft angle encoders are used. This resolution table aids in determining accurately the angle represented by a specific number of counts or conversely, the precise number of counts which equals a given angle.

| n |  | $7^{\text {-n }}$ | Angular Resolution Corresponding to Imegral-Exponent Bibibary Fraction |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | m |  | $1296000 / 7{ }^{\text {n }}$ (seconds) | $21.000 / 2^{7 n}$ (minutes) | 360/27 (degrees) |  |  |
| 0 |  |  | 1296000 | $21+8)$ | 360.0 | 6. $28818853071795884780^{\circ}$ | 0 |
| , |  | 3 | -48000 | 10800 | 190.0 | 1. 1215159265359997932388 +6 | , |
| 2 |  | ${ }^{3}$ | 324000 | 5400 | 90.0 |  | \% |
| 3 | * | 18 | 162000 | 2700 | 45.0 | .795 398163397448309615 | 3 |
|  | 16 | ous ${ }^{\text {a }}$ | 81000 | 1350 | 22.5 | . 39260008161698724154898 | ; |
| ? | ${ }_{4}^{32}$ | - 0128 | -0580 | ${ }_{3}^{675}$ |  |  | S |
|  | 178 | (00)8123 | 1012 | 168.75 |  |  |  |
| , | 86 | $0 \times 2 \infty$ | S $x_{2} 5$ | 84, 378 | 1.40625 |  | ${ }^{8}$ |
|  | 517 | -014 |  |  |  |  |  |
| 10 | 1034 | 0009765023 | $1{ }^{2} \mathbf{4}$. 685 | 21.09375 | ,331562 5 | .006 1359893515151550105989 | 10 |
|  | 7048 | 00084898123 | 62. 12125 | 10.946875 | . 17378125 |  | 11 |
| 17 | . 006 | 00034140825 | J16.404 25 | 5,271437 5 | . 087808025 |  | 17 |
| 12 | 1102 | 0001270703125 | 158203120 | 2.625 7188 | ,0139493912 3 | .00070000309007877 016800 | 13 |
|  | 10884 | cose mat ass 158 | * 9.10150025 | 1.318339375 |  |  | 14 |
| 13 | ${ }^{37} 76$ | 00002011>5914 | *. 3502017 | , 651010675 | . 010 95 328 126 | . 000191774398485703135 ils |  |
| 18 |  | 000015307800875 | 197500025 | . 374589894373 |  |  |  |
| 18 | listor |  |  |  | © $\infty 27$ 276 58203122 |  | 18 |
| 19 | 32848 |  | 2.471923828125 | .041 19673048858 | . 00088650450078125 | 0000 011,980 723 $005236597310 \%$ ? | 18 |
| 2 | 104518 |  | 1.2159819160023 |  | 1000 219322275390623 |  | \% |
| 22 | 2007152 | 0000004780477158 | 61908089797125 | . 010 208082617 1875 | .000 171 66613748983125 |  | 21 |
| 23 | - 1904308 | 000000220416381015025 | . 2089000478515625 | . 005149886130859375 | .000 085839688647656625 |  | 2 |
| 23 | I 308000 |  | 1540952392578125 |  | .000 0229153423828125 |  | 23 |
| 24 | 16 m7 214 |  |  | .001287400.37 1484375 | .000 021457672119140625 |  | 24 |
| 25 | 3354482 |  | .038 0238098141433125 | .000 54073018357421875 | . 0000107288360595703125 | .000 $000198785351414819848 \times 178$ | $\checkmark$ |


| $\begin{aligned} & \text { words } \\ & \text { (Englis) } \end{aligned}$ | HATHEMATICS （Sel Theory） | logic | engineering | GEOHETRICAL DIAGRAWS |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  of an element． |  | $O \wedge \theta=0$ | $\begin{aligned} & 0+0=0 \\ & 0 \cdot a=0 \end{aligned}$ |  |  |
| 2 THE LAWS OF COMMMUTKTION，Disjunclion or conjanction is not alfected by sequential change． JOusperfion－0 ；sither inpul a or inpul $b$ ，or beth ingets a and the are ronducling，then the antpu！ only T ．both inpuls a and b are conducting．then the outpul ？－W is conoucting．I | aUb $=$ bua anbiona | $O \vee D=\Delta V O$ <br> a＾力．b＾o | $a+b=b+a$ <br> $0 \cdot b=0 \cdot 0$ |  |  |
| 3．The taHm or ASSOCIAIGN．Disjunction or con jemection is capelected by nomping． | soubluc： <br> auloues <br> tonolnc： <br> $o n(o \cap a)$ | $(a \mathrm{Vb}) \mathrm{Vc}=$ ov（bva） <br> （ $0 \wedge$ b）$A c=$ <br> $\sigma \wedge(b \wedge c)$ | $\begin{gathered} (a+b)+c= \\ 0+(0 . c) \\ \\ (0 . b) \cdot c= \\ 0 \cdot(0 . c) \end{gathered}$ |  |  |
|  to a wodext to zemme he elemant to act membet <br>  | $o$ 山（bกc）＝ （aubinfouc） <br> on $(\Delta \cup c)=$ （o円b）U（bกc） | $a \vee(0 \wedge c)=$ <br> －（ovolanga） <br>  lonb）V（oAc） | $\begin{aligned} & 0+(0 . c)= \\ & (0+b) \cdot(0 . c) \\ & 0 \cdot(b+c)= \\ & (0 . b)+(0 . c) \end{aligned}$ |  |  |
|  <br>  | $a \cup(a \cap b)=a$ <br> 0 तीto U b）$=0$ | $\sigma \vee(O \wedge b)=0$ $O A\|Q \vee D\|=0$ | $\begin{aligned} & 0+(0 \cdot 0)=0 \\ & 0 \cdot(0+0)=0 \end{aligned}$ | $\begin{aligned} & \text { 80y } \\ & \end{aligned}$ |  |


| CIRCUIT DIAGRAMS | TRUTH TABLES (1 = fruth, 0 - folsity) |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0 <br> 1 <br> 0 | $\frac{0}{1}$ |  |  |  |  |  |  |  |  |  |  |  |
|  | 0 <br> 1 <br> 1 <br> 0 <br> 0 | 0 1 0 1 0 | $a+b$  <br> 1  <br> 1  <br> 1 0 | $+b$ $b * a$ <br> 1 1 <br>  1 <br>  1 | 0.0 <br> 1 <br> 0 <br> 0 <br> 0 | 0.0 <br> 1 <br> 0 <br> 0 |  |  |  |  |  |  |  |
|  | 0 <br> 1 <br> 1 <br> 1 <br> 1 <br> 0 <br> 0 <br> 0 <br> 0 | 0 1 1 0 0 1 0 0 1 0 | 6 <br> 1 <br> 0 <br> 1 <br> 0 <br> 1 <br> 1 <br> 0 <br> 0 | $a+b$  <br> 0 1 <br>  1 <br>  1 <br>  1 <br>  1 <br> 0 1 <br> 0 0 | $0+c$ <br> 1 <br> 1 <br> 1 <br> 1 <br> 1 <br> 1 <br> 1 <br> 0 <br> 0 | $c\|c\|$  <br> 1  <br> 1  <br> 1  <br> 0  <br> 1  <br>  1 <br> 0 1 |  | 00 <br> 1 <br> 1 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 |  | 0.6 | 早¢ <br> 1 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 |  |  |
|  | 0 <br> 1 <br> 1 <br> 1 <br> 1 <br> 1 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 | $b$ <br> 1 <br> 1 <br> 1 <br> 0 <br> 0 <br> 1 <br> 0 <br> 1 <br> 0 | 6  <br>  1 <br>  0 <br> 0 1 <br> 0 0 <br>  1 <br>  1 <br> 0 0 | 0.0  <br>  1 <br> 0 1 <br>  0 <br>  0 <br>  0 <br> 0 0 <br> 0 0 | $0 . c$  <br> 1 0 <br> 1  <br> 0  <br> 0  <br> 0  <br> 0  <br> 0  | $c$ $0+c$ <br>  1 <br>  0 <br>  0 <br>  0 <br>  1 <br>  0 <br>  0 | \|l|l | 10+c | (1) 0 | 3 <br> 0 <br> $\vdots$ <br> $*$ <br> 0 <br> 1 <br> 1 <br> 1 <br> 1 <br> 1 <br> 1 <br> 1 | 等 | 6 <br> 0 <br> 0 <br> 0 <br> 1 <br> 1 <br> 1 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 |  <br>  <br>  <br>  <br> 0 <br>  <br> 1 <br> 1 <br> 1 <br> 1 <br> 0 <br> 0 <br> 0 <br> 0 |
|  | 0 <br> 1 <br> 1 <br> 0 <br> 0 | $b$ 1 0 0 1 0 | $a$ $0, b$ <br> 1 1 <br> 0 0 <br> 1 0 <br> 0 0 | $\square$ | $10 n b$  <br> 1 1 <br> 1  <br>  0 |  |  |  |  |  |  |  |  |


|  | WORD5 <br> (English) | MATHEMATICS (Set Theory) | LOGIE | ENGINEERING | GEOMEYRICAI DIAGRAMS |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1. THE LAWS Of THE UNWERS! CIASS Tin sum conasising of an Element and the priverse class is equivident to the unierse chas, The buduct consisting of an element and the univelist ciass is equivalent to the element. | $a \cup 1=1$ $o \Pi 1=0$ | $o \vee I=1$ $a \wedge 1=\sigma$ | $0+1=1$ $o \cdot 1=a$ |  |  |
| THE LAWS OF THE | 2 THe wais of THE thut class the sum consustang of an zermed mad the null class is equira: lemt to the cipzent lime presact consisting ol an elem:ent and the nult titss is asemitert to the ruth thes. | $a \cup 0=0$ $a \cap 0=0$ | $o v 0=0$ $O A O=0$ | $0+0=0$ $0.0=0$ |  |  |
|  |  sistiafol of wement and its complement is equive: Lent 10 dike unfiveras elass. The product consisling of metement amb its complement is equissient to the null class. | $0 \cap 0^{\circ}=0$ | $o v-q=1$ $o A-o=0$ | $0+\bar{a}=1$ $\sigma \cdot \bar{\sigma}=0$ |  |  |
|  |  is *trostem to ise complement of an etement b. it is ampled inat tee eterent is equivalent to the somprecent et bse elerictt 1 | $o=b^{\prime} \cdot \exists \cdot b \cdot a^{4}$ |  | $0=\vec{b} \cdot \nabla_{-b}=\vec{a}$ |  |  |
| $\underset{\text { 花 }}{\underset{\sim}{2}}$ | 3. The lait of douele hecition lime condlemient of the neation ol an element is egrudent to the flement | $0=0^{\circ} \mathrm{C}$ | $\theta=\sim a^{\prime}$ | $\theta=\bar{\square}^{\prime \prime}$ |  |  |
|  | 4. TEE LAWS OF EXPRMSION. The disfunction of a proanct camposec of the elemenit a ind bo and a podeded composed al the elements and the complement of element bis equizitent to the :lement a the canpurtics of s sum andoosed of the elegents a and $\mathbf{b}$ and a san cooposed of the element a and lie compenent ol enerral th is equivilent 10 the sibment | $(o \cap b) \cup\left(o \cap b^{\prime}\right)=0$ <br> $\{a \cup b\} \cap\left\{a \cup b^{\prime}\right\}=0$ | $(0 \wedge b)\left(o A_{-}-b\right) * o$ $\{o \vee o, n t a \vee \sim b\}=0$ | $\{0.0),(0 . \bar{b})=0$ $\{a \times b) \cdot(a+\bar{b})=a$ |  |  |
|  | 5. THE LAWS OF DUALIFY The complement of a sum connposed of the alonients a jed h is equivalent to the corfiuntion of the complemint al element : and the complement of clemsal t, Tho complement al a ptoduct compasto of the slemeals a and bits equivaleat to the disunction al thic compleferient on elenental and the complement of element $b$. | $\{o \cup b\}^{\prime}=a^{\prime} \cap b^{\prime}$ $\lfloor\cap \cap b)^{\prime}=a^{\prime} \cup b^{\prime}$ | $\begin{aligned} & \sim(o \vee b)=\sim a \wedge \sim b \\ & \sim(0 \wedge \theta)=\sim O \vee \sim b \end{aligned}$ | $(a+b)^{\prime}=\bar{b} \cdot \vec{b}$ $(o-b)^{\prime}=\bar{a}+\bar{b}$ |  |  |



## Boolean Relationships

Idempoint:
$a+0=a \quad a 0=0 \quad$ where
$a+1=1 \quad a 1=a \quad 0 \equiv \bar{a}$
$a+a=a \quad a a=a$
Commutative: $a+b=b+a$

$$
a b=b a
$$

Associative: $(a+b)+c=a+(b+c)$

$$
(a b) c=a(b c)
$$

Distributive: $a b+a c=a(b+c)$

$$
a+b c=(a+b)(a+c)
$$

Absorption: $a(a+b) \equiv a+a b \equiv a$
DeMorgan Theorem: $\overline{\bar{a}}=a$

$$
\begin{aligned}
& (\overline{a b})=\bar{a}+\bar{b} \quad \frac{(\overline{a b})}{(a b}=a+b \\
& \overline{a+b}=\overline{a b} \quad \frac{\bar{b}+\bar{b}}{\bar{a}}=a b
\end{aligned}
$$

Basic Logic


Clocked Logic Elements


## CONVERSION CHART OF STANDARD METRIC PREFIXES

This chart shows, in their relative positions, symbols, multiples ( $10^{2}$ ), and abbreviations for all the international multiples and submultiples as recommended by the International Committee on Weights and Measures (1962) and adapted by the National Bureau of Standards.

This chart provides a fast and easy method of conversion from any metric notation to any other. "Unity" represents the basic unit of measurement such as volts, ohms, watts, amperes grams, hertz, etc. The number of steps up or down between the two prefixes which are being compared is equal to the direction and the number of places in which the decimal point has to be moved to convert from one to the other.

FOR EXAMPLE: To convert 0.0032 milliampere to nanoampere-move six places down. Answer: $3,200 \mathrm{nA}$.
To convert 43,280 kilohertz to megahertz-move three places up. Answer: 43.28 MHz .
To convert 10.74 microns to millimeters-move three places up. Answer: 0.01074 mm .


## HARMONIC REJECTION NOMOGRAM

This scale relates the magnitude of harmonic distortion, expressed as a rejection ratio in decibels, to percentage of distortion.

FOR EXAMPLE: (1.) A design specifies that a given audio sine-wave oscillator should have its closest harminic at least 28 dB below the fundamental. The chart indicates that the closest harmonic must be less than $3.9 \%$ of the magnitude of the fundamental.
(2.) Find the harmonic content of a signal made up of the following:
Fundamental frequency
100 V ms
Second harmonic
5 V ms
Third harmonic
2 V ms

Adding harmonics vectorially gives

$$
\sqrt{5^{2}+2^{2}}=5.39
$$

\% distortion $=\frac{\text { harmonic voltage }}{\text { fundamental voltage }} \times 100=\frac{5.39}{100} \times 100$

Thus the distortion is $5.30 \%$, which means that the harmonic content of the signal is 25.2 dB below the fundamental.


$2^{-11}$
0
1.0
0.5
0.25
0.125
0.0625
0.03125
0.015625
0.0078125
0.00390625
0.001953125
0.0009765625
0.00048828125
0.000244140625
0.0001220703125
$0.000 \quad 061035 \quad 156 \quad 25$
$0.000 \quad 030 \quad 517 \quad 578125$
$0.000 \quad 015 \quad 254789062$ \$
$\begin{array}{llllll}0.000 & 015 & 258 & 789 & 062 & \$ \\ 0,000 & 007 & 829 & 394 & 531 & 25\end{array}$
$0.000 \quad 0031814697 \quad 265624$
0.000 D01 $507348632812 \$$
$0.000 \quad 000 \quad 959674316 \quad 406 \quad 25$
$0.000 \quad 000 \quad 476 \quad 837158203125$
$\begin{array}{llllllllllll}0.000 & 000 & 238 & 41 & 579 & 101 & 562 & 5\end{array}$
$0.000000119209289550 \% 78123$
$\begin{array}{llllllll}0.000 & 000 & 119 & 209 & 289 & 580 & 781 & 25 \\ 0.000 & 000 & 059 & 604 & 644 & 775 & 350 & 625\end{array}$
$\begin{array}{lllllllll}0.000 & 000 & 059 & 604 & 644 & 775 & 350 & 625 \\ 0.000 & 000 & 029 & 802 & 322 & 387 & 695 & 312 & 5\end{array}$
$\begin{array}{llllllllllll}0.000 & 000 & 014 & 901 & 161 & 193 & 547 & 656 & 25\end{array}$

$0.000 \quad 000 \quad 003725 \quad 2902984619140825$ $0.000 \quad 000 \quad 00186254514923095703125$

| 0 | $2^{4}$ |
| :---: | :---: |
| 73 | 9444732965739290427392 |
| 74 | 18889 \$6593 1478580854784 |
| 75 | 377789318829571 61709 568 |
| 76 | 75557863725914328419136 |
| 77 | 151115727451828 B4683 6272 |
| 78 | 302231454903657293678514 |
| 79 | 604462909807314587353088 |
| 80 | 120892581961462917470178 |
| 81 | 2417851639229258348412352 |
| 82 | 483570327845851 669BA 24704 |
| 83 | 967140655691703 33976 49400 |
| 84 | 1934281311 3434086783 2982 |
| 85 | 3868562622766813359059783 |
| 86 | 77371252455336267181 19826 4 |
| 87 | 154742504910672534382395528 |
| 88 | $30948500 \% 21345068724781055$ |
| 89 | 518970010642690137449582112 |
| 90 | 12378400392853840274890124224 |
| 91 | 24758800785707605407 9024c 440 |
| 92 | 4951760157141521090690496896 |
| 93 | 9903520314283042190192993792 |
| 94 | 19807040828548004300385987584 |
| 95 | 39514081251132188790711075185 |
| 96 | 79228162514204337593543950258 |
| 97 | 158456325028528675187087900672 |
| 98 | 316912650057057350374175801344 |
| 99 | 633825300114114700748351602048 |
| 100 | 1267650600228229401496703203378 |

288435 456
336870912

| 1 | 073 | 741 | 824 |
| :--- | :--- | :--- | :--- |
| 2 | 147 | 48 |  |

2147487646
4294967 216
$8 \quad \$ 89934592$
$17 \quad 179869184$ 3435973836 68719476736 68719476736 $\begin{array}{llll}137 & 438 & 953 & 472 \\ 274 & 877 & 906 & 94\end{array}$ 349 15s 183 84 1098511627776 $2199023255 \$ 52$ 4394046311104 - 796093022209 17592186040416 35 184 372 ntall 132 $\begin{array}{lllllll} & 70 & 368 & 744 & 177 & 654\end{array}$ 140737 4B6 355 32d 2a1 474976710636 562949953421312 125899906842624 2251799613685248 $\begin{array}{llllll}2 & 251 & 799 & 613 & 685 & 240 \\ 4 & 503 & 599 & 627 & 370 & 496\end{array}$ $\begin{array}{lllllll}9 & 007 & 199 & 254 & 740 & 992\end{array}$ 18014390509481904 3602879701896.3 968 72 057 594037927936 $\begin{array}{llllllllllll}144 & 115 & 188 & 075 & 855 & 672\end{array}$ $\begin{array}{llllllll}288 & 230 & 376 & 151 & 711 & 744\end{array}$ $\begin{array}{lllllll}576 & 460 & 752 & 303 & 423 & 488\end{array}$ $1152921 \cdot 5046061846976$ $2305843 \quad 005 \quad 213 \quad 693 \quad 952$
4 611 686018427387904
9223372036 144 775 80d
18446744073709551616
35893493147419103232

71736976294138206464
147573952569676412926
$398 \quad 147905 \quad 179 \quad 352 \quad 325 \quad 356$
 180591620717411303424 361 165241434822606848 132236648286984513656

$$
0.000 \quad 000000 \quad 931322574 \quad 815478 \quad 515824
$$

$\begin{array}{llllllllll}0.000 & 000 & 000 & 931 & 322 & 574 & 515 & 478 & 513 & 824 \\ 0.000 & 000 & 000 & 465 & 561 & 287 & 307 & 739 & 257 & 12\end{array}$
$0.000000000232830543,653889628506$ 2s
$0.000000000116415321826 \quad 934814453125$
0.00010000000582078609134671072265625

0.000000000014551915229366851806840625

$\begin{array}{llllllllllll}0.000 & 000 & 000 & 007 & 275 & 957 & 614 & 183 & 425 & 903 & 380 & 312\end{array}$

0.000000000 000 9094947017129281379150390625

0.000000 b00 000227373675443232059476759765625
0.000500000000113666137721616027393798828123


 $\begin{array}{llllllllllllllll}0.000 & 000 & 000 & 000 & 014 & 210 & 854 & 715 & 202 & 003 & 717 & 422 & 485 & 351 & 962 & 5 \\ 0.000 & 000 & 000 & 000 & 007 & 105 & 427 & 357 & 601 & 001 & 858 & 711 & 242 & 675 & 781 & 25\end{array}$ $\begin{array}{lllllllllllllllllll}0.000 & 000 & 004 & 000 & 007 & 105 & 427 & 357 & 601 & 001 & 858 & 711 & 242 & 675 & 781 & 25 \\ 0.000 & 000 & 000 & 000 & 003 & 552 & 713 & 678 & 800 & 500 & 989 & 355 & 621 & 337 & 890 & 625\end{array}$

























| $n$ | $n^{2}$ | $\sqrt{n}$ | $\sqrt{10 n}$ | $n$ | $n$ | $\sqrt[3]{n}$ | $\sqrt[3]{10 n}$ | $\sqrt[3]{100 n}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1 | 1.000000 | 3.162278 | 1 | 1 | 1.000000 | 2.154435 | 4.641589 |
| 2 | 4 | 1.414214 | 4.472136 | 8 | 2 | 1.259921 | 2.714418 | 5.848035 |
| 3 | 9 | 1.732051 | 5.477226 | 27 | 3 | 1.442250 | 3.107233 | 6.694330 |
| 4 | 16 | 2.000000 | 6.324555 | 64 | 4 | 1.587401 | 3.419852 | 7.368063 |
| 5 | 25 | 2.238088 | 7.071068 | 125 | 5 | 1.709976 | 3.684031 | 7.937005 |
| 6 | 36 | 2.449490 | 7.745967 | 216 | 6 | 1.817121 | 3.914868 | 8.434327 |
| 7 | 49 | 2.845751 | 8.368600 | 343 | 7 | 1.912931 | 4.121285 | 8.879040 |
| 8 | 64 | 2.828427 | 8.944272 | 512 | 8 | 2.000000 | 4.308869 | 9.283178 |
| 9 | 81 | 3.000000 | 9.486833 | 729 | 9 | 2.080084 | 4.481405 | 9.654894 |
| 10 | 100 | 3.162278 | 10.00000 | 1,000 | 10 | 2.154435 | 4.641589 | 10.00000 |
| 11 | 121 | 3.316825 | 10.48809 | 1,331 | 11 | 2.223980 | 4.791420 | 10.32280 |
| 12 | 144 | 3.464102 | 10.95445 | 1,728 | 12 | 2.289428 | 4.932424 | 10.62659 |
| 13 | 169 | 3.605551 | 11.40175 | 2,197 | 13 | 2.351335 | 5.065797 | 10.91393 |
| 14 | 196 | 3.741657 | 11.83216 | 2,744 | 14 | 2.410142 | 5.192494 | 11.18689 |
| 15 | 225 | 3.872983 | 12.24745 | 3,375 | 15 | 2.466212 | 5.313293 | 11.44714 |
| 16 | 256 | 4.000000 | 12.64911 | 4,096 | 16 | 2.519842 | 5.428835 | 11.69607 |
| 17 | 288 | 4.123106 | 13.03840 | 4,913 | 17 | 2.571282 | 5.539658 | 11.93483 |
| 18 | 324 | 4.242641 | 13.41641 | 5,832 | 18 | 2.620741 | 5.646216 | 12.16440 |
| 19 | 361 | 4.358899 | 13.78405 | 6,859 | 19 | 2.688402 | 5.746897 | 12.38562 |
| 20 | 400 | 4.472136 | 14.14214 | 8,000 | 20 | 2.714418 | 5.848035 | 12.59921 |
| 21 | 441 | 4.582576 | 14.49138 | 9,261 | 21 | 2.758924 | 5.943922 | 12.80579 |
| 22 | 484 | 4.690416 | 14.83240 | 10,648 | 22 | 2.802039 | 6.036811 | 13.00591 |
| 23 | 529 | 4.795832 | 15.16575 | 12,167 | 23 | 2.843867 | 6.126926 | 13.20006 |
| 24 | 576 | 4.898979 | 15.49193 | 13,824 | 24 | 2.884499 | 6.214465 | 13.38866 |
| 25 | 625 | 5.000000 | 15.81139 | 15,625 | 25 | 2.924018 | 6.299605 | 13.57209 |
| 26 | 676 | 5.099020 | 16.12452 | 17,576 | 26 | 2,962496 | 6.382504 | 13.75069 |
| 27 | 729 | 5.196152 | 16.43168 | 19,683 | 27 | 3.000000 | 6.463304 | 13.92477 |
| 28 | 784 | 5.291503 | 16.73320 | 21,952 | 28 | 3.036589 | 6.542133 | 14.09460 |
| 29 | 841 | 5.385165 | 17.02939 | 24,389 | 29 | 3.072317 | 6.619106 | 14.26043 |
| 30 | 900 | 5.477226 | 17.32051 | 27,000 | 30 | 3.107233 | 6.694330 | 14.42250 |
| 39 | 951 | 5.567764 | 17.60682 | 29,791 | 31 | 3.141384 | 6.767899 | 14.58100 |
| 32 | 1.024 | 5.656854 | 17.88854 | 32,788 | 32 | 3.174802 | 6.899904 | 14.73613 |
| 33 | 1,089 | 5.744563 | 18.16590 | 35,937 | 33 | 3.207534 | 6.910423 | 14.88806 |
| 34 | 1,156 | 5.830952 | 18.43909 | 39,304 | 34 | 3.239612 | 6.979532 | 15.03695 |
| 35 | 1,225 | 5.916080 | 18.70829 | 42,875 | 35 | 3.271066 | 7.047299 | 15.18294 |
| 36 | 1,296 | 6.000000 | 18.97367 | 46,656 | 38 | 3.301927 | 7.113787 | 15.32619 |
| 37 | 1,369 | 6.082763 | 19.23538 | 50,653 | 37 | 3.332222 | 7.179054 | 15.46680 |
| 38 | 1,444 | 6.164414 | 19.49359 | 54,872 | 38 | 3.361975 | 7.243156 | 15.80491 |
| 39 | 1,521 | 6.244998 | 19.74842 | 59,319 | 39 | 3,391214 | 7.306144 | 15.74061 |
| 40 | 1,600 | 6.324555 | 20.00000 | 64,000 | 40 | 3.419952 | 7.366063 | 15.67401 |
| 41 | 1.681 | 6.403124 | 20.24846 | 68,921 | 41 | 3.448217 | 7.428959 | 16.00521 |
| 42 | 1,764 | 6.480741 | 20.49390 | 74,088 | 42 | 3.476027 | 7.4888872 | 16.13429 |
| 43 | 1,849 | 6.557439 | 20.73644 | 79,507 | 43 | 3.503398 | 7.547842 | 16.26133 |
| 44 | 1,936 | 6.633250 | 20.97618 | 85,184 | 44 | 3.530348 | 7.605905 | 16.38643 |
| 45 | 2,025 | 6.708204 | 21.21320 | 91,125 | 45 | 3.556893 | 7.663084 | 16.50964 |
| 46 | 2,116 | 6.782330 | 21.44761 | 97,336 | 46 | 3.583048 | 7.719443 | 16.63103 |
| 47 | 2,209 | 6.855655 | 21.67948 | 103,823 | 47 | 3.608826 | 7.774980 | 16.75069 |
| 48 | 2,304 | 6.928203 | 21.90890 | 110,592 | 48 | 3.634241 | 7.829735 | 16.86865 |
| 49 | 2,401 | 7.000000 | 22.13594 | 117,649 | 49 | 3.659306 | 7.683735 | 16.98499 |
| 50 | 2.500 | 7.071068 | 22.36068 | 125,000 | 50 | 3.684031 | 7.937005 | 17.09976 |


| $n$ | $n^{2}$ | $\sqrt{n}$ | $\sqrt{10 n}$ | $n^{\text {I }}$ |
| :---: | :---: | :---: | :---: | :---: |
| 50 | 2,500 | 7.071068 | 22.36068 | 125,000 |
| 51 | 2,601 | 7.141428 | 22.58318 | 132,651 |
| 52 | 2,704 | 7.211103 | 22.80351 | 140,608 |
| 53 | 2,809 | 7.280110 | 23.02173 | 148,877 |
| 54 | 2,916 | 7.348469 | 23.23790 | 157,464 |
| 55 | 3,025 | 7.416198 | 23.45208 | 166,375 |
| 56 | 3,136 | 7.483315 | 23.66432 | 175,616 |
| 57 | 3,249 | 7.549834 | 23.87467 | 185,193 |
| 58 | 3,364 | 7.615773 | 24.08319 | 195,112 |
| 59 | 3,481 | 7.681146 | 24.28992 | 205,379 |
| 60 | 3,600 | 7.745967 | 24.49490 | 216,000 |
| 61 | 3,721 | 7.810250 | 24,69818 | 226,981 |
| 62 | 3,844 | 7.874008 | 24.89980 | 238,328 |
| 63 | 3,969 | 7.937254 | 25.09980 | 250,047 |
| 64 | 4,096 | 8.000000 | 25.29822 | 282,144 |
| 65 | 4,225 | 8.062258 | 25.48510 | 274,625 |
| 66 | 4,356 | B. 124038 | 25.69047 | 287,496 |
| 67 | 4,489 | 8.185353 | 25.88436 | 300,763 |
| 68 | 4,624 | 8.246211 | 26.07681 | 314,432 |
| 69 | 4,761 | 8.306624 | 26.26785 | 328,509 |
| 70 | 4,900 | 8.366600 | 26.45751 | 343,000 |
| 71 | 5,041 | 8.428150 | 28.64583 | 357,911 |
| 72 | 5,184 | 8.485281 | 26.83282 | 373,248 |
| 73 | 5,329 | 8.544004 | 27.01851 | 389,017 |
| $74$ | 5,476 | 8.602325 | 27.20294 | $405,224$ |
| 75 | 5,625 | 8.660254 | 27.38613 | 421,875 |
|  | 5,776 | 8.717798 | 27.58810 | 438,976 |
| 77 | 5,929 | 8.774964 | 27.74887 | 458,533 |
| 78 | 6,084 | 8.831761 | 27.92848 | 474,552 |
| 79 | 6,241 | 8.888194 | 28.10694 | 493,039 |
| 80 | 6,400 | 8.944272 | 2 B .28427 | 512,000 |
| 81 | 6,561 | 9.000000 | 28.46050 | 531,441 |
| 82 | 6,724 | 9.055385 | 28.63564 | 551,368 |
| 83 | 6,889 | 9.110434 | 28.80972 | 571,787 |
| 84 | 7,056 | 9.165151 | 28.98275 | 592,704 |
| 85 | 7,225 | 9.219544 | 29.15476 | 614,125 |
| 86 | 7,396 | 9.273618 | 29.32576 | 636,056 |
| 87 | 7,569 | 9.327379 | 29.49576 | 658,503 |
| 88 | 7,744 | 9.380832 | 29.66479 | 681,472 |
| 89 | 7,921 | 9.433981 | 29.83287 | 704,969 |
| 90 | 8,100 | 9.486833 | 30.00000 | 729,000 |
| 91 | 8,281 | 9.539392 | 30.16621 | 753,571 |
| 92 | 8,464 | 9.591663 | 30.33150 | 778,688 |
| 93 | 8,649 | 9.643651 | 30.49590 | 804,357 |
| 94 | 8,836 | 9.695360 | 30.65942 | 830,584 |
| 95 | 9,025 | 9.746794 | 30.82207 | 857,375 |
| 96 | 9,216 | 9.797959 | 30.98387 | 884,736 |
| 97 | 9,409 | 9.848858 | 31.14482 | 912,673 |
| 98 | 9,604 | 9.899495 | 31.30495 | 941,192 |
| 99 | 9,801 | 9.949874 | 31.46427 | 970,299 |
| 100 | 10,000 | 10.00000 | 31.62278 | 1,000,000 |


| $n$ | $\sqrt[3]{n}$ | $\sqrt[3]{10 n}$ | $\sqrt[3]{100 n}$ |
| :---: | :---: | :---: | :---: |
| 50 | 3.684031 | 7.937005 | 17.09976 |
| 51 | 3.708430 | 7.989570 | 17.21301 |
| 52 | 3.732511 | 8.041452 | 17.32478 |
| 53 | 3.756286 | 8.092672 | 17.43513 |
| 54 | 3.779763 | 8.143253 | 17.54411 |
| 55 | 3.802952 | 8.193213 | 17.65174 |
| 56 | 3.825862 | 8.242571 | 17.75808 |
| 57 | 3.848501 | 8.291344 | 17.86316 |
| 58 | 3.870877 | 8.339551 | 17.96702 |
| 59 | 3.892996 | 8.387207 | 18.06969 |
| 60 | 3.914868 | 8.434327 | 18.17121 |
| 61 | 3.936497 | 8.480926 | 18.27160 |
| 62 | 3.957892 | 8.527019 | 18.37091 |
| 63 | 3.979057 | 8.572619 | 18.46915 |
| 64 | 4.000000 | 8.617739 | 18.56636 |
| 65 | 4.020726 | 8.662391 | 18.66256 |
| 66 | 4.041240 | 8. 706588 | 18.75777 |
| 67 | 4.061548 | 8.750340 | 18.85204 |
| 68 | 4.081655 | 8.793659 | 18,94536 |
| 69 | 4.101566 | 8.836556 | 19.03778 |
| 70 | 4,121285 | 8.879040 | 19.12931 |
| 71 | 4.140818 | 8.921121 | 19.21997 |
| 72 | 4.160168 | 8.952809 | 19.30979 |
| 73 | 4.179339 | 9.004113 | 19.39877 |
| 74 | 4,198336 | 9.045042 | 19.48695 |
| 75 | 4.217163 | 9.085603 | 19.57434 |
| 76 | 4.235824 | 9.125805 | 19.66095 |
| 77 | 4.254321 | 9.165856 | 19.74681 |
| 78 | 4.272659 | 9.205164 | 19.83192 |
| 79 | 4.290840 | 9.244335 | 18.91632 |
| 80 | 4,308869 | 9.283178 | 20.00000 |
| 81 | 4.326749 | 9.321698 | 20.08299 |
| 82 | 4.344481 | 9.359902 | 20.16530 |
| 83 | 4.362071 | 9.397796 | 20.24694 |
| 84 | 4.379519 | 9.435388 | 20.32793 |
| 85 | 4.396830 | 9.472682 | 20.40828 |
| 86 | 4.414005 | 9.509685 | 20.48800 |
| 87 | 4.431048 | 9.546403 | 20.56710 |
| 88 | 4.447960 | 9.582840 | 20.64560 |
| 89 | 4.464745 | 9.619002 | 20.72351 |
| 90 | 4.481405 | 9.654894 | 20.80084 |
| 91 | 4.497941 | 9.690521 | 20.87759 |
| 92 | 4.514357 | 9.725888 | 20.95379 |
| 93 | 4.530655 | 9.761000 | 21.02944 |
| 94 | 4.546836 | 9.795861 | 21.10454 |
| 95 | 4.562903 | 9.830476 | 21.17912 |
| 96 | 4.578857 | 9.864848 | 21.25317 |
| 97 | 4.594701 | 9.898983 | 21.32671 |
| 98 | 4.610436 | 9.932884 | 21.39975 |
| 99 | 4.626065 | 9.966555 | 21.47229 |
| 100 | 4.641589 | 10.00000 | 21.54435 |


| $n$ | $n^{*}$ | $n^{3}$ | $n^{4}$ | $n^{*}$ | $n^{1}$ | $n$ | $n^{4}$ | $n^{3}$ | $n^{4}$ | $n$ ' | $n^{\prime}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 |  |  |  |  |  |  |  | $\times 10^{7}$ | $\times 10^{11}$ | $\times 10^{13}$ |
| 1 |  |  |  |  | 256 | 50 | 6250000 | 312500000 | 15.625000 | 7.812500 | 3.906250 |
| 2 | 16 | 32 | 64 | 128 | 256 | 51 | 6765201 | 345025251 | 17.598288 | 8.974107 | 4.576794 |
| 3 | 81 | 243 | 729 | 2187 | ${ }_{6561} 653$ | 52 | 7311616 | 380204032 | 19.770610 | 10.280717 | 5.345973 |
| 4 | 250 | 1024 | 4096 | 16384 | 655316 | 53 | 7890481 | 418195493 | 22.164361 | 11.747111 | 6.225969 |
| 5 | 625 | 3125 | 15625 | 78125 | 390025 | 54 | 8503056 | 459165024 | 24.794911 | 13.389252 | 7.230196 |
| 8 | 1208 | 7776 | 48656 | 279936 | 1678818 | 55 | 9150525 | 503284375 | 27.680641 | 15.224352 | 8.373394 |
| 7 | 2401 | 16807 | 117649 | 023543 2097152 | 5784801 1677216 | 56 | 8834496 | 550731776 | 30.840979 | 17.270948 | 9.671731 |
| 8 | 4098 | 32788 | 262144 | 2097152 4782969 | 16577216 43046721 | 57 | 10558001 | 601692057 | 34.296447 | 19.548975 | 11.142916 |
| $\theta$ | 6561 | 59049 | 531441 | 4782969 | 43046721 | 5859 | $\begin{aligned} & 11316496 \\ & 12117361 \end{aligned}$ | $\begin{aligned} & 656356768 \\ & 714924299 \end{aligned}$ | $\begin{aligned} & 38.068693 \\ & 42.180534 \end{aligned}$ | $\begin{aligned} & 22.079842 \\ & 24.885515 \end{aligned}$ | $\begin{aligned} & 12.806308 \\ & 14.683044 \end{aligned}$ |
|  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  | $\times 10^{4}$ |  |  |  |  |  |  |
| 10 | 10000 | 100000 | 1000000 | 10000000 | 1.000000 |  |  | $\times 10^{4}$ | $\times 10^{10}$ | $\times 10^{11}$ | $\times 10^{13}$ |
| 11 | 14641 | 161051 | 1771561 | 19487171 |  | 60 | 12960000 | 7.776000 | 4.865600 | 27.993600 | 16.786160 |
| 12 | 20736 | 248832 | 2985984 | 35831808 | 4.299817 | 61 | 13845841 | 8.445963 | 5.152037 | 31.427428 | 19.170731 |
| 13 | 28581 | 371293 | 4826809 | 62748517 | 8.157307 | 62 | 14776336 | 9.161328 | 5.680024 | 35.216146 | 21.834011 |
| 14 | 36416 | 537824 | 7529536 | $\begin{aligned} & 105413504 \\ & 170859375 \end{aligned}$ | $\begin{aligned} & 14.757891 \\ & 25.628905 \end{aligned}$ | 6364 | $\begin{array}{r} 15750000 \\ 18757918 \end{array}$ | 9.924365 | 6.252350 | 39.389806 | 24.815578 |
| 15 | 50625 | 759375 | 11390625 |  |  |  |  | $\begin{array}{r} 10.737418 \\ 11.602906 \end{array}$ | 6.871948 |  | 28.147498 |
| 18 | $\begin{aligned} & 65536 \\ & 83521 \end{aligned}$ | 1048576 | 16777216 | $\begin{aligned} & 170859375 \\ & 268135456 \end{aligned}$ | $\begin{aligned} & 25.628906 \\ & 42.949673 \end{aligned}$ | $\begin{aligned} & 64 \\ & 64 \\ & 65 \end{aligned}$ | $\begin{aligned} & 16777216 \\ & 17850625 \end{aligned}$ |  | $7.541889$ | $49.022279$ | $31.864481$ |
| 17 |  | $\begin{aligned} & 1888568 \\ & 2476059 \end{aligned}$ | 24137569 | $\begin{aligned} & 268135456 \\ & 410338673 \end{aligned}$ | $\begin{aligned} & 42.949673 \\ & 69.757574 \end{aligned}$ | $65$ | $\begin{array}{r} 17850655 \\ 18974736 \end{array}$ | $\begin{aligned} & 11.602906 \\ & 12,523326 \end{aligned}$ |  | 54.551607 | $36.00406 才$40.606768 |
| 18 | 104976 130321 |  | 3401222447045881 | $\begin{aligned} & 612270032 \\ & \mathbf{8 9 3 8 7 1 7 3 9} \end{aligned}$ | $\begin{aligned} & 110.199606 \\ & 169.835530 \end{aligned}$ | $\begin{aligned} & 66 \\ & 67 \end{aligned}$ | $\begin{aligned} & 18974736 \\ & 20151121 \end{aligned}$ | $\begin{aligned} & 12.523326 \\ & 13.501251 \end{aligned}$ | 0.045838 | 80.607116 |  |
| 19 |  |  |  |  |  | 68 | 21381376 | 14.539336 | 9.886748 | 67.229826 | 45.716324 |
|  |  |  |  |  |  | 69 | 22667121 | 15.640313 | 10.791816 | 74.463533 | 51.379837 |
|  | 160000 | 3200000 |  | $\times 10$ | $\times 10^{18}$ |  |  |  |  |  |  |
| 20 |  |  | 84000000 | 1.280300 | 2.560000 |  |  | $\times 10^{4}$ | $\times 10^{10}$ | $\times 10^{12}$ | $\times 10^{14}$ |
| 21 | 194481 | 4084101 | 85766121 | 1.801009 | 3.782288 | 70 | 240100300 | 16.807000 | 11.764000 | 8.235430 | 5.764801 |
| 82 | 234256 | 5153612 | 113378904 | 2.494358 | 5.487587 | 71 | 25411681 | 18.042294 | 12.810028 | 9.095120 | 8.457535 |
| 23 | 278341 | 6436343 | 148035889 | 3.404825 | 7.831099 | 72 | 26973856 | 18.349176 | 13.931407 | 10.030513 | 7.222041 |
| 24 | 331778 | 7082624 | 191402976 | 4.588471 | 11.00751 | 73 | 28388241 | 20.730718 | 15.133423 | 11.047398 | 8.084601 |
| 25 | 390825 | 9765625 | 244140825 | 6.103316 | 15.258789 | 74 | 29986576 | 22.120066 | 16.420649 | 12,151280 | 8.991947 |
| 26 | 456978 | 11831376 | 308915776 | 8.031810 | 20.882706 | 75 | 31640625 | 23.730469 | 17.797852 | 13,348388 | 10.011292 |
| 27 | 531441 | 14348907 | 387420489 | 10.460353 | 28.242954 | 76 | 33362176 | 25.355254 | 19.269993 | 14,645985 | 11.130348 |
| 28 | 614858 | 17210388 | 481890304 | 13.492929 | 37.780200 | 37 | 35153041 | 27.057842 | 20.842838 | 16.048523 | 12,357383 |
| 20 | 707281 | 20511148 | 594823321 | 17.249876 | 50.024641 | 7879 | 3701505638950081 | $\begin{aligned} & 28.871744 \\ & 30.770584 \end{aligned}$ | $\begin{aligned} & 22.519960 \\ & 24.309746 \end{aligned}$ | $\begin{aligned} & 17.585589 \\ & 19.203909 \end{aligned}$ | $13.701144$ |
|  |  |  |  |  |  |  |  |  |  |  | 15.171088 |
|  |  |  | $\times 100$ | $\times 1014$ | $\times 10^{14}$ |  |  | $\times 104$ | $\times 10^{19}$ |  | $\times 10^{14}$ |
| 30 | 810000 | 24300000 | 7.200000 |  | 6.561000 |  |  | 32.768000 | $\times 26.214400$ | $\underset{\sim}{\times 1012}$ | ${ }_{16.777218}$ |
| 31 | 923521 | 28529151 | 8.873037 | 2.751261 | $\begin{array}{r} 8.528910 \\ 10.995116 \end{array}$ | 88 | 43046721 | 32.768000 34.86784 | $\begin{aligned} & 26.214400 \\ & 28.242954 \end{aligned}$ | $\begin{aligned} & 20.971520 \\ & 22.876792 \end{aligned}$ |  |
| 32 | $\begin{aligned} & 1048575 \\ & 1185921 \end{aligned}$ | 33554432 | $\begin{aligned} & 10.737418 \\ & 12.914880 \end{aligned}$ | $\begin{aligned} & 3.435974 \\ & 4.261844 \end{aligned}$ | $\begin{aligned} & 10.995116 \\ & 14.054085 \end{aligned}$ | 82 | 45212176 | 37.073984 | 30.400087 | 24,928547 | $20.441409$ |
| 33 |  | 39135393 |  |  |  | 83 | 47458321 | 38.390406 | 32.694037 | 27.136051 | 22,522922 |
| 34 | 1336336 | 45435424 | 15,448044 | \$.252335 | 17.857939 | 84 | 49787136 | 41.821194 | 35.128803 | 29,309035 | 24,787389 |
| 35 | 1500625 | 52521875 | 18.382556 | 6.433930 | 22.518754 | 85 | 52200625 | 44.370531 | 37.714952 | 32,087709 | 27.249053 |
| 38 | 1679616 | 60466176 | 21.787823 | 7.836416 | 28.211099 | 86 | 54700816 | 47.042702 | 40.456724 | 34,792782 | 29.921783 |
| 37 | 1874161 | 69343957 | 25.557264 | 9.493188 | 35.124795 | 87 | 57289761 | 49.842092 | 43.362620 | 37,725478 | 38.821167 |
| 38 | 2095136 | 79235168 | 30.109384 | \$1.441558 | 43.477921 | 87 | \$9769536 | 59.8473192 $\mathbf{5 2 . 7 7 3 2}$ | 46.440409 | 40,867580 | 35.863452 |
| 39 | 2313441 | 90224198 | 35.197438 | 13.723101 | 53.520093 | 89 | \$2742241 | 55.84059 ${ }^{\text {d }}$ | 49.698129 | 44.231335 | 39.3658888 |
|  |  |  | $\times 10^{7}$ | $\times 10^{14}$ | $\times 10^{13}$ |  |  | $\times 108$ | $\times 1011$ | $\times 10^{19}$ | $\times 1015$ |
| 40 | 2560000 | 102400000 | 4.006000 | 18.384000 | 6.553600 | 90 | 85610000 | 5.904900 | 5.314410 | 4,789969 | 4.304672 |
| 41 | 2825761 | 115856201 | 4.750104 | 19.475427 | 7.984925 | 91 | 88574961 | 6.240321 | 5.678693 | 5.167610 | 4.702525 |
| 42 | 3111696 | 130691232 | 5.489032 | 23.053933 | 9.682652 | 92 | 71639296 | 6.590815 | 6.0033550 | 5.578466 | 5.132189 |
| 43 | 3418801 | 147008443 | 6.321363 | 27.181861 | 11.688200 | 93 | 74805201 | 6.956884 | 0.469902 | 6.017009 | 5.595818 |
| 44 | 3748096 | 164916224 | 7.256314 | 31.927781 | 14.048224 | 94 | 78074896 | 7.339040 | 6.898698 | 6.484776 | 6.095689 |
| 45 | 4100825 | 184528125 | 8.303766 | 37.306945 | 16.815125 | 95 | 81450625 | 7.737809 | 7.350919 | 6.983373 | 6.634204 |
| 48 | 4477456 | 205962976 | 9.474287 | 43.581766 | 20.047612 | 96 | 81934656 | 8.153727 | 7.827578 | 7.514475 | 7.213896 |
| 47 | 4879681 | 229345007 | 10.779215 | 50.662312 | 23.811287 | 97 | 88529281 | 6.587340 | 8.320720 | 8.079828 | 7.837434 |
| 48 | 5308416 | 254803868 | 12,230590 | 58.706834 | 29.179280 | 98 | 92236816 | 9.039208 | 8.858424 | 8.681255 | 8.507630 |
| 49 | 5764801 | 282475249 | 13.841287 | 67.8223107 | 33.232931 | 99 | 96059801 | 9.509900 | 9.414801 | 9.320653 | 9.227447 |
| 50 | 6250000 | 312500000 | 15,625000 | 79.125000 | 39.062500 | 100 | 100000000 | 10.000000 | 10.000000 | 10.000000 | 10,000000 |
|  |  |  |  |  |  |  |  |  |  |  |  |

- Radix (base) point
- Logic multiplication symbol
$\infty \quad$ Intinity
$+\quad$ Plus, positive, logic OR function
- Minus, negative
$\pm \quad$ Plus or minus, positive or negative
$\mp \quad$ Minus or plus, negative or positive
$\times$ Times, logic AND function
$\div \quad$ Divided by
/ Divided by (expressive of a ratio)
$=$ Equal to
$\equiv$ Identical to, is defined by
$\cong$ Approximately equal to, congruent to
$\doteq$ Approximately equal to
$\neq$ Not equal to
~ Similar to
$<\quad$ Less than
$\$ \quad$ Not less than
$\ll \quad$ Much less than
$>\quad$ Greater than
> Not greater than
>> Much greater than
$\leqslant \quad$ Equal to or less than
$\geqslant$ Equal to or greater than
$\propto \quad$ Proportional to, varies directiy as
$\rightarrow \quad$ Approaches
: Is to, proportional to
. Therefore
\# Number
\% Percent
@ At the rate of; at cost of
$\epsilon$ or $e \quad$ The natural number $=2.71828$ ~
$\pi \quad \mathrm{Pi} \cong 3.14159 \ldots$
() Parentheses. Used to enclose a common group of terms.
[] Brackets. Used to enclose a common group of terms which includes one or more groups in parentheses.
\{ \} Braces. Used to enclose a common group of terms which includes one of more groups in brackets.
$\angle$ Angle
$\therefore$ Degrees (arc or temperature)
, Minutes, prime
" Seconds, double prime
1 Parallel to
$\perp$ Perpendicular to
... And beyond, ellipsis

| $y+y$ | $x$ added to $y, x$ OR $y$ |
| :---: | :---: |
| $\boldsymbol{x}-\mathbf{y}$ | $y$ subtracted from $x$ |
|  | $x$ multiplied by $y, x$ AND $y$ |
| $I-1$ | $x$ divided by $y$ |
| $x / y$ or $\frac{1}{y}$ | $x$ divided by $y$ |
| $1 / x$ | Feciprocal of $x$ |
| $\sqrt{1}$ | $x$ raised to the indicated power of $n$ |
| $\sqrt[n]{x}$ | Indicated root ( $\sqrt{ }$ ) of $x$ |
| I: ${ }^{\text {I }}$ | $x$ is to $y$ |
|  | Absolute value of $x$, magnitude of $x$ |
| $\underline{X}, x$, or $X$ | Vector $X$ |
| $\bar{x}$ | Average value of $x$ |
| $f(x)$ or $F(x)$ | Function of $x$ |
| 1 | $\sqrt{-1}$ |
| j | Operator, equal to $\sqrt{-1}$ |
| $\Delta x$ | increment of $x$ |
| dx | Differential of $x$ |
| 3 x | Partial differential of $\boldsymbol{x}$ |
| $\Delta{ }_{\text {dr }}$ | Change in $x$ with respect to $y$ |
| $\Delta{ }^{\prime}$ |  |
| $\frac{d x}{d y}$ | Derivative of $x$ with respect to $y$ |
| $\frac{d}{d y}\|x\|$ | Derivative of $x$ with respect to $y$ |
| $\mathrm{Dr}^{1}$ | Derivative of $x$ with respect to $y$ |
| $\frac{\partial I}{3 y}$ | Partial derivative of $x$ with respect to $y$ |
| 区 | Summation |
| $\Sigma_{0}^{0}$ | Summation between limits (from $a$ to $b$ ) |
| $\square$ | Product |
| $\stackrel{+}{\square}$ | Product between limits (from $a$ to $b$ ) |
| § | Integral |
| $\int_{0}$ | Integral between limits (from $a$ tob) |
| $\int x d y$ | Integral of $x$ with respect to $y$ |
| $l$ | Evaluated at $a$ |
| 10 | Evaluated beween limits (from $a$ to $b$ ) |

factorials

## Numerical

| $n$ | $\frac{1}{n!}$ |  |  |  |  |  |  | $n!$ |  | $n$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1. |  |  |  |  |  |  |  | 1 | 1 |
| 3 | . 16866 | 66666 | 66666 | 66666 | 66667 |  |  |  | 6 | 3 |
| 4 | . 04166 | 66666 | 66666 | 66666 | 66667 |  |  |  | 24 | 4 |
| 5 | . 00833 | 33333 | 33333 | 33333 | 33333 |  |  |  | 120 | 5 |
| 6 | 0.00138 | 88888 | 88888 | 98888 | 88889 |  |  |  | 720 | 6 |
| 7 | . 00019 | 84126 | 98412 | $6984{ }^{1}$ | 26984 |  |  |  | 5040 | 7 |
| 8 | . 00002 | 48015 | 87301 | 58730 | 15873 |  |  |  | 40320 | 8 |
| 9 | . 00000 | 27557 | 31922 | 39858 | 90653 |  |  | 3 | 62880 | 9 |
| 10 | .00000 | 02755 | 73192 | 23985 | 89055 |  |  | 36 | 28800 | 10 |
| 11 | 0.00000 | 00250 | 52108 | 38544 | 17188 |  |  | 399 | 18800 | 11 |
| 12 | . 00000 | 00020 | 87675 | 68878 | 68099 |  |  | 4790 | 01600 | 12 |
| 13 | . 00000 | 00001 | 60590 | 43836 | 82161 |  |  | 62270 | 20800 | 13 |
| 14 | . 00000 | 00000 | 11470 | 74559 | 77297 |  | 8 | 71782 | 91200 | 14 |
| 15 | . 00000 | 00000 | 00764 | 71637 | 31820 |  | 130 | 76743 | 68000 | 15 |
| 16 | 0,00000 | 00000 | 00047 | 79477 | 33239 |  | 2092 | 27898 | 88000 | 16 |
| 17 | . 00000 | 00000 | 00002 | 81145 | 72543 |  | 35568 | 74280 | 96000 | 17 |
| 18 | . 00000 | 00000 | 00000 | 15619 | 20697 | 6 | 40237 | 37057 | 28000 | 18 |
| 19 | . 00000 | 00000 | 00000 | 00822 | 06352 | 121 | 64510 | 04088 | 32000 | 19 |
| 20 | . 00000 | 00000 | 00000 | 00041 | 10318 | 2432 | 90200 | 81766 | 40000 | 20 |
| $n t=1 \times 2 \times 3 \times 4 \times 5 \ldots n$ |  |  |  |  |  |  |  |  |  |  |

FOR EXAMPLE: For $n=7, n!=5040$.
$1 / n!=0.001984126984126984126984$, $\log (n!)=3.702431$.
Logarithmic
Logarithms of the products $1 \times 2 \times 3 \ldots, n$ from 1 to 100 .

| $\underline{\square}$ | log (n) | $n$ | $\log (\mathrm{nl})$ | n | $\log (n)$ | $n$ | $\log$ (n) 1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0.000000 | 26 | 26.605619 | 51 | 66.190645 | 76 | 111.275425 |
| 2 | 0.301030 | 27 | 28.036983 | 52 | 67.905648 | 77 | 113.161916 |
| 3 | 0.778961 | 28 | 29.484141 | 53 | 69.630924 | 78 | 115054011 |
| 4 | 1.380211 | 29 | 30.946539 | 54 | 71.363318 | 79 | 116.951638 |
| 5 | 2,079181 | 30 | 32.423660 | 55 | 73,10368: | 80 | 118.854728 |
| 6 | 2.857332 | 31 | 33.915022 | 56 | 74.851869 | 81 | 120.763213 |
| 7 | 3.702431 | 32 | 35.470172 | 57 | 76.607744 | 82 | 122.677027 |
| 8 | 4.605521 | 33 | 36.938686 | 58 | 78.371172 | 83 | 124.596105 |
| 9 | 5.559763 | 34 | 38.470165 | 59 | 80.142024 | 84 | 126.520384 |
| 10 | 6.559763 | 35 | 40.014233 | 60 | 81.920175 | 85 | 128.449803 |
| 11 | 7.601156 | 36 | 41.570535 | 61 | 83.705505 | 86 | 130.384301 |
| 12 | 8.680337 | 37 | 43.138737 | 62 | 85.497896 | 87 | 132.323821 |
| 13 | 9.794280 | 38 | 44.718520 | 63 | 87.297237 | 88 | 134.268303 |
| 14 | 10.940408 | 39 | 46.309585 | 64 | 89.103417 | 89 | 136.217693 |
| 15 | 12.116500 | 40 | 47.911645 | 65 | 90.916330 | 90 | 138.171936 |
| 16 | 13.320820 | 41 | 49.524429 | 66 | 92.735874 | 91 | 140.130977 |
| 17 | 14.551069 | 42 | 51.147678 | 67 | 94.561949 | 92 | 142.094765 |
| 18 | 15.806341 | 43 | 52.781147 | 68 | 96.394458 | 93 | 144.063248 |
| 19 | 17.085095 | 44 | 54.424599 | 69 | 98,233307 | 94 | 146.036376 |
| 20 | 18.386125 | 45 | 56.077812 | 70 | 100.078405 | 95 | 148.014099 |
| 21 | 19.708344 | 46 | 57.740570 | 71 | 101.929663 | 96 | 149.996371 |
| 22 | 21.050767 | 47 | 59.412688 | 72 | 103.786996 | 97 | 151.983142 |
| 23 | 22.412494 | 48 | 61.093909 | 73 | 105.650319 | 98 | 153.974368 |
| 24 | 23.792706 | 49 | 62.789 105 | 74 | 107.519550 | 99 | 155.970004 |
| 25 | 25.190646 | 50 | 64.483075 | 75 | 109.394612 | 100 | 15797000 |

## RECTANGULAR-POLAR CONVERSION CHART

This chart quickly converts belween cartesian (rectangular) and polar forms of notation. The horizontal (real) and the vertical (imaginary) coordinates are used for rectangular notations, and the angular (magnitude) and circular (angle) coordinates are used for polar notation. The same units of measurement are used for both systems. This makes conversion from one system to the other readily possible. The range of the chart can be extended by multiplying the horizontal and vertical axes by the same power of ten.

FOR EXAMPLE:

1. $2+\beta$ is equivalent to $3.6 / 56^{\circ}$
2. $70 / 55^{\circ}$ is equivalent to $40+j 57$
3. $6-\beta$ is equivalent to $6.7 / 333^{\circ}$


$X^{2}+Y^{2}=a^{2}$
$X=a \cos \mu . Y=a \sin \mu$

$r=2 a \cos \mu$

$\mathrm{r}=\mathrm{a} \cos \mu \mathrm{b} \mathrm{b} \sin \mu$

$r=2 a \sin \mu$

$$
\begin{aligned}
& \frac{X^{2}}{a^{2}}+\frac{Y^{2}}{b^{2}}=1 \quad r=a+b \cos \mu \quad r=a(1+\cos \mu) \\
& X=a \operatorname{a} \cos \mu, Y=b \sin \mu
\end{aligned}
$$


$r^{2}=a^{2} \cos 2 \mu$

$X Y=a^{2}$

$\frac{X^{2}}{a^{2}}-\frac{Y^{2}}{b^{2}}=1$

$a^{2} Y=X^{3}$

$a Y^{2}=X^{3}, a>0$

$\frac{Y^{2}}{b^{2}}=\frac{X}{a}$

$X^{w_{2}}+Y^{w_{2}}=a^{1_{2}}$


$r=a \cos 3 \mu$


$r=a \cos 2 \mu$

$r=a \sin 2 \mu$

$Y^{2}(2 a-X)=X^{3}$

$y^{2}=X^{2} \frac{a+X}{a-X}$

$Y=a^{x}$

$Y=\log _{\mathrm{a}} X$


$$
Y=e^{-x^{2}}
$$


$X=a(\mu-\sin \mu)$
$\mathrm{Y}=\mathrm{a}(1-\cos \mu)$

$X^{3}+Y^{n}=a^{n} \quad Y=a\left(\cos H \frac{X}{a}-1\right)$

$$
\begin{aligned}
& X= \\
& \pm\left(a \operatorname{sech}^{-1} \frac{Y}{a} \sqrt{a^{2}-Y^{2}}\right)
\end{aligned}
$$

Cube


Surface Area
$A=6 s^{4}$
Volume
$y=s^{1}$

## Disgonal

$\mathrm{D}=1.7321 \mathrm{~s}$

## Parallelopiped



$$
A=2(a b+b c+x c)
$$

Volume
$\mathrm{V}=\mathrm{abc}$
Diagonal
$D=\sqrt{a^{2}+b^{\frac{1}{2}}+c^{2}}$

Right Circular Cyiinder


Surface Area

$$
A=1.5708 \mathrm{~d}(2 \mathrm{~h}+\mathrm{d})
$$

Volume
$Y=.7854 d^{2} h$

Right Rexular Pyramid


Surfice Acea
$A={ }^{3}, n b l+A$ (ares of base)

Volume
$V=15 A \mu h$


Surlace Area
$A=1.5708 d(.5 d+1)$

## Volume

$V=.26 J \mathrm{Bd} \mathrm{H}_{\mathrm{h}}$

Frustrum of Right Regular Pyramid


## Surface Area

$A=1 / 2\left[n\left(b+b_{1}\right)+A B+A T \mid\right.$

Volume
$V=I / S h(A B+A T+\sqrt{A B A T})$

Frustrum of Right Círcular Cylinder


Frustrum of Right Regular Cone


## Suribce Area

$A=.3927\left(d^{1}+d^{2}+41\left(d+d_{1}\right)\right.$

## $V$ olume

$V=.2618 h\left(d^{2}+\left(d d_{1}+d_{1}{ }^{2}\right)\right.$



| Known | F)nd |  |
| :---: | :---: | :---: |
| b, | $A_{,} \mathbf{B}, \mathrm{b}$ | $\operatorname{tin} A=\frac{a}{c}$, tos $B=\frac{a}{c}, b=\sqrt{c^{3}-a^{2}}$ |
|  | Ares | $\frac{1}{2} \sqrt{c^{3}-4^{4}}$ |
| b, b | A, 3, | $\tan \lambda=\frac{b}{b}, \tan B=\frac{b}{a}, t=\sqrt{a^{2}+b^{2}}$ |
|  | Areo | $\frac{a b}{2}$ |
| $A, 0$ | 1, b, s | $s=90^{\circ}-A, b=a \cot A, c=\frac{0}{\sin \lambda}$ |
|  | Alen | $\frac{a^{3} \cot \lambda}{2}$ |
| A, b | 3, 0,5 | $t=90^{*}-\lambda, a=b \tan A, c=\frac{b}{\cos A}$ |
|  | Aroo | $\frac{b^{2} \tan A}{2}$ |
| A, 6 | B,, , b | $\theta=90^{\circ}-A, a=s \sin A, b=c \cos A$ |
|  | Arro | $\frac{c^{2} \sin A \cos A}{2}=\frac{c^{2} \sin 2 A}{4}$ |
| Known | Find |  |
|  | A | $\begin{aligned} & \sin \frac{1}{2} A=\sqrt{\frac{[b-b](1-c)}{b c}}, \cos \frac{i}{2} A= \\ & \sqrt{\frac{(\{(1-a)}{. b c}}, \tan \frac{1}{2} A=\sqrt{\frac{(b-b)(1-c)}{b\{(5-a\}}} \end{aligned}$ |
|  | - | $\begin{aligned} & \operatorname{tin} \frac{1}{2}=\sqrt{\frac{(v-a)(b-c)}{a c}}, \cos \frac{1}{2}= \\ & \sqrt{\frac{1(b-b)}{a c}}, \tan \frac{1}{2}=\sqrt{\frac{(1-a)((b-c)}{1(b-b)}} \end{aligned}$ |
|  | $C$ |  |
|  | Aroso | $\sqrt{\text { (1a-a) (2-b) (b-c) }}$ |
| A, A, $\mathbf{B}_{4}$ | b.e | $b=\frac{a \sin B}{\sin A}, c=\frac{a \sin C}{\sin A}=\frac{a \sin (A+B)}{\sin A}$ |
|  | C | $C=160^{\circ}-(A+B$ |
|  | Arad | $\frac{1}{2} a b \sin C=\frac{a^{2} \sin B a \ln C}{2 \sin A}$ |
| c, b, A | - | $\min t=\frac{b \sin A}{0}$ |
|  | $C$ | $C=18 Q^{\circ}-(A+3)$ |
|  | c | $c=\frac{a \sin C}{\sin A}=\frac{b \sin C}{\sin b}=\sqrt{a^{2}+b^{2}-2 a b \cos C}$ |
|  | Arat | $\frac{1}{2} a b \sin c=\frac{1}{2} a \cos A=\frac{1}{2} b \operatorname{cin} A$ |
| $\bullet, t, c$ | $\cdots$ | $\tan A=\frac{0 \sin c}{b-\cos \varepsilon}$ |
|  | 1 |  |
|  | $c$ | $c=\frac{\sin t}{\sin A}=\sqrt{a^{2}+b^{2}-2 a b \cos C}$ |
|  | Area | $\frac{1}{2}=b \operatorname{lin} c$ |
| $\begin{gathered} a^{3}=b^{2}+c^{3}-2 b c \cos A, b^{2}=a^{2}+c^{2}-2 a \cos A . \\ c^{2}=a^{2}+b^{2}-2 a b \cos C \\ \frac{a}{\sin A}=\frac{b}{\sin B}=\frac{c}{\sin C} \end{gathered}$ |  |  |


| Angle deg. | Arc | 5 in | Cos | Ton | Cot | Suc | Cse | Choed. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 0 | 0 | +1 | 0 | - | +1 | $\infty$ | 0 |
| 30 | 1/6 $\pi$ | 1/2 | $1 / 2 \sqrt{3}$ | $1 / 3 \sqrt{3}$ | $\sqrt{3}$ | $2 / 3 \sqrt{3}$ | 2 | $\sqrt{2-\sqrt{3}}$ |
| 45 | 1/4 $\pi$ | $1 / 2 \sqrt{2}$ | $1 / 2 \sqrt{2}$ | +1 | $+1$ | $\sqrt{2}$ | $\sqrt{2}$ | $\sqrt{2-\sqrt{2}}$ |
| 60 | 1/3 $\pi$ | $1 / 2 \sqrt{3}$ | 1/2 | $\sqrt{3}$ | $1 / 3 \sqrt{3}$ | 2 | $2 / 3 \sqrt{3}$ | 1 |
| 90 | $1 / 2 \pi$ | $+1$ | 0 | m | 0 | $\infty$ | +1 | $\sqrt{2}$ |
| 120 | 1/3 \% | $1 / 2 \sqrt{3}$ | -1/2 | $-\sqrt{3}$ | $-1 / 3 \sqrt{3}$ | -2 | $2 / 3 \sqrt{3}$ | $\sqrt{3}$ |
| 135 | 3/4 F | $1 / 2 \sqrt{2}$ | -1/2 $\sqrt{2}$ | -1 | -1 | $-\sqrt{2}$ | $\sqrt{2}$ | $\sqrt{2+\sqrt{2}}$ |
| 150 | 5/6 $\quad$ \% | 1/2 | $-1 / 2 \sqrt{3}$ | -1/3 $\sqrt{3}$ | $-\sqrt{3}$ | $-2 / 3 \sqrt{3}$ | 2 | $\sqrt{2+\sqrt{3}}$ |
| 180 | $\pi$ | 0 | -1 | 0 | $\infty$ | -1 | - | 2 |
| 210 | 7/6 \# | -1/2 | $\pm 1 / 2 \sqrt{3}$ | $1 / 3 \sqrt{3}$ | $\sqrt{3}$ | $-2 / 3 \sqrt{3}$ | -2 | $\sqrt{2+\sqrt{3}}$ |
| 225 | 5/4 7 | $-1 / 2 \sqrt{2}$ | $-1 / 2 \sqrt{2}$ | +1 | +1 | $-\sqrt{2}$ | $-\sqrt{2}$ | $\sqrt{2+\sqrt{2}}$ |
| 240 | 4/3 $\pi$ | $-1 / 2 \sqrt{3}$ | -1/2 | $\sqrt{3}$ | $1 / 3 \sqrt{3}$ | -2 | -2/3 $\sqrt{3}$ | $\sqrt{3}$ |
| 270 | 3/2 $\%$ | -1 | 0 | $\infty$ | 0 | $\infty$ | -1 | $\sqrt{2}$ |
| 300 | 5/3 $\quad$ \% | $-1 / 2 \sqrt{3}$ | 1/2 | $-\sqrt{3}$ | $-1 / 3 \sqrt{3}$ | 2 | $-2 / 3 \sqrt{3}$ | 1 |
| 315 | 7/4 $\quad$ \% | $-1 / 2 \sqrt{2}$ | 1/2 $\sqrt{2}$ | -1 | -1 | $\sqrt{2}$ | $-\sqrt{2}$ | $\sqrt{2-\sqrt{2}}$ |
| 330 | 11/6 \% | $-1 / 2$ | $1 / 2 \sqrt{3}$ | $-1 / 3 \sqrt{3}$ | $-\sqrt{3}$ | $2 / 3 \sqrt{3}$ | -2 | $\sqrt{2-\sqrt{2}}$ |
| 360 | $2 \pi$ | 0 | +1 | 0 | + | +1 | - | 0 |




Fundampatal Trigonometric Funetions

$$
\begin{array}{ll}
\sin A=\frac{a}{c}, & \csc A=\frac{c}{a} \\
\cos A=\frac{b}{c} & \sec A=\frac{c}{b} \\
\sin A=\frac{B}{b} & \cot A=\frac{b}{a}
\end{array}
$$

Functions of one angle

$$
\begin{aligned}
& \sin ^{2} A+\cos ^{\prime} A=1 \\
& \sec ^{2} A-\cos ^{2} A=1
\end{aligned}
$$

$$
\sec ^{2} \mathrm{~A}-\cot ^{2} \mathrm{~A}=1
$$

Functions of the sum of two angles
$\sin (A+B)=\sin A \cos B+\cos A \sin B$
$\cos (A+B)=\cos A \cos B-\sin A \sin B$
$\tan (A+B)=\frac{\tan A+\tan B}{1-\tan A \tan B}$
$\cot (A+B)=\frac{\cot A \cot B-1}{\cot B+\cot A}$

Functions of the difference of two anyles

$$
\begin{aligned}
& \sin (A-B)=\sin A \cos B-\operatorname{con} A \sin B \\
& \cos (A-B)=\cos A \cos B+\sin A \sin B \\
& \tan (A-B)=\frac{\tan A-\tan B}{1+\tan A \tan B} \\
& \cot (A-B)=\frac{\cot A \cot B+1}{\cot B-\cot A}
\end{aligned}
$$

Functions of ope-half an angle

$$
\begin{aligned}
& \sin 1 / 2=\frac{\sin A}{2 \cos 1 / 2 A}= \pm \sqrt{\frac{1-\cos A}{2}} \\
& \cos 1 / 2 A=\frac{\sin A}{2 \sin 1 / 2 A}= \pm \sqrt{\frac{1+\cos A}{2}} \\
& \tan 1 / 2 A=\frac{1-\cos A}{\sin A}= \pm \sqrt{\frac{1-\cos A}{1+\cos A}} \\
& \cot 1 / 2 A= \pm \sqrt{\frac{1-\cos A}{1+\cos A}}
\end{aligned}
$$

Functions of twice an angle

$$
\begin{aligned}
& \sin 2 A=2 \sin A \cos A=\frac{2 \operatorname{can} A}{1+\tan A} \\
& \cos 2 A
\end{aligned}=\cos ^{2} A-\sin ^{2} A=1-2 \sin ^{2} A \quad, ~ \begin{aligned}
\tan 2 A & =\frac{2 \cos ^{2} A-1-\frac{1-\tan ^{2} A}{1-\tan ^{2} A}}{1-\tan ^{2} A}=\frac{\sin 8 A-\sin A}{\cos 3 A+\cos A} \\
\cot 2 A & =\frac{\cot A-1}{2 \cot A}
\end{aligned}
$$

Functions of three times an angle
Functions of angles squared
$\sin 3 A=3 \sin A+4 \sin ^{3} A$
$\cos B A=4 \cos ^{2} A-3 \cos A$
$\tan 3 A=\frac{3 \operatorname{lan} A-\tan ^{2} A}{1-3 \tan ^{2} A}$

$$
\begin{aligned}
& \sin ^{2} A=\frac{1-\cos 2 A}{2} \\
& \cos ^{2} A=\frac{1+\cos 2 A}{2} \\
& \tan ^{2} A=\frac{1-\cos 2 A}{1+\cos 2 A} \\
& \cot ^{2} A=\frac{1+\cos 2 A}{1-\cos 2 A}
\end{aligned}
$$

$\operatorname{cots} A=\frac{\cot ^{2} A-3 \cot A}{3 \cot ^{3}-1}$
$\sin ^{2} A-\sin ^{2} B=\sin (A+B) \sin (A-B)$
$\cos ^{2} A-\sin ^{2} B=\cos (A+B) \cos (A-B)$

Functions - Relstionships
$\sin A=\frac{\cos A}{\cot A}=\frac{1}{\csc A}=\cos A \tan A=\sqrt{1-\cos ^{2} A}$
$\cos A=\frac{\sin A}{\tan A}=\frac{1}{\sec A}=\sin A \cot A=\sqrt{1-\sin ^{2} A}$
$\tan A=\frac{\sin A}{\cos A}=\frac{1}{\cot A}=\sin A \sec A$
$\cot A=\frac{\cos A}{\sin A}=\frac{1}{\operatorname{con} A}=\cos A \csc A$
$\sec A=\frac{\tan A}{\sin A}=\frac{1}{\cos A}$
$\csc A=\frac{\cot A}{\sin A}=\frac{1}{\sin A}$
$\sin A+\sin B=2 \sin 1 / 2(A+B) \cos 1 / 2(A-B)$
$\sin A-\sin B=2 \cos 1 / 2 \cdot(A+B) \sin 1 / 2(A-B)$
$\cos A+\cos B=2 \cos 1 / 2(A+B) \cos 1 / 2(A-B)$
$\cos A-\cos B=-2 \sin 1 / 2(A+B) \sin 1 / 2(A-B)$
$\tan A+\tan B=\frac{\sin (A+B)}{\cos A \cos B}$
$\tan A-\tan A=\frac{\sin (A-B)}{\cos A \cos B}$
$\cot A+\cot B=\frac{\sin (A+B)}{\sin A \sin B}$
$\cot A-\cot B=\frac{\sin (B-A)}{\sin A \sin B}$

For two signals having the same frequency, the phase can be determined by measuring the major and minor axes of the ellipse. The phase angle is equal to twice the angle whose tangent is the ratio of the major axis to the minor axis. The absolute accuracy of this method is dependent upon the phase in the horizontal and vertical amplifiers of the oscilloscope being equal and the care that is taken to make the horizontal and vertical amplitudes equal.



## PULSE PARAMETER NOMOGRAM

This normalized nomogram relates pulse rise time, repetition frequency, and pulse width to data channel bandwidth. To use the nomogram, connect a horizontal line through the selected bandwidth. The intersection with the other columns gives maximum pulse repetition frequency, minimum pulse width, and minimum risetime. For a given bandwidth, any combination of factors below the line can be used.

FOR EXAMPLE: For a bandwidth of $10 \mathrm{MHz}\left(10 \times 10^{6} \mathrm{~Hz}\right)$ the fastest risetime is $0.035 \times 10^{-6} \mathrm{sec}$, the maximum pulse repetition frequency is $3.34 \times 10^{6}$ pulses per second, and the minimum pulse width is $0.15 \times 10^{-6} \mathrm{sec}$.


PULSE DEFINITIONS


This scale is based on the formula $f=1 / T$ ．It converts between the frequency（ $f$ ）and the period（ $D$ ）of any recurrent waveform between 1 Hz and $10,00 \mathrm{GHz}$ ．It is useful where a large number of conversions are re－ quired as in the case when an oscilloscope with a time－calibrated sweep is used for frequency mea－ surements．

FOR EXAMPLE：（1）The period of a $40-\mathrm{MHz}$ sig－ nal is 25 nsec ．（2）The frequency of a signal with a period of $12.5 \mu \mathrm{sec}$ is 80 kHz ．

| FREQUENCY | fCR100 |
| :---: | :---: |
| $\mathrm{Hz}^{\longrightarrow}$－mes |  |
| $\mathrm{HH}_{2}$－－－nase |  |
| $\mathrm{MH}_{\mathrm{L}}$－ |  |
| Chis－prec |  |
| $10000=0.1$ |  |
| $8000=$ |  |
| $6000-$ |  |
| 5000 実 0.2 |  |
| 4000 － |  |
| 000青 0.3 |  |
| $300 \sim 0$ |  |
| $0000 \text { 昰 } 0.5$ |  |
| $2000 e^{-E_{E}}-0.5$ |  |
|  |  |
| 1000 $\frac{2}{2-0.6}$ |  |
|  |  |
| $800 \sim$ |  |
| ${ }^{800}$ 二三 |  |
| 000 二上 |  |
| 500 清 |  |
| 400 素 |  |
| \％00 $=3$ |  |
|  |  |
| 200桭 |  |
|  |  |
| － |  |
| 100 E $=10$ |  |
|  |  |
| $80-1$ |  |
|  |  |
| $50-\overline{\text { E }}$ |  |
|  |  |
| 40 老 30 |  |
| $30 \sum_{40}$ |  |
|  |  |
| $20 \frac{\text { 春 }}{5} 50$ |  |
| $E^{-E}$ |  |
| ＝$=80$ |  |
| $10 \frac{1}{7} 100$ |  |
|  |  |
| \％$\frac{7}{-1}$ |  |
| $\bigcirc 5$ |  |
|  |  |
| $3 \text { 羓 } 300$ |  |
|  |  |
| $\text { 奉 } 400$ |  |
| 2 三晨 500 |  |
| E－400 |  |
| $1 \underset{=100}{E=-100}$ |  |
|  |  |


| Letter |  | Name | Letter |  | Name |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Small | Capital |  | Small | Capital |  |
| $\begin{aligned} & \alpha \\ & \beta \\ & \gamma \\ & \gamma \\ & \epsilon \\ & \zeta \\ & \eta \\ & \theta \\ & \iota \\ & \kappa \\ & \lambda \\ & \mu \end{aligned}$ | $\begin{aligned} & \hline \mathrm{A} \\ & \mathrm{~B} \\ & \mathrm{C} \\ & \Delta \\ & \mathrm{E} \\ & \mathrm{Z} \\ & \mathrm{H} \\ & \Theta \\ & \mathrm{I} \\ & \mathrm{~K} \\ & \Lambda \\ & \mathrm{M} \end{aligned}$ | Alpha Beta Gamma Delta Epsilon Zeta Eta Theta lota Kappa Lambda Mu | $\begin{aligned} & \nu \\ & \xi \\ & o \\ & \pi \\ & \rho \\ & \sigma \\ & \tau \\ & \nu \\ & \phi \\ & \chi \\ & \psi \\ & \omega \end{aligned}$ |  | Nu <br> XI <br> Omicron <br> Pi <br> Rho <br> Sigma <br> Tau <br> Upsilon <br> Phi <br> Chi <br> Psi <br> Omega |

## ROMAN NUMERALS

The chief symbols are $I=1 ; V=5 ; X=10 ; L=50 ; \mathrm{C}=100 ; \mathrm{D}=500$; and $\mathrm{M}=1,000$. Note that $I V=4$, means 1 short of $5 ; I X=9$, means 1 short of ten; $X L=40$, means 10 short of 50 ; and $X C=90$, means 10 short of 100 . Any symbol following one of equal or greater value adds its value- $\mathrm{II}=2$. Any symbol preceding one of greater value subracts its value- $\mathrm{IV}=4$. When a symbol stands between two of greater value its value is subtracted from the second and the remainder is added to the first-XIV $=14$; LIX $=59$. Of two equivalent ways of representing a number, that in which the symbol of larger denomination preceded is preferred-XIV instead of VIX for 14.

|  |  |  |  |
| :--- | :--- | ---: | :--- |
| 1 | I | $\mathbf{8}$ | VIII |
| 2 | $I I$ | 9 | IX |
| 3 | III | 10 | X |
| 4 | $I V$ | 50 | L |
| 5 | $V$ | 100 | C |
| 6 | VI | 500 | D |
| 7 | VII | 1,000 | M |

PHASE ANGLE, TIME INTERVAL, AND FREQUENCY NOMOGRAM
Time delay, phase angle, and frequency are related by the following formula:

$$
\mathrm{t}=\frac{10^{2} \theta}{36 f}
$$

where
$t$ is in milliseconds
$\theta$ is in degrees
$f$ is in hertz

FOR EXAMPLE: A phase angle of $90^{\circ}$ between two $60-\mathrm{Hz}$ wave shapes has a time interval of 4.16 msec . NOTE: Corresponding right-hand frequency and time scales are used logether as are lett-hand frequency and time scales. The range of the nomogram can be extended by multiplying the frequency scale by any power of 10 and dividing the time scale by the same power of 10.

CHARACTERISTICS OF RECURRENT WAVEFORMS-RELATIONSHIP BETWEEN PEAK, RMS, AND AVERAGE VALUES

| Description | Wavetorm | $E_{\text {rms }}$ | $E_{\text {ava }}$ |
| :---: | :---: | :---: | :---: |
| Alternating sine wave |  | $\frac{E_{\text {peak }}}{\sqrt{2}}$ | $\frac{2 E_{\text {peak }}}{\pi}$ |
| Sawtooth wave | $\text { M-1- } \frac{t}{E_{\text {peok }}}$ | $\frac{E_{\text {peak }}}{\sqrt{3}}$ | $\frac{E_{\text {peak }}}{2}$ |
| Clipped sawtooth wave |  | $E_{\text {peak }} \sqrt{\frac{T_{0}}{3 T}}$ | $\frac{E_{\text {peak }} T_{0}}{2 T}$ |
| Square wave |  | $E_{\text {peak }} \sqrt{\frac{1}{2}}$ | $\frac{E_{\text {peok }}}{2}$ |
| Rectified sine wave | の边 | $\frac{E_{\text {paak }}}{\sqrt{2}}$ | $\frac{2 E_{\text {peak }}}{\pi}$ |
| Clipped sine weve | $\xrightarrow[\sim T-1]{\sim}$ | $E_{\text {Dank }} \sqrt{\frac{T_{0}}{2 T}} \stackrel{\begin{array}{c} \text { if } T_{=}^{o r} \\ E_{\text {patk }}^{2} \\ 2 \end{array}}{\substack{0 \\ 0}}$ | $\frac{E_{\text {poak }}}{\pi}$ |
| Allernating square wave |  | $E_{\text {peak }}$ | $E_{\text {peok }}$ |
| Rectangular wave |  | $E_{\text {peak }} \sqrt{\frac{T_{0}}{T}}$ | $\frac{E_{\text {pma }} T_{0}}{T}$ |
| Triangular wave |  | $\frac{E_{\text {peak }}}{\sqrt{3}}$ | $\frac{E_{\text {poak }}}{2}$ |

## FOURIER CONTENT OF COMMON PERIODIC WAVEFORMS

The Fourier content of five common periodic wavelorms, out to the seventh harmonic, is given in this table. Magnitudes only are tabulated-not phase relationships. The magnitudes are those of the voltage waveform, followed by the corresponding percentage values in parentheses. If energy content is desired, these values must be squared. Note that there are no even harmonics present in any of the symmetrical waveforms.

| Waveform | Name | Hasmonic Comporition (magnitude) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Furnd. | 2ad | Jrd | 4th | $51 /$ | 61h | 7 h |
|  | Squire Ware | $\begin{aligned} & \frac{4}{3} E \\ & (127 \%) \end{aligned}$ | 0 <br> ( $0 \%$ ) | $\begin{aligned} & \frac{4}{3 \pi} \mathrm{E} \\ & (42.5 \%) \end{aligned}$ | $10 \%$ | $\begin{aligned} & \frac{4}{5 \pi} \mathrm{E} \\ & (25.5 \%) \end{aligned}$ | 0 (0\%) | $\begin{aligned} & \frac{4}{7 \pi} E \\ & (1 \theta .2 \%) \end{aligned}$ |
|  | Triangular Wave | $\begin{aligned} & \frac{\theta}{F^{2}} E \\ & (61 \%) \end{aligned}$ | $\begin{gathered} 0 \\ (0 \%) \end{gathered}$ | $\begin{aligned} & \frac{8}{9 \pi^{*}} E \\ & (9 \% \%) \end{aligned}$ | $(0 \%)$ | $\frac{6}{25 \pi^{37}}$ $(3.2 \%)$ | $0$ $(0 \%)$ | $\begin{aligned} & \frac{8}{49 \pi^{2}} \mathrm{E} \\ & (1.6 \%) \end{aligned}$ |
|  | Sawrooth Wave | $\begin{aligned} & \frac{2}{\pi} E^{i} \\ & (63.6 \%) \end{aligned}$ | $\begin{gathered} \frac{1}{7} \mathrm{E} \\ \{31.8 \%\rangle) \end{gathered}$ | $\begin{aligned} & \frac{2}{3 \pi} \mathrm{E} \\ & (21.2 \%) \end{aligned}$ | $\begin{gathered} \frac{1}{2 \pi} E \\ (15.9 \%) \end{gathered}$ | $\begin{gathered} \frac{2}{5 \pi} \varepsilon \\ (12.7 \%) \end{gathered}$ | $\begin{aligned} & \frac{1}{3 \pi} \epsilon \\ & (10.6 \%) \end{aligned}$ | $\begin{aligned} & \frac{2}{7 \pi} E \\ & (9.1 \%) \end{aligned}$ |
|  | Half.Weves Rechifigr Output | $\begin{aligned} & \frac{1}{\pi} \mathrm{E} \\ & (01.8 \%) \end{aligned}$ | $\begin{aligned} & \frac{2}{3 \pi} E \\ & \{21.2 \%\} \end{aligned}$ | 0 $(0 \%)$ | $\begin{aligned} & \frac{2}{15 \pi} \xi \\ & (d .2 \%) \end{aligned}$ | $(0 \%)$ | $\begin{aligned} & \frac{2}{35 \pi} E \\ & (1.9 \%) \end{aligned}$ | 0 (0\%) |
|  | full-Wave Rectifies Output | $\begin{gathered} \frac{2}{\pi} E \\ (63.6 \%) \end{gathered}$ | $\begin{gathered} \frac{4}{3 \pi} \mathrm{E} \\ \{42.3 \%\} \end{gathered}$ | 0 <br> (0\%) | $\begin{aligned} & \frac{4}{15 \pi} E \\ & \{0.5 \%\} \end{aligned}$ | $0$ $\{0 \%\}$ | $\begin{aligned} & \frac{4}{35 \pi} E \\ & (3.6 \%) \end{aligned}$ | $\begin{gathered} 0 \\ (0 \%) \end{gathered}$ |





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## DECLBEL NOMOGRAMS

The nomogram below is based on the equation shown and makes possible rapid additlon or subtraction of two or more dB levels.

For ott-scale levels $1,2,5,10,20,30$, etc., can be added or subtracted, simultaneously, to all nomograph scale values. For more than two levels, add any two, and to the first sum add the third, etc.

FOR EXAMPLE: (1) What is the combined sound power level of 70,76 and 80.5 dB ? Align $(\mathrm{dB})_{\mathrm{a}}=76$ with $(\mathrm{dB})_{\mathrm{b}}=70$ and read $(\mathrm{dB})_{t}=77.0$; align $(\mathrm{dB})_{\mathrm{t}}=77.0$ with $(\mathrm{dB})_{\mathrm{b}}=80.5$ and read the answer as $(\mathrm{dB})_{t}=82.1$ dB.
(2) When a fan is on, the sound pressure level equals 68 dB and 64 dB with the fan off. What is the sound pressure level of the fan? To extend the range of the nomogram, subtract 10 from all scale values; align $(\mathrm{dB})_{\mathrm{k}}=68=78-10$ with $(\mathrm{dB})_{\mathrm{a}}=64=74-10$, and read $(\mathrm{dB})_{b}=75.8-10=65.8 \mathrm{~dB}=$ fan sound pressure level.

(From "Nomograph lets you add and subtract decibels," EDN, March 20, 1977, p. 149, courtesy of EDN.)

## DECIBEL NOMOGRAPHS

With the nomograph below and the one on the next page dB gain or loss ol any equipment can be determined (even if input and output impedances difler) if input and output voltages and resistances can be measured. The nomograms cover a power range of 10,000 to 1 , a voltage range of 100 to 1 , and a decibel range from +40 to -40 dB. Voltage and resistance scales of nomogram 1 bearing the same suffix are used together.


FOR EXAMPLE: Determine the gain of an amplifier that produces an output of 5 V across 8 ohms with a $10-\mathrm{V}$ signal applied to its 500 -ohm input. From nomogram 1 , the input power is 0.2 W and the outpul power is 3.1 W, Connecting input and output power on nomogram 11 shows the amplifier gain to be slighlly less than 12 dB .


## LETTER SYMBOLS FOR QUANTITIES USED IN ELECTRICAL SCIENCE AND ELECTRICAL ENGINEERING

## Extracted from IEEE Standard Mo. 280

The tables that follow list quantities grouped in several categories, and give quantity symbols, units based on the International System,* and unit symbols.

Those quantity symbols that are separated by a comma are alternalives on equal standing. Where two symbols for a quantity are separated by three dots (...), the second is a reserve symbol, which is to be used only where there is specific need to avoid a conflict. As a rule the tables do not indicate the vectorial or tensorial character that some of the quantities may have.

The international System of Units (Systeme International d'Unites) is the coherent system of units based on the following units and quantities:

| Unit | Quantity |
| :--- | :--- |
| meter | length |
| kilogram | mass |
| second | time |
| ampere | electric current |
| kelvin | temperature |
| candela | luminous intensity |
| radian | plane angle |
| steradian | solid angle |

This system was named (and given the intemational designation SI ) in 1960 by the Conférence Générale des Poids et Mesures (CGPM). The SI units include as subsystems the MKS system of units, which covers mechanics, and the MKSA or Giorgi system, which covers mechanics, electricity, and magnetism.
*The name of the unit is given as a further guide to the definition of the symbol. A quantity shall be represented by the standard letter symbol appearing in the table regardless of the system of units in which the quantity is expressed.



Bommas senarate symbols on equal standing. Where iwo symbols are separated by three dots the second is a reserve symbol and is to be used only when there is specific need to avoid a conflict. See Introduction to the Tables.

| logerithmic decrement | $\wedge$ | (numeric) |  | then $\delta$ is the dsmpIng coefficient. $\Lambda \approx T \delta$, where $T$ and $\delta$ are as given in the equation of 1,28 . |
| :---: | :---: | :---: | :---: | :---: |
| ettenuation coed. ficiont | 0 | neper por meter | No/m |  |
| phase coefficient | $\beta$ | redian per meter | $\mathrm{rad} / \mathrm{m}$ |  |
| propagation co. efficient | 4 | reciprocal meter | $\mathrm{m}^{-1}$ | $\boldsymbol{\gamma}=\alpha+j \beta$. |
| 2. Mechanics ${ }^{\text {b }}$ |  | kilogram |  |  |
| (mass) density | $\cdots$ | kitogramper cubic mater | $\mathrm{kg} / \mathrm{m}^{3}$ | Mass divided by volume. |
| momentum | $\rho$ | kllogram meter per second | $\mathrm{kg} \cdot \mathrm{m} / \mathrm{s}$ |  |
| moment of inertis | $1, J$ | kilogram meter squared | $\mathrm{kg} \cdot \mathrm{m}^{2}$ |  |
| second (axial) moment of ares | 1, 18 | meter to the fourth power | $\mathrm{m}^{4}$ | Quantities 2.4a and 2.4 b should be distinguished from 2.4. |


${ }^{0}$ The units and corresponding unit symbols are included for use in electrical science and electrical engineering. In mechanics and mechanieal engineering other units and corresponding unit symbols are also used. (USAS Y10.3 now being revised.I

| energy (valume) density | $w$ | jouls per cubic meter | $\mathrm{J} / \mathrm{m}^{3}$ |  |
| :---: | :---: | :---: | :---: | :---: |
| power | $\rho$ | watt | W | Rate of energy trans. fer. $w=\mathrm{J} / \mathrm{s}$ |
| efficiency | 7 | (numeric) |  |  |
| 3. Heat ${ }^{\text {c }}$ |  |  |  |  |
| absalute temperature thermodynamic | $T \ldots \theta$ | kelvin | K | In 1967 the CGPM voled to give the |
| temperature |  |  |  | name kelvin to the SI unit of rempera- |
|  |  |  |  | turo, which was |
|  |  |  |  | formerly called degree Kolvin, and to |
|  |  |  |  | assign it the symbel |
|  |  |  |  | $K$ lwithgut the |
|  |  |  |  | symbol ${ }^{\circ}$ ). |



CThe units and corresponding unit symbols are included for use in electrical science and engingering. In mechanicel engineering other units and corresponding unit symbols are also used. (Cf. USAS Y 10.4.)

| thermal conduc. tivity | A...k |
| :---: | :---: |
| thermal conduc. tance | $\boldsymbol{G}_{\boldsymbol{\theta}}$ |
| thermal resistivity | ${ }^{2} 8$ |
| thermal resistarice | $\boldsymbol{F}_{8}$ |
| thermat capacitance | $C_{\theta}$ |
| heat capacizy |  |
| thermal imped- | $z_{8}$ |
| anca |  |
| specific heat | c |


| watt per meter keivin | $W /(m \cdot K)$ |  |
| :---: | :---: | :---: |
| watt per kelvin | W/K |  |
| meter kalvin per watt | m. K/N |  |
| kelvin per watt | KNW |  |
| joule per kelvin | J/K |  |
| kelvin per watt | KNW |  |
| joula par kelvin kilo. gram | $\mathrm{J} /(\mathrm{K} \cdot \mathrm{kg})$ | Heat capacity divided by mass. |






| Item Quantity | Quantrity Symbord | Unit Based on International System | Unit Symbol | Remarks |
| :---: | :---: | :---: | :---: | :---: |
| hysteresis coefficient | $k_{h}$ | (nurneric) |  | The neme cycle per sweond (c/s) is also used for this unit. |
| eddy-current coafficient | $k_{\mathrm{e}}$ | (numeric) |  |  |
| phasa angle <br> phase difference | $\phi, \theta$ | rsdian | red |  |
| 6. Electronics and Tejecommunication carrier frequency | $f_{C}$ | hertz | Hz |  |
| instantaneous frequency | $f_{r} f_{i}$ | hertz | Hz |  |
| Fntermediate frequency | $f_{\mathrm{i}}, f_{\text {if }}$ | hertz | Hz |  |
| modulation frequency | $f_{\mathrm{m}}$ | hertz | Hz |  |
| pulse repetition frequency | $f_{\mathrm{p}}$ | hertz | Hz |  |
| frequency deviation | $f_{d}$ | hertz | Hz |  |
| Doppler frequency shift | ${ }^{\prime} \mathrm{D}$ | hertz | Hz |  |
| pulse duration | ${ }^{1} \mathrm{p}$ | second | * |  |
| rise time tof a pulse) | ${ }_{T}$ | second | 3 |  |
| ```fall time (of a pulse) decay time (of a pulsel``` | $f_{f}$ | second | \% |  |
| duty factor pulse duty factor | $D$ | inumerict |  | $D=t_{p} f_{\mathrm{p}}$ |
| phase propagation time | ${ }^{\boldsymbol{t}}{ }_{\phi}$ | second | 5 |  |
| group propagation time | $t_{9}$ | second | , |  |
| duration of a signal element | 7 | second | s |  |
| signaling speed | $1 / \mathrm{r}$ | bsud | Ed |  |
| cathode-heating time | ${ }^{\prime} /{ }^{\prime}$ | second | $s$ |  |
| deionization time | ${ }^{\text {d }}$ | second | $5$ |  |
| ionization time | $\mathrm{t}_{\mathrm{i}}$ | second | 5 |  |
| form factor | $k_{f}$ | \{numeric) |  |  |
| distortion factor | $k_{d}$ | (numeric) (numeric) |  |  |
| modulation factor (AM) | $m$ | (numeric) |  |  |
| modulation index (FM) | 7 | Inumeric) |  |  |
| signal power | $P_{5} . S$ | watt |  |  |
| noise power | $P_{\text {n }}, N$ | watt | W |  |
| noise-power density | No | watt per hertz | W/Hz |  |
| energy of a signal element | $E$ | joule | 1 |  |
| signat-to norse power, ratio ${ }^{-}$ | A, S/N | (numeric) |  | $R=P_{5} / P_{n}$ |
| elementary signal-to-noise ratioe | A, $\boldsymbol{R}_{\mathbf{e}}$ | inumeric) |  | $R_{e}=E / N_{0}$ |
| gain (power) ${ }^{\text {e }}$ | $G$ | (numeric) |  |  |
| amplification tcurrent or voltege)e | A | (numeric) |  |  |
| noise factore ${ }^{e}$ nolse figure | $F$ | (numaric) |  |  |




## LETTER SYMBOLS FOR UNITS USED IN ELECTRICAL SCIENCE AND ELECTRICAL ENGINEERING

## Extracted from IEEE Standard No. 260

The use of unit symbols, instead of the spelled-out names of the units, is frequently desirable where space is restricted. Their use presupposes that the reader will find them intelligible. If there is any doubt that the reader will understand a symbol, the name of the unit should be written in full. When an unfamiliar unit symbol is first used in text, it should be followed by its name in parentheses; only the symbol need be used thereafter. Explanatory notes or keys should be included where-appropriate on drawings and in tabular matter.

The use of unit symbols is never mandatory, but when unit symbols are employed they must conform to those given in the Standard.

## List of Symbols

Symbols for units are listed alphabetically by name of unlt below. The list is intended to be reasonably complete, but could not possibly include all units that might concelvably be used in modern eiectrical technology. Many compound symbols and many illustrations of the use of the metric prefixes are included. Other combined forms may easily be constructed.

Every ethort should be made to maintain the distinction between upper- and lowercase letters shown in the list, wherever the symbols for units are used, even if the surrounding text uses uppercase style.
in the notes accompanying the symbols, some units are identified as SI units. These units belong to the International Systern of Units (Système International d'Unités), which is the name given in 1960 by the Conference Generale des Poids et Mesures to the coherent system of units based on the following basic units and quantities:

| Unit | Quantity |
| :--- | :--- |
| meter | length |
| kilogram | mass |
| second | time |


| Unit | Quantity |
| :--- | :--- |
| ampere | electric current |
| kelvin | temperature |
| candela | luminous intensity |

The Sl units include as subsystems the MKS system of units, which covers mechanics, and the MKSA or Giorgi system, which covers mechanics, electricity, and magnetism.


LETTER SYMBOLS FOR UNITS USEDIN ELECTRIGAL SCIENCE AND ELECTRICAL ENGINEERING


| Unit | Symbof | Remarks |
| :---: | :---: | :---: |
| footlambert | $f$ | If fuminance is to be measured in English units, the candela per square foot ( $\mathrm{cd} / \mathrm{ft}{ }^{2}$ ) is preferred. |
| foot per minute | $\mathrm{ft} / \mathrm{min}$ |  |
| foot per second | $\mathrm{ft} / \mathrm{s}$ |  |
| foot per second squared | $\mathrm{ft} / \mathrm{s}^{2}$ |  |
| foot poundal | $\mathrm{ft} \cdot \mathrm{pdl}$ |  |
| foot pound-force | $\mathrm{ft} \cdot \mathrm{lbf}$ |  |
| gal | Gal | $1 \mathrm{Gal}=1 \mathrm{~cm} / \mathrm{s}^{2}$ |
| gallon | gal | The gatlon, quart, and pint differ in the |
| galion per minute | gal/min | U.S. and the U.K. and their use is depre. cated. |
| gauss | G | The gauss is the electromagnetic CGS unit of magnetic flux density. Use of SI unit, the tesla, is preferred. |
| gigacycle per second | Gc/s | See note for cycle per second. |
| gigaelectronvolt | Gev |  |
| gigaheriz | GHz |  |
| gifbert | Gb | The gilbert is the electromagnetic CGS unit of magnetomotive force. Use of the S। unit, the ampere for ampere turn), is preferred. |
| gram | $g$ |  |
| henry | H |  |
| hertz | $\mathrm{Hz}_{2}$ |  |
| horsepower | hp |  |
| hour | h | Time may be designated as in the following example: $9^{h} 46^{m} 30^{t}$. |
| inch | in |  |
| inch per second | $\mathrm{in} / \mathrm{s}$ |  |
| joule | J |  |
| joule per kelvin | J/K |  |
| kelvin | K | In 1967 the CGPM gave the name kelvin to the SI unit of temperature which had farmerly been called degree Kelvin and assigned it the symbol $K$ iwithout the symbot ${ }^{\circ}$ ). |
| kilocycle per second | kc/s | See note for cycle per second. |
| kiloelectronvolt | keV |  |
| kilogauss | kG |  |
| kilogram | kg |  |
| kilogram-force | kgt | In some countries the name kilopond (kp) has been adopted for this unit. |
| kilohercz | kHz |  |
| kilojoule | k.」 |  |
| kilohm | $k \Omega$ |  |
| kilometer | km |  |
| kilometer per hour | $\mathrm{km} / \mathrm{h}$ |  |
| kilovar | kvar |  |


| Unit | Symbol | Remarks |
| :---: | :---: | :---: |
| kilovolt | kV |  |
| kilovoltampere | kVA |  |
| kilowatt | kW |  |
| kilowathour | kWh |  |
| knot | knot |  |
| lambert | L | The lambert is the CGS unit of luminance. Use of the SI unit, the candela per square meter, is preferred. |
| liter | 1 |  |
| liter per second | 1/s |  |
| lumen | Im |  |
| lumen per square foot | $\mathrm{im} / \mathrm{ft} \mathrm{t}^{2}$ |  |
| humen per square meter | $\mathrm{mm} / \mathrm{m}^{2}$ |  |
| tumen per watt | $1 \mathrm{~m} / \mathrm{W}$ |  |
| Iumen second | 1 m |  |
| lux | $1 \times$ | $1 \mathrm{~lx}=1 \mathrm{~lm} / \mathrm{m}^{2}$ |
| maxwell | M ${ }^{\text {I }}$ | The maxwell is the electromagnetic CGS unit of magnetic flux. Use of the SI unit, the weber, is preferred. |
| megacycle per second | $\mathrm{Mc} / \mathrm{s}$ | See note for cycle per second. |
| megaelectronvolt | MeV |  |
| megahertz | MHz |  |
| megavolt | MV |  |
| megawatt | MW |  |
| megohm | $M \Omega$ |  |
| meter | m |  |
| mho | mho | The IEC has adopted the name siemens (S) for this unit. |
| microampere | $\mu \mathrm{A}$ |  |
| microbar | $\mu \mathrm{bar}$ |  |
| microfarad | $\mu \mathrm{F}$ |  |
| microgram | $\mu \mathrm{g}$ |  |
| microhenry | $\mu \mathrm{H}$ |  |
| micrometer | $\mu \mathrm{m}$ |  |
| micromho | $\mu \mathrm{mho}$ | See note for mho. |
| micron | $\mu \mathrm{m}$ | The name micrometer is preferred. |
| microsecond | $\mu_{5}$ |  |
| microsiemens | $\mu \mathrm{S}$ |  |
| microwatt | $\mu \mathrm{W}$ |  |
| mil | mil | $1 \mathrm{mil}=0.001 \mathrm{in}$ |
| mile (statute) | mi |  |
| nautical mile | nmi |  |
| mile per hour | $\mathrm{mi} / \mathrm{h}$ |  |
| milliampere | mA |  |
| millibar | mbar |  |
| millibarn | mb |  |
| milligal | mGat |  |
| milligram | mg |  |
| millihenry | mH |  |


| Unit | Symbol | Remarks |
| :---: | :---: | :---: |
| millifiter | ml |  |
| millimeter | mm |  |
| conventional millimeter of mercury | $\mathrm{mmHg}^{\text {a }}$ | $1 \mathrm{mmHg}=133.322 \mathrm{~N} / \mathrm{m}^{2}$ |
| millimicron | nm | The name nanometer is preferred. |
| millisecond | ms |  |
| millisiemens | mS |  |
| millivalt | mV |  |
| milliwatt | mW |  |
| minute [plane angle] | ... |  |
| minute (time) | $\min$ | Time may be designated as in the following example: $9^{\text {th }} 46^{m} 30^{5}$ |
| nanoampere | nA |  |
| nanofarad | nF |  |
| nanometer | nm |  |
| ranosecond | ns |  |
| nanowatı | nW |  |
| nautical mile | nmi |  |
| neper | Np |  |
| newton | N |  |
| newton meter | $N \cdot m$ |  |
| newton per square meter | $\mathrm{N} / \mathrm{m}^{2}$ |  |
| oersted | Oe | The oersted is the electromagnetic CGS unit of magnetic field strength. Use of the SI unit, the ampere per meter, is preterred. |
| ohm | $\Omega$ |  |
| ounce (avoirdupois) | Oz |  |
| piccampere | pA |  |
| picofarad | pF |  |
| picosecond | ps |  |
| picowatt | ow |  |
| pint | pt | The gallon, quart, and pint differ in the U.S. and the U.K., and their use is deprecated. |
| pound | Ib |  |
| poundal | pdl |  |
| pound-force | lbf |  |
| pound-force foot | $\mathrm{lbf} \cdot \mathrm{ft}$ |  |
| pound-force per square inch | $\mathrm{lb} / \mathrm{in}^{2}$ |  |
| pound per square inch |  | Although use of the abbreviation psi is common, it is not recommended. See pound-force per square inch. |
| quart | qt | The gallon, quart, and pint differ in the U.S. and the U.K., and their use is deprecated. |
| red | rd | Unit of absorbed dose in the field of radiation dosimetry. |
| radian | rad |  |
| rem | rem | Unit of dose equivalent in the field of radiation dosimetry. |


| Unit | Symbol | Remarks |
| :---: | :---: | :---: |
| revolution per minute | r/min | Although use of the abbreviation fprn is common, it is not recommended. |
| revalution per second | r/s |  |
| roentgen | R | Unit of exposure in the field of radiation dosimetry. |
| second (piane angle] | . . ${ }^{\prime \prime}$ |  |
| secord (time) | s | Time may be designated as in the following example: $9^{n} 46^{n} 30^{s}$. |
| siemens | S | $1 S=1 \Omega^{-1}$ |
| square foot | $\mathrm{ft}^{2}$ |  |
| square inch | $\mathrm{in}^{2}$ |  |
| square meter | $\mathrm{m}^{2}$ |  |
| square yard | $\mathrm{Vd}^{2}$ |  |
| steradian | sr |  |
| testa | : ${ }^{\text {T }}$ | $1 \mathrm{~T}=1 \mathrm{~Wb} / \mathrm{m}^{2}$ |
| tonne | t | $\boldsymbol{t} \mathbf{t}=1000 \mathrm{~kg}$ |
| (unified) atomic mass unit | u | The (unified) atomic mass unit is defined as one-twelfth of the mass of an atom of the ${ }^{12} \mathrm{C}$ nuclide. Use of the old atomic mass unit (amu), defined by reference to oxygen, is deprecated. |
| var | var | Unit of reactive power |
| volt | V |  |
| voltampere | VA | Unit of apparent power |
| watt | W |  |
| watthour | Wh |  |
| watt per steradian | W/sr |  |
| watt per steradian square meter | W/sr $\cdot \mathrm{m}^{2}$ ) |  |
| weber | Wb | $1 \mathrm{~Wb}=1 \mathrm{~V} \cdot \mathrm{~s}$ |
| vard | Yd |  |

## COMVERSKON OF ELECTROMAEMETIC UWTS

Three common systems of electromagnetic units are in universal employ. They are:

1. The absolute system of CGS electromagnetic system.
2. The practical CGS electromagnetic system.
3. The MKS system (Gaussian of Giorgi depending upon the choice of constants).

The chart allows rapid conversion from one system to another. In any one row, any quantity divided by any other quantity produces unily.

These Quantities Are Those Effected by Rationalization

| Quantily | Rationalized |  |  | Unrationalized |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | MKS | CGS Em | CGS Es | MKS | CGS EM | çs Es |
| Dielectric displacement | 1 | 10-5 | $3 \times 10^{5}$ | $4{ }^{4}$ | $4 \pi \times 10^{-5}$ | $12 \pi \times 10^{5}$ |
|  | $10^{5}$ | 1 | $3 \times 10^{10}$ | $4 \pi \times 10^{5}$ | 47 | $12 \pi \times 10^{10}$ |
|  | $1 / 3 \times 10-5$ | $1 / 3 \times 10-10$ | 1 | $4 \mathrm{H} / 3 \times 10^{-5}$ | $4 \pi / 3 \times 10-10$ | 48 |
|  | $1 / 4 \pi$ | $1 / 4 \pi \times 10^{-5}$ | $3 / 4 \pi \times 10^{3}$ | 1 | $10-5$ | $3 \times 10-5$ |
|  | $1 / 4 \pi \times 10^{5}$ | $1 / 4 \pi$ | $3 / 4 \pi \times 10^{10}$ | $10^{5}$ | 1 | $3 \times 10^{10}$ |
|  | $1 / 12 \times \times 10^{-5}$ | $1 / 12 \pi \times 10^{-10}$ | $1 / 4 \pi$ | $1 / 3 \times 10^{-5}$ | $1 / 3 \times 10^{-10}$ | 1 |
| Unit: | Coulomb/m ${ }^{2}$ | Abcoulomb/m2 | Statcoulomb/ $\mathrm{cm}^{2}$ | Coulomb/m2 | Abcoulomb/ $/ \mathrm{cm}^{2}$ | Stoteoulomb/ $\mathrm{cm}^{2}$ |
| Magnetic fiald intensity | 1 | 10-3 | $3 \times 10^{7}$ | $4 \pi$ | $4 \pi \times 10^{-3}$ | $12 \pi \times 10^{7}$ |
|  | $10^{3}$ | 1 | $3 \times 10^{10}$ | $17 \times 10^{3}$ | 4 | $12 \pi \times 10^{10}$ |
|  | $1 / 3 \times 10^{-7}$ | $1 / 3 \times 10^{-10}$ | 1 | $1 \pi / 3 \times 10^{-7}$ | $4 \pi / 3 \times 10^{-10}$ | $4 \pi$ |
|  | $1 / 4 \pi$ | $1 / 4 * \times 10^{-3}$ | $3 / 4 \pi \times 10^{7}$ | 1 | $10^{-3}$ | $3 \times 10^{7}$ |
|  | $1 / 4 \pi \times 10^{3}$ | $1 / 4 \pi$ | $3 / 4 \pi \times 10^{10}$ | $10^{3}$ | 1 | $3 \times 10^{10}$ |
|  | $1 / 12 \pi \times 10^{-7}$ | $1 / 12 \pi \times 10-10$ | $1 / 4 \pi$ | $1 / 3 \times 10^{-7}$ | $1 / 3 \times 10^{-10}$ | 1 |
| Units | Ampotum/m | Oersted | ESU | Amp.tuen/m | Oersted | ESU |
| Megnetometlve force | 1 | 10-1 | $3 \times 10^{9}$ | $4 \pi$ | $48 \times 10-1$ | $120 \times 109$ |
|  | 10 | 1 | $3 \times 10^{10}$ | $40 \%$ | 4 1 | $12 \pi \times 10^{10}$ |
|  | $1 / 3 \times 10^{-9}$ | $1 / 3 \times 10^{-10}$ | 1 | $4 \pi / 3 \times 10^{-9}$ | $4 \times / 3 \times 10-10$ | $4 \pi$ |
|  | 1/4r | $1 / 4 n \times 10^{-1}$ | $3 / 4 \pi \times 10^{9}$ | 1 | $10-1$ | $3 \times 10^{9}$ |
|  | 10/4 ${ }^{1 / 2}$ | $1 / 4 \pi$ | $3 / 4 \pi \times 10^{10}$ | 10 | 1 | $3 \times 1010$ |
|  | $1 / 12 \pi \times 10-9$ | $1 / 12 \pi \times 10^{-10}$ | $1 / 4$. | $1 / 3 \times 10^{-9}$ | $1 / 3 \times 10-10$ | 1 |
| Unit* | Amp-turn | Gilbert | ESU | Amprorn | Gilbert | ESU |


|  | Practical Unit | Evactromagnetic Unit | Electrostatic Unit |
| :---: | :---: | :---: | :---: |
| Quontlly | MKS | Cos Em | $\cos 65$ |
| 1. Coperitucte | 1 Farad | $10^{-9}$ Ablarad | $9 \times 10^{11}$ starfarad |
|  | $10^{9}$ Farded | 1 Abforad | $9 \times 10^{20}$ Statiorad |
|  | $1 / 9 \times 10^{-11}$ Forad | 1/9 a $10-20$ ablorod | 1 saratored |
| 2. Ohorye | 1 Couloch | 10-1 Absoulomb | $3 \times 10^{9}$ Statsoulound |
|  | 10.0 Coviamb | 1 Abeoulamb | $3 \times 1010$ Slatcoulemb |
|  | $1 / 3,10^{-9}$ Coulomb | $1 / 3 \times 19^{-10}$ Alcoulonb | 15 totcrulogb |
| 3. Charge densily | 1 Covlomb/m ${ }^{3}$ | $10 \rightarrow 7$ Abrowlanp/cm ${ }^{3}$ | 3. $10^{3}$ Statcoulemb/ $\mathrm{cm}^{3}$ |
|  | ${ }_{10} 7$ Coutiomb/m ${ }^{3}$ | 1 Abcoulomb/em ${ }^{3}$ | $3 \times 10^{10}$ Sigatgoulomb/ $\mathrm{cm}^{3}$ |
|  | $1 / 3 \times 10^{-3}$ Coutomb/m ${ }^{3}$ | $1 / 5 \times 10^{-10}$ Abeorlamb/cm ${ }^{\text {2 }}$ | 1 statcrutamb/em ${ }^{3}$ |
| 4. Conduetivity | $1 \mathrm{mho} / \mathrm{m}$ | $10^{-11}$ Abenta/cm | $9.10{ }^{9}$ Slatmhe/ $/ \mathrm{sm}$ |
|  | ${ }_{3} 0^{11}$ Mhemm | 1 Abumho/cm | 9 $: 10^{20} \mathrm{Slotmhaz} / \mathrm{cm}$ |
|  | $1 / 9 \times 10-9 \mathrm{mho} / \mathrm{m}$ | 1/9 $: 10-20$ Abmha/em | $15 \mathrm{tg} \mathrm{lagho} / \mathrm{cm}$ |
| 3. Currmi | 1 Ampars | $10^{-1}$ abompers | 3.1099 Stetompate |
|  | Lo Anperis | 1 Abempare | $3 \times 10^{\text {F0 }}$ Statampure |
|  | 1/3×10-9 Ampar* | $1 / 3 \leq 10^{-10}$ Abameara | 1 Statampers |
| 6. Curumi dentily | 1 Ampara/m ${ }^{2}$ | 19-5 Abomparnem? | 3. 1055 Statemera/ce ${ }^{3}$ |
|  | $10^{5}$ Amabat $/ \min ^{2}$ | 1 Absmorem/cm ${ }^{2}$ | 3 s 10 $10^{10}$ Stolampore/ $/ \mathrm{cm}^{2}$ |
|  | $1 / 3 \times 10-5$ Ampura/m ${ }^{2}$ | $1 / 3 \times 10-10$ Abamperes/sm ${ }^{2}$ | $15191 \mathrm{mpout} / \mathrm{cm}^{2}$ |
| 7. Electric field intentity | $1 \mathrm{Yal} / \mathrm{mal}$ | $10^{6}$ Abvol $1 / \mathrm{cm}$ | $1 / 3 \times 10^{-t} 5$ Stataib/em |
|  |  | 1 Abvolt/ea | $1 / 3 \mathrm{z}$ Ip-10 Stalyali/cm |
|  | $3 \times 10^{4} \mathrm{~V}_{\text {olt }}$ /nuter | $3 \times 1010$ Abvolt/cm | 15 talvoli/cm |
| a. Elastric poturial | 1 Yolt | $10^{\text {A A A wollis }}$ | $3 / 3 \pm 10^{-2}$ Stalvalte |
|  | 10-8 Vall | 1 Abwalt | $1 / 3 \times 10-90$ Stalugis |
|  | 3-102 $\mathrm{V}_{0}$ | $3 \times 7010$ abvolts | 1 Statueli |
| 8. Electric dipole moment | 1 Coulombumaler | 10 Abcoulomb-cm | 3x $10^{11}$ Statsoulombeem |
|  | 10-1 Coulernt-ater | 1 Abeaulamb-cm | 3 E if 10 Storsoplomb-cm |
|  | $1.2 \times 20^{-11}$ Coutamt-mets | $\{1 / 3=10-10$ Abcoulombecm | 1 3totcoulomb-cm |
| 10. Enulay | 1 Joul: | $10^{7} \mathrm{Erg}$ | $10^{7} \mathrm{ErO}$ |
|  | 10-9 joul. | 1 Erg | 1 ErO |
|  | 50-9 dovis. | 1 Erg | 1 Erg |
| 11. Fores | 1 Nowlen. | $10^{5}$ Dyn: | $10^{5}$ Ornt |
|  | 10-5 Nawion | 1 Dra" | 1 Dyna |
|  | $10-5$ Nextan | 1 Dyse | 10x |
| 12. Fiva dencior | 1 weborcm ${ }^{2}$ | $10^{4}$ goun | $1 / 3 \times 10^{-6 / 44}$ |
|  | 10-4 Weber'm ${ }^{\text {\% }}$ | 1 Gausa | $13 \times 10^{-19}$ anw |
|  | $1 \times 10^{4}$ Webw $/ \mathrm{m}^{2}$ | 3-10 10 Gaun | Insw |
| 12. Imductence | 1 Hemrg | $10^{9}$ abhenry | $1 / 9 \times 10^{-11}$ stathemry |
|  | 10.9 Hanty | 1 Abhanry | $1 / 9 \times 10-705$ tamenir |
|  | $9 \times 10^{11}$ Honry | $19 \times 10^{20}$ athenty | 15 tathenfy |
| 14. indursive capatioy | 1 Foted/metaic | $10^{-11}$ Asmaradicm | $9.13^{9}$ Statieradicm |
|  | roil Forod muter | 1-ktratad/cm | 9 $\times 10^{20}$ Staflatodicm |
|  | 1/9 , 10-9 Forad/mbrat | $1 / 9: 10^{-20}$ Abiarad/em | 15 tefiorod/sm |
| 15. Maghatic flux | 1 Webor | $10^{\circ}$ Heswel\| | $1 / 3 \times 10-240$ |
|  | 10-n Wober | \| Mraswal| | $1 / 3 \times 10-10 \mathrm{axu}$ |
|  | 3. 102 Wabar | $3 \times 1010$ mamel\| | 1-20 |
| 18. Magnotic dipole moment | 1 Ampert-matar ${ }^{2}$ | $10^{2}$ Abomp-com ${ }^{\text {a }}$ | $3=10^{12} 5 \times 80 m p-5{ }^{2}$ |
|  | $10^{-3}$ Anpure-matar ${ }^{\text {2 }}$ | 1 Abeap-cm ${ }^{2}$ | 3) $10^{10} 5$ Stelemp-cm ${ }^{2}$ |
|  | //3 $\times 10=12$ Amperematar ${ }^{2}$ | $13 \times 10-10 \mathrm{Abamp}-\mathrm{m}^{2}$ | 15 totomp- $\mathrm{sm}^{2}$ |
| 17. Pemeability | 1 Henry masar | $10^{7}$ Abhanry cm |  |
|  | $10^{-7}$ Henir mater | 19 Abhenir cm | 1/9 $\times 10$-70 Stothentyitu. |
|  | $0: 10^{13}$ Henty matar | $9 \times 10^{20}$ Athanry $<\mathrm{m}$. | 1 Stationry sm |
| I8. Power | 1 Walt | $10^{7}$ He/rec | $10^{7}$-ta/ase |
|  | 10-7 Way | 1-40.zec | 1 -refore |
|  | 10-7 Wort | $1{ }^{1}$ | I erg/ase |
| 19. Recialenet | 10 hm | $10^{\circ}$ Abohm | $1 / 9.100^{11}$ Sratahion |
|  | 10-90hm | 1 Abohm | 1/9, $10-20$ statehm |
|  | $\cdots \times 10^{11} 0 \mathrm{hm}$ | $10.10 \%$ aboke | 15 ratohm |

## SPACE-TIME-VELOCITY AND ACCELERATION FORMULAS

This tabulation presents all basic linear motion formulas with all their variations. Terms are defined and units of measurement are specified.
A = Acceleration or deceleration- $\mathrm{H} / \mathrm{sec} / \mathrm{sec}$ ( 32.2 for gravity)
D = Distance- It (may be used in lieu of " H " in vertical free fall)
E = Energy-fl-lbs
$F=$ Force -lbs
H = Height -ft (may be used lieu of " $D$ " with A-32.2)
$M=$ Mass $\quad \frac{\mathrm{W}}{32.2}=\frac{\mathrm{lb}-\mathrm{sec}^{2}}{\mathrm{Ht}}$
T = Time-sec
$\mathrm{V}_{\mathrm{e}}=$ Average velocity- $\mathrm{ft} / \mathrm{sec}$
$V_{f}^{2}=$ Final velocity-ft/sec
$\mathrm{V}_{\mathrm{I}}=$ initial velocity- $\mathrm{t} / \mathrm{sec}$
$\mathrm{W}=$ Weight -lbs

CONVERSION FACTORS

| To Convert | Into | Mutiply 8 y | To Convert | Into | Multipfy $\mathrm{BV}^{\text {V }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| A |  |  |  |  |  |
| Abcoulomb | Statcoulombs | $2.998 \times 10^{10}$ | ares | sq meters | 100.0 |
| Acre | Sq. chain (Gunters) | 10 | Astronomical Unit | Kilometers | $1.495 \times 10^{8}$ |
| Acre | Pods | 160 | Atmospheres | Ton/sq. inch | . 007348 |
| Acre | Square links \{Gunters) | $1 \times 10^{5}$ | atmospheres | cms of mercury | 76.0 |
| Acre | Hectare or sq. |  | atmospheres | $f\left(\right.$ of water (at $4^{\circ} \mathrm{C}$ ) | 33.90 |
|  | hectometer | . 4047 | atmospheres | in. of mercury (at $0^{\circ} \mathrm{C}$ ) | 29.92 |
| acres | sq feet | 43,560.0 | atmospheres | $\mathrm{kgs} / \mathrm{sq} \mathrm{cm}$ | 1.0333 |
| acres | sa meters | 4,047. | atmospheres | kgs/sq meter | 10,332. |
| acres | sa miles | $1.562 \times 10^{-3}$ | atmospheres | pounds/sq.in. | 14.70 |
| acres | sq yards | 4,840. | atmospheres | tons/sq ft | 1.058 |
| acre-feet | ou feet | 43,560.0 | B |  |  |
| acre-feet | galions | $3.259 \times 10^{5}$ |  |  |  |
| amperes/sq cm | $a m p s / s q$ in. | 6.452 | Berrels (U.S., dry) | cu . inches | 7056. |
| amperes/so cm | amps/sq meter | $10^{4}$ | Barrels (U.S., div) | quarts (dry) | 105.0 |
| amperes/sq in. | $\mathrm{amps} / \mathrm{sq} \mathrm{cm}$ | 0.1550 | Barrels (U.S., liquid) | gallons | 31.5 |
| amperes/sq in. | amps/sq meter | 1,550.0 | barreis (oil) | gallont (oil) | 42.0 |
| amperes/sq meter | $a \mathrm{mps} / \mathrm{sq} \mathrm{cm}$ |  | bars | atmospheres | 0.9869 |
| amperes/sa meter | amps/sq in, | $6.452 \times 10^{-4}$ | bars | dynes/sa cmin |  |
| amperehours | coulombs | 3.600 .0 | bars | kgs/sq meter | $1.020 \times 10^{4}$ |
| ampere-hours | faradays | 0.03731 | bars | pounds/sq ft | 2,089. |
| ampere-turns ${ }^{\text {a }}$ | gilberts | 1.257 | bars | pounds/sq in. | 14.50 |
| ampere-turns/cm | amp-turns/in. | 2.540 | Baryl | Dyne/sq. cm. | 1.000 |
| ampere-turns/cm | amp-turns/meter | 100.0 | Bolt IUS Clotht | Meters | 36.576 |
| ampere-tuins/cm | gilberts/cm | 1.257 | ETU | Liter-Atmosphere | 10.409 |
| ampere-turns/in. | amp-turns/cm | 0.3937 | Btu | ergs | $1.0550 \times 10^{10}$ |
| ampereturns/in. | amp turns/meter | 39.37 | Btu | foot-lbs | 778.3 |
| ampere-turns/in, | gilberts/am | 0.4950 | Etu | gram-calories | 252.0 |
| ampere-turns/meter | amp-turns/cm | 0.01 | Btu | horsepowerthrs | $3.931 \times 10^{-4}$ |
| ampere-turns/meter | amp-turns/in. | 0.0254 | Btu | joules | 1,054.8 |
| ampere-turns/meter | gilberts/cm | 0.01257 | Btu | kilogram-calories | 0.2520 |
| Angstrom unit | Inch | $3937 \times 10^{-9}$ | Btu | kilogram-meters | 107.5 |
| Angstrom unit | Meter | $1 \times 10^{-10}$ | Btu | kilowatt-hrs | $2.928 \times 10^{-4}$ |
| Angstrom unit | Micron or (Mu) | $1 \times 10^{-4}$ | Btu/hr | foot-pound/sec | 0.2162 |
| Are | Acre (US) | . 02471 | Btu/hr | gram-cal/sec | 0.0700 |
| Ares | sq. yards | 119.60 | Btu/hr | horsepower-hrs | $3.929 \times 10^{-4}$ |
| ares | acres | 0.02471 | Etu/hr | watts | 0.2931 |



| fato |
| :--- |
| gallons (U.S. liq.) |
| lizers |
| pints (U.S. liq.) |
| quarts (U.S. liq.) |
| bushels (dry) |
| cu cms |
| cu inches |
| cu meters |
| cu yards |
| gallons (U.S. liq.) |
| liters |
| pints (U.S. Ilq.) |
| quarts (U.S. Iiq.) |
| cu cms/sec |
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| liters/sec ( |
| pounds of water/min |
| million gals/day |
| gallons/min |
| cu cms |
| cu feet |
| cu meters |
| cu yards |
| gallons (U.S. liquid) |
| liters |
| mil-feet |
| pints (U.S. liq.) |
| quarts (U.S. liq.) |
| bushels (diry) |
| cu cms |
| cu feet |
| cu inches |
| cu yards |
| gallons (U.S. liq.) |
| liters |
| pints (U.S. liq.) |

To Convert
cubic centimeters cubic centimeters cubic centimeters

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$\stackrel{y}{6}$

$\stackrel{0}{3}$芯 cubic feet | 5 |
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| 0 |范 cubic feet $/ \mathrm{min}$








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 cubic meters | $\stackrel{4}{4}$ |
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| $\frac{0}{3}$ |






quarts（U．S．liq．）
cu cms
cu feet
cu inches
cu meters
gallons（U．S．liq．）
liters
pints（U．S．liq．）
quarts（U．S．liq．）
cubic ft／sec
gallons／sec
liters／sec
$\quad$ D
Gram
seconds
grams
liters
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seconds
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revolutions／min
revolutions／sec
grams
liters
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ounces（troy）
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grains
ounces
Erg／sq．millimeter
Atmospheres
cubic meters cubic meters
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$\frac{0}{3}$
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 cubic yards cubic yards／min 들
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$\frac{0}{0}$
$\frac{3}{3}$ cubic yards／min Dalton
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dacimeters
degrees（angle）
degress（angle）
diggrees（angle）
degraes／sec
degrees／sec
degres／sec
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dekameters Drams（apothecaries＇ or troy） Drams（apothecaries＇
or troy）
Drams（U．S．， Drams（apothecaries＇
or troy）
Drams（U．S．． Drams（U．S．，

fluid or apo fluid or apoth．）帚 E | E |
| :---: |
| $\stackrel{y}{0}$ |
| 豆 |

Dyne／sq．cm．


| centimeter－grams | pound－feet |
| :--- | :--- |
| centimeters of mercury | atmospheres |
| centimeters of mercury | feet of water |
| centimeters of mercury | kgs／sq meter |
| centimeters of mercury | pounds／sq ft |
| centimeters of mercury | pounds／sq in． |
| centimeters／sec | feet／min |
| centimeters／sec | feet／sec |
| centimeters／sec | kilometers／hr |
| centimeters／sec | knots |
| centimeters／sec | meters／min |
| centimeters／sec | miles／hs |
| centimeters／sec | miles／min |
| centimeters／sec／sec | feet／sec／sec |
| centimeters／sec／sec | kms／hr／sec |
| centimeters／sec／sec | meters／sec／sec |
| centimeters／sec／sec | miles／hr／sec |
| Chain | Inches |
| Chein | meters |
| Chains（survevors＇ |  |
| or Gunter＇s） | vards |
| circuler mils | sq cms |
| cireuiar mils | sq mils |
| Circumference | Redians |
| circular mils | sq inches |
| Cords | cord feet |
| Cord feet | cu feet |
| Coulomb | Statcoulombs |
| coulombs | faradays |
| coulombs／sq cm | coulombs／sq in． |
| coulombs／sq cm． | coulombs／sq meter |
| coulombs／sq in． | caulombs／sq cm |
| coulombs／sq in． | coulombs／sq meter |
| coulombs／sq meter | coulombs／sq cm |
| coulombs／sq meter | coulombs／sq in． |
| cubic centimeters | cu feet |
| cubic centimeters | cu inches |
| cubic centimeters | cu meters |
| cubic centimeters | cu yards |
|  |  |


| To Convert | Into | Muftiply By |
| :---: | :---: | :---: |
| foor－pounds | ergs | $1.356 \times 10^{7}$ |
| foot－pounds | gram－calories | 0.3238 |
| foot．pounds | hp－hrs | $5.050 \times 10^{-7}$ |
| foot－pounds | joules | 1.356 |
| foot－pounds | kg－calories | $3.24 \times 10^{-4}$ |
| foot－pounds | kg－meters | 0.1383 |
| foot－pounds | kilowatt－hrs | $3.766 \times 10^{-7}$ |
| foot－pounds／min | Btu／min | $1.286 \times 10^{-3}$ |
| foot－pounds／min | foot－pounds／sec | 0.01667 |
| foot－pounds／min | horsepower | $3.030 \times 10^{-5}$ |
| foot－pounds／min | kg－calories／min | $3.24 \times 10^{-4}$ |
| foot－pounds／min | kilowatts | $2.260 \times 10^{-5}$ |
| foot－pounds／sec | Btu／hr | 4.6263 |
| foot－pounds／sec | Etu／min | 0,07717 |
| loot－pounds／sec | horsepower | $1.818 \times 10^{-3}$ |
| foot－pounds／sec | kg－calories／min | 0.01945 |
| foot－pounds／sec | kilowatts | $1.356 \times 10^{-3}$ |
| Furiongs | miles（U．S．） | 0.125 |
| furlongs | rods | 40.0 |
| furlongs | feet | 660.0 |
| G |  |  |
| galions | cu cms | 3，785．0 |
| gallons | cu feet | 0.1337 |
| gallons | cu inches | 231.0 |
| gallons | cu meters | $3.785 \times 10^{-3}$ |
| gallons | cu yards | $4.951 \times 10^{-3}$ |
| gailons | liter＇s | 3.785 |
| gailons（liq．Br． 1 mp ．） | gallans（U．S．liq．） | 1.20095 |
| gallons（U．S．） | gallons（Imp．） | 0.83267 |
| gallons of water | pounds of water | 8.3453 |
| gallons／min | cu ft／sec | $2.228 \times 10^{-3}$ |
| gallons／min | Hitars／sec | 0.06308 |
| gallons／min | $\mathrm{cu} \mathrm{ft} / \mathrm{hr}$ | 8.0208 |
| gausses | tinesisa in． | 6.452 |
| gousses | webers／sq cm | $10^{-8}$ |

Multiply By

$\boldsymbol{w}$

离㴓 $\frac{6}{6}$ c品
蕆
送炭 $\frac{4}{4}$


# gausses <br> gilberts gilberts／cm gilberts／cm gilberts／cm Gills（British） gills gills Grade Grains grains（troy） grains（troy） grains（troy） grains（troy） grains／U．S．gal grains／U．S．gal grains／Imp．gal <br> grams <br> 毚 E育 E E $\stackrel{n}{E}$ E E J E E W    复 E E Hin   



4
 ampere－hours coulombs Meter
feet centimeters kilometers meters miles（naut．） millimeters $\stackrel{\overline{\bar{E}}}{\underline{E}}$ atmospherss in．of mercury $\mathrm{kgs} / \mathrm{sq} \mathrm{cm}$
$\mathrm{kgs} / \mathrm{sq}$ meter pounds／sq ft
 $\mathrm{cm} / \mathrm{sec}$
feat $/ \mathrm{sec}$ $\mathrm{kms} / \mathrm{hr}$ meters／min miles／hr $\mathrm{cms} / \mathrm{sec}$
$\mathrm{kms} / \mathrm{hr}$ knots meters／min miles／hr miles／min $\mathrm{cms} / \mathrm{sec} / \mathrm{sec}$ meters／sec／sec miles／hr／sec per cemt grade
lumen／sq．meter き Fareday／sec离䇾萬
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$\stackrel{\square}{\Phi}$ ． $\stackrel{\Phi}{\Phi}$戠 ert water



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| 3 |
| $\vdots$ |

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|  | E 듣 $\stackrel{E}{E}$薷 \＄

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©
\＄呂 $\stackrel{y}{4}$ eet／sec


 fert／sec／sec eet／100 feel




 To Convert | gram-calories |
| :--- |
| gram-calories |
| gram-calories |
| gram-calories |
| gram-calories/sec |
| gram-centimeters |
| gram-centimeters |
| gram-centimeters |
| gram-centimeters |
| gram-centimeters |

Hand
hectares
hectares
hectograms
hectoliters
hectometers
hectowat's
henries
Hogsheads (British)
Hogsheads (U.S.)
Hogsheads (U.S.)
horsepower
horsepower
horsepower
horsepower (metric)
(542.5 tt lb/sec)
horsepower
(550 ft lb/sec)
horsepower
horsepower
horsepower
horsepower (boiler)
horsepower (boiler)
horsepower-hrs
horsepower-hrs

pounds/sq ft
pounds/sq in.
$\mathrm{kgs} / \mathrm{sq}$ meter
Btu
foot-pounds
hp-hrs
jaules
kg-merers
kilojoules
kilowatt-hrs
Btu
ergs
foot-pounds
joules
kg-calories
kilowatt-hrs
maxwells
liters
centimeters
feet
inches
meters
miles
millimeters
vards
cms/sec
feet/min
feet/sec
knots
meters/min
miles/hr
cm/sec/sec
ft/sec/sec
meters/sec/sec
miles/hr/sec
Btu/min
foot-lbs/min
foot-lbs/sec
horsepower

# kilograms/sq meter 

 kilograms/sq mm kilogram-calories kilogram-calories รа씨티-шен60!! se!̣ojes-шел6о! sa!!oles-we」6o!!y

 kilogram meters
 Starw we.f어! s.argu wefol! kilogram meters
 $\stackrel{\text { ® }}{\stackrel{\leftrightarrow}{t}}$
$\frac{5}{2}$


 kilometers




 kilometers/hr
 kilometers/hr
 kilometer $/ / h r / s e c$ kilometers/hr/sec
 kilowatts kilowatts






kitowath-hrs
knots
knots
knots
knots
knots
knots

[^2]



| To Convert | Into | Mutioly By |
| :---: | :---: | :---: |
| pounds (tray) | pennywaights (troy) | 240.0 |
| pounds (troy) | pounds (avdp.) | 0.822857 |
| pounds (troy) | tons (tong) | $3.6735 \times 10^{-4}$ |
| pounds (troyl | tons (metric) | $3.7324 \times 10^{-4}$ |
| pounds (troy) | tons (short) | $4.1143 \times 10^{-4}$ |
| pounds of water | cu feet | 0.01602 |
| pounds of water | cu inches | 27.68 |
| pounds of water | gallons | 0.1198 |
| pounds of water/min | cu ft/sec | $2.670 \times 10^{-4}$ |
| pound-feet | cm-dynas | $1.356 \times 10^{7}$ |
| pound-feet | cm-grams | 13,825. |
| pound-feet | meter-kgs | 0.1383 |
| poundsfouft | grams/cu cm | 0.01602 |
| pounds/cu ft | kgsicu meter | 16.02 |
| pounds/cu ft | pounds/cu in. | $5.787 \times 10^{-4}$ |
| pounds/cu ft | pounds/mit-foot | $5.456 \times 10^{-9}$ |
| pounds/cu in. | gms/cu cm | 27.68 |
| pounds/cu in. | kgs/cu meter | $2.768 \times 10^{4}$ |
| pounds/cu in. | poundsicu ft | 1,728. |
| pounds/cu in. | pounds/mil-foot | $9.425 \times 10^{-6}$ |
| pounds/ft | kgs/meter | 1.488 |
| pounds/in. | gms/em | 178.6 |
| pounds/mil-foot | $\mathrm{gms} / \mathrm{cu} \mathrm{cm}$ | $2.306 \times 10^{6}$ |
| pounds/sq it | atmospheres | $4.725 \times 10^{-4}$ |
| pounds/sq ft | feet of water | 0.01602 |
| pounds/sq ft | inches of mercury | 0.01414 |
| pounds/sq ft | $\mathrm{kgs} / \mathrm{sq}$ meter | 4.882 |
| pounds/sq ft | pounds/sq in. | $6.944 \times 10^{-3}$ |
| pounds/sq in. | atmospheres | 0.06804 |
| pounds/sq in. | feet of water | 2.307 |
| poundsTsq in. | inches of mercury | 2.036 |
| pounds/sq in. | kgs/sq meter | 703.1 |
| pounds/sq in. | pounds/sq ft | 144.0 |
| 0 |  |  |
| quadrants (angte) | degrees | 90.0 |
| quadrants (angle) | minutes | 5,400.0 |



| To Convert | into |
| :---: | :---: |
|  | N |
| nepers | decibels |
| Newton | Dynes |
|  | 0 |
| OHM (International) | OHM (absolute) |
| ohmes | megohms |
| ohms | microhms |
| ounces | dirams |
| ounces | grains |
| ounces | grams |
| ounces | pounds |
| ounces | ounces (troy) |
| ounces | tons (long) |
| ounces | tons imetric) |
| ounces (fluid) | cutinches |
| ounces (ffuid) | liters |
| ounces (troy) | grains |
| ounces (troy) | grams |
| ounces (troy) | ounces (avdp.) |
| ounces (troy) | pennyweights (troy) |
| ounces (troy) | pounds (troy) |
| Ounce/sq. inch ounces/sp in. | Dynes/sq. cm. pounds/sq in. |
|  | P |
| Parsec | Miles |
| Parsec | Kilometers |
| parts/million | grains/U.S. gal |
| parts/million | grains/Imp. gal |
| parts/million | pounds/million gal |
| Pecks (British) | cubic inches |
| Pecks (British) | lisers |
| Pecks (U.S.) | bushels |
| Pecks (U.S. $\}$ | cubic inches |
| Pecks (US.) | litters |



quarts (dry)
grains
ounces (troy)
grams
pounds (troy)
cu inches
cu cms.
cu feet
cu lnches
cu meters
cu yards
gallons
liters
quarts (lia.)
Erg-second
Gram/cm. sec.
ounces (troy)
dynes
grams
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joules/meter (newtons)
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| Pecks (U.S.) |
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| pennyweights (troy) |
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| pounds (troy) |
| pounds. (troy) |

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\begin{gathered}
8 \\
24.0 \\
0.05 \\
1.55517 \\
4.1667 \times 10^{-3} \\
33.60 \\
473.2 \\
0.1671 \\
28.87 \\
4.732 \times 10^{-4} \\
6.189 \times 10^{-4} \\
0.125 \\
0.4732 \\
0.5 \\
6.624 \times 10^{-27} \\
1.00 \\
14.5833 \\
13,826 . \\
14.10 \\
1.383 \times 10^{-3} \\
0.1383 \\
0.01410 \\
0.03108 \\
256 . \\
44.4823 \times 10^{4} \\
7.000 \\
453.5924 \\
0.04448 \\
4.448 \\
0.4536 \\
16.0 \\
14.5833 \\
32.17 \\
1.21528 \\
0.0005 \\
5.760 \\
373.24177 \\
13.1657 \\
12.0
\end{gathered}
$$

| To Convert | Into M | Multiply By |
| :---: | :---: | :---: |
| T |  |  |
| tempersture $i^{\circ} \mathrm{Cl}+273$ | absolute temperature $/{ }^{\circ} \mathrm{C}$ | C) 1.0 |
| temperature $\left({ }^{\circ} \mathrm{C}\right)+17.78$ | temperature ( ${ }^{\circ} \mathrm{F}$ ) | 1.8 |
| temperature ( ${ }^{\circ} \mathrm{F}$ ) $\mathbf{+ 4 6 0}$ | absolute temperature $\left({ }^{\circ} \mathrm{F}\right.$ | F) 1.0 |
| temperature ${ }^{\circ} \mathrm{F}$ )-32 | temperature $f^{\circ} \mathrm{C}$ ) | 5/9 |
| tons (lang) | kilograms | 1,016. |
| tons flong) | pounds | 2,240. |
| tons (long) | tens (short) | 1.120 |
| tons (metric) | kilograms | 1,000. |
| tons (metric) | pounds | 2,205. |
| tons (short) | kilograms | 907.1848 |
| tons (short) | ounces | 32,000. |
| tons (short) | ounces (troy) | 29.166.66 |
| tons (short) | pounds | 2,000. |
| tons (short) | pounds (troy) | 2,430.56 |
| tons (short) | tons (long) | 0.89287 |
| tons (short) | tons imetric) | 0.9078 |
| tons (short/sq ft | $\mathrm{kgs} / \mathrm{sq}$ meter | $9,765$ |
| tons of water 124 hrs | pounds of water/hr | 83.333 |
| tons of water $/ 24 \mathrm{hrs}$ | gallons/min | 0.16643 |
| tons of water/24 hrs | $\mathrm{cu} \mathrm{ft}^{\text {/ }} \mathrm{hr}$ | 1.3349 |
| $\checkmark$ |  |  |
| Voitfinch | Voit/cm. | . 39370 |
| Volt \{absolute) | Statvolts | . 003336 |
| w |  |  |
| wates | Bru/hr | 3.4129 |
| wat ts | Etu/min | 0.05688 |
| watts | ergs/sec | $10^{7}$ |
| watts | foot-lbs/min | 44.27 |




foot-lbs/sec
horsepower
horsepower (metric)
kg-calories/min
kilowatts
B.T.U. (mean)/min.
joules/sec.
Btu
ergs
foot-pounds
gram-calories
horsepowor-hrs
kilogram-calories
kilogram-meters
kilowett-hrs
Watt labsolute)
maxwells
kilolines
gausses
lines/sq in.
webers/sq cm
webers/sq meter
gausses
lines/sq in.
webers/sq cm
webers/sq in.
$\quad$ Y
centimeters
kilometers
meters
miles (naut.)
miles (stat.)
millimeters



square kilometers square kilometers
 square kilometers quare kilometers

 square meters

 5
$\frac{8}{4}$
$\frac{5}{4}$ square meters square miles square miles square miles quare miles *qu quare millimetars square millimeters
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This nomogram is used to estimate the safe range at which an object may be illuminated direcilly. It incorporates a scale for the introduction of loss factors including losses in the eye, optical surfaces external to the laser mirror, and optical losses.

FOR EXAMPLE: Assume system losses of $50 \%$, a pupil diameler ol 4 mm , a laser output of 0.05 J , and a laser beamwidth of 1 mrad . Connect loss factor and pupil size to turning scale (1). from thal point to laser output of 0.05 $J$ to turning scaie(2), then through safety threshold point to turning scale(3). and finally through laser beamwidth (4) to distance line. In this case the safe range is approximately 4.0 km or 2.6 statule miles.

NOTE: "Safe" threshold levels are a subject of some controversy and the figures specified in the nomogram should bo interpreted in the light of mosi recent information.


## LASER RADIATION MOMOGRAM

This nomogram relates laser radiation terms, which may be given as photon energy, wave number, frequency, or wavelength. Any of these terms can be converted to the others by a horizontal line across the nomogram.

FOR EXAMPLE: 1. Light at a wavelength of $0.5 \mu$ can also be described as having (1) A wavelength of 5000 $\AA_{\text {, ( (2) a }}$ a frequency of 600 THz or $6 \times 10^{14} \mathrm{~Hz}$, (3) a wavenumber of $20,000 \mathrm{~cm}^{-1}$, and (4) a photon energy of 2.48 eV .
2. Electrons when falling through 4 V will radiate at $3100 \AA$.
3. Light at 200 THz will produce conduction in semiconductors with band-gaps up to 0.83 V .


## SPECTRAL CHARACTERISTICS OF PHOTORECEPTORS AND LIGHT SOURCES

This figure shows spectral sensitivity of various photoreceptors. Response of cadrnium sulfide cells is similar to that of the human eye, but other commonly used receptors perform best at wavelenglhs invisible to the eye.


## PHOTOMETRY NOMOGRAM

This nomogram solves the light intensity equation:

$$
\text { foot-candles }=\frac{\text { candlepower }}{(\text { distance in feet })^{2}}
$$

which assumes a point source (distance greater than five times maximum lamp dimension).
Most lamps are classified according to wattage, and the following approximate relations apply:

1. The shorter the rated life of the lamp, the higher the efficiency (op/watt) and the higher the color temperature of the light.
2. For standard 120 - V inside-frosted incandescent lamps raled for $1,000 \mathrm{hr}$, the following hold true:
a. Efficiency increases with increasing wattage.
b. A $25-\mathrm{W}$ lamp is approximately 19 cp , a $60-\mathrm{W}$ lamp about 60 cp , and a $150-\mathrm{W}$ lamp is near 200 cp .
c. Color temperature increases with increasing wattage ( $150-\mathrm{W}$ lamp is near $2,900 \mathrm{~K}$ ).
d. When lamps are operated at constant voltage, light outpul falls with time, rapidly during the first 50 hrs and more slowly thereatter.
e. When lamps are operated at constant current, light output rises with time, slowly at first, then accelerating to catastrophic failure.
FOR EXAMPLE: A 6 -cp lamp will produce a light intensity of 100 fc , at a distance of 2.94 in . ( 0.245 ft ) from the lamp filament. The same lamp will provide 1 fc at 29.4 in , and 0.01 fc at 294 in .

## Several Useful Definitions

A foot-candle is the illumination produced when the light from one candle falls normally on a surface at a distance of one foot.

A /ux (commonly used in Europe) is the illumination produced when the light from one candle falls normally on a surface at a distance of one meter.

A point source emitting light uniformiy in all directions radiates $4 \pi$ lumens/candle.
A lambert is the brightness of a perfectly diffusing surface emitting or reflecting one lumen per square centimeter.

A foot lambert $1 / \pi$ candles $/ \mathrm{t}^{2}$.



SugaEsted values of illuminance

Auditorium
Lecture room-ibibrary
Classroom
Drafting room
Low-contrast work inspection
Hospital operating room
10 fo
30 fo
30 fo
30 fo
$\mathbf{2 5 0} \mathrm{fc}$
$\mathbf{5 0 0}-1,000 \mathrm{fc}$

## ILLUMINATION UNITS CONVERSION NOMOGRAM

This nomogram relates candles/square foot, footcandles, lumens/square foot, lamberts, foot-lamberts, lumens/square centimeter, candles/square centimeter, candles/square inch, end lux, and it is based on the following relationships:
foot-lamberts $=$ lumens/square foot $=$ foot-candles $=10.764$ lux
lambets $=$ lumens/square centimeter $=295.72$ candles/square toot $=929.03$ lumens/square foot
lux = fumens/square centimeter and candles/square centimeter $=3.14159$ lambert
A line from any known value through the index point intersects all other scales at corresponding values. FOR EXAMPLE:

$$
\begin{aligned}
4 \mathrm{~L} & =8.2 \mathrm{~cd} / \mathrm{in} .^{2} & =3,715 \mathrm{lM} / \mathrm{tt}^{2} \\
& =4,400 \mathrm{fc} & =1,103 \mathrm{~cd} / \mathrm{t}^{2}
\end{aligned}
$$

NOTE: the ranges can be extended by multiplying all scales by the same power of 10 .


Measurements of Sources (as Seen by Observer)
(Examples: Lamps, Stars, T.V., Lighthouse)

| Measurement | Aadiometric (Wide Band Receiver) | Photometric <br> (Eye will be the Receiver) | Where Used |
| :---: | :---: | :---: | :---: |
| Total emission | Power: watts | : Lumens | Lamps light standards |
| Emissions into a solid angle from a point source | Intensity: watts/steradian | Luminous Intensity $\text { Candela }=\frac{\text { Lumen }}{\text { Steradian }}$ | Stars |
| Emissions into a solid angle from a large source | Radiance watts/m ${ }^{2} /$ steradian | Luminance (Brighness) $\begin{aligned} & : \frac{\text { Candle }}{\mathrm{ft}^{2}}=\pi \text { foot lemberts } \\ & : \frac{\text { Candle }}{\mathrm{m}^{2}}=1 \text { nit } \\ & \frac{\text { Candle }}{\mathrm{cm}^{2}}=1 \text { stilb }=\pi \text { lamberts } \\ & \text { also: } 1 \text { foot lambert } \\ & =.0010764 \text { lamberts } \\ & =3.426 \text { nits } \end{aligned}$ | Lamps <br> T.V. Screen L.E.D. |
| Emission into all angles point source | Emittance watts/m ${ }^{2}$ | Luminous Emittance <br> : Lumen $/ \mathrm{ft}^{2}$ <br> : Lumen/m ${ }^{2}$ <br> : Lumen/cm ${ }^{2}$ | Flourescent lamps |

Measurements of Sources (as Seen by Observer)
(Examples: Lamps, Stars, T.V., Lighthouse)

| Meesurement | Radiometric <br> (Wide Band <br> Receiver) | Photometric <br> (Eye will be the Receiver) | Where Used |
| :--- | :--- | :--- | :--- |
| Total emissions <br> received | Power: watts | : Lumens | Detectors |
| Emissions per <br> unit area | Irrediance <br> W/m² | Illuminance <br> $: \frac{\text { Lumen }}{\mathrm{ft}^{2}}=$ foot candle <br> $: \frac{\text { Lumen }}{\mathrm{m}^{2}}=$ lux $=$ meter candle <br> $: \frac{\text { Lumen }}{\mathrm{cm}^{2}}=$ phot <br> also: <br> 1 foot candle $=10.764$ lux |  |

## Typical Measurements and Values

| Source | Total Emissions |  | Luminance <br> Photometric <br> Foot Lamberts | H/uminance |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Photometric Lumens | Radiometric Watts |  | Photometric Lumens/m ${ }^{2}$ | Radiometric $\mathrm{w} / \mathrm{m}^{2}$ |
| Sun (noon) <br> Lightning Flash |  |  | $\begin{aligned} & 4.7 \times 10^{8} \\ & 2 \times 10^{10} \end{aligned}$ | $10^{5}$ | . 1 |
| 100W Lamp | 1630 | 30 | $2.6 \times 10^{6}$ |  |  |
| 40W Fiourescent Lamp | 2560 | 16 | 2000 |  |  |
| Moon |  |  | 730 | . 27 |  |
| Twilight |  |  |  | 10 |  |
| Starlight (Total) |  |  |  | . 001 |  |
| (zero magnitude) |  |  |  | $2.6 \times 10^{-6}$ |  |
| (6th magnitude) |  |  |  | $10^{-8}$ |  |

## ILLUMINATION POWER CONVERSION NOMOGRAM

This nomogram relates internalional lumens, watls, and candlepower, Select the known value. A line from that point through the index point intersects other scales at corresponding values.

FOR EXAMPLE:

$$
\begin{aligned}
5 \mathrm{~lm} & =0.0074 \mathrm{~W} \\
50 \mathrm{~lm} & =3.98 \mathrm{cp}
\end{aligned}
$$

NOTE: the ranges can be extended by multiplying all scales by the same power of 10 . The nomogram is based on the following:

$$
\begin{aligned}
& 1 \mathrm{cp}=12.566 \mathrm{~lm} \\
& 1 \mathrm{~lm}=0.001496 \mathrm{~W}
\end{aligned}
$$


LUMANANCE SPECTRUM


## TABULATION OF SOUMO INTENSITY LEVELS

This tabulation extends from the barely audible to the unbearable and/or damaging sound intensity levels. The various levels are given in terms of sound pressure in dynes per square centimeter, sound intensity (at the eardrum) in watts per square centimeter, and intensity levet in decibels above $10^{-16} \mathrm{~W} / \mathrm{cm}^{2}$ and related to familiar sound situations.

FOR EXAMPLE: A faint to moderate sound such as can be found in an average residence is equal to a sound pressure of $0.024 \mathrm{dyn} / \mathrm{cm}^{2}$, which produces a sound intensity at the eardrum of $10^{-12} \mathrm{~W} / \mathrm{cm}^{2}\left(1 \mathrm{pW} / \mathrm{cm}^{2}\right)$ and is equal to an intensity level of 40 dB above $10^{-16} \mathrm{~W} / \mathrm{cm}^{2}$.

| Dexcription or Etieet | Sound Presiute devalem ${ }^{7}$ ) | Sound intensify \& Esrofrim (1W/Cm') | fontensity Leret for dbove $\left.10^{-16} \mathrm{~W} / \mathrm{cm}^{2}\right)$ | Famitar Sources of Sound inumber in parentheses shows diatance trom source) |
| :---: | :---: | :---: | :---: | :---: |
| Impars heating |  | $10^{1}$ | $150$ | jet engrne |
| Pam | 2040 | $10^{-3}$ | 140 | largest aur raid siren $\{100 \mathrm{ft}$ ) |
| Threshold of pail) |  | $10^{-1}$ | 130 | level of paniful sound |
| Thresholti ol discomiort | 204 | $10^{4}$ | 120 | pneunvath hammer ( 5 ft ) <br> arplane 1600 rpm ( 18 ft fom propeiles) <br> -autometule horn |
|  |  |  |  | engite foum of submarine (at full speed) bass tium (maximum) |
| Deafering |  | $10^{-9}$ | 110 | bohler tactory <br> loud bus horn <br> thunder clay <br> subway dexpress passing a lofal stationt |
| Discomlort begus | 20.4 | $10^{n}$ | 100 | can manutacturing plant <br> very loud musical perak : noisiesi spot al Niagera Fadls |



## ECUAL LOUDNESS CURVES OF THE AVERAGE HUMAN EAR

The curves show that the frequency response characteristic of the human ear varies with the loudness of the sound. At low sound levels the ear is relatively insensitive to the lower frequencies, which must be at least 60 dB to be heard. Higher sound levels are heard nearly equally well at the high and low frequencies. Therefore, for listening at low volume levels, the low frequencies must be boosted considerably to produce the effect of equal loudness and to avoid an apparent lack of low frequency tones. The ear is most sensitive to sounds in the 2,000 to $4,000 \mathrm{~Hz}$ range.
(20- to 29-year old subjects)


## REVERBERATION TIME

These graphs determine the optimum recommended reverberation time as a function of room volume and usage. The optimum times for speech rooms, motion picture theaters, and school auditoriums are given by a single line, whereas the optimum time for music is a broad band. Furthermore, the optimum reverberation time is not the same for all kinds of music. For example, slow organ and choral music require more reverberation than does a brilkiant allegro composition played on woodwinds or a harpischord.

The first chart is used to find the optimum reverberation time for frequencies above 512 Hz . For lower frequencies that value must be multiplied by the appropriate factor in the second graph. For small rooms the lower part of the shaded portion (closer to 1.0 should be used.)


## PHYSIOLOGICAL EFFECTS OF ELECTRIC CURRENT DN THE HUMAN BODY

The chart shows the physiological effect of various current densities on the human body. Voltage is not the prime consideration, though it takes voltage to produce the current flow. The amount of shock current depends on the body resistance between the points of contact and the skin condition, (that is, moist or dry). For example, the internal resistance between the ears is only $\mathbf{1 0 0}$ ohms (less the skin resistance), while from hand to foot it is close to 500 ohms. Skin resistance may vary from about 1,000 ohms for wet skin to over $1 / 2$ Mohm for dry skin, and is even lower for ac.

The chart shows that shock becomes more severe as current rises. At values as low as 20 mA breathing becomes labored, and as the current approaches 100 mA , ventricular fibrillation of the heart occurs. Above 200 mA , the muscuiar contractions are so severe that the heart is forcibly clamped during the shock. This clamping protects the heart from going into ventricular fibrillation and the victim's chances for survival are good if the victim is given immediate attention. Resuscitation, consisting of arificial respiration, will usually revive the victim.


This graph relates light output, current, and life of incandescent lamps with rated (design) voltage. The curves show that the light output varies directly as the applied voltage raised to the 3.4th power, while life is inversely proportional to applied voltage raised to the 121 h power.

FOR EXAMPLE: At $110 \%$ of rated voltage, the current will increase by $5 \%$, light output increases by $40 \%$, and life will be reduced to nearly $35 \%$ of that at design voltage.

At $80 \%$ of rated voltage, current decreases by $10 \%$, light output drops by more than $50 \%$, but lamp life is increased to 18 times normal.

COLOR CODES FOR ELECTRONIC COMPONENTS

|  |  |  |  | 旁 |  |  | $-\infty$ <br> 몬 |  | I |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 晨 | 晨 | 䠪 | 蕓 |  | ¢ |  |  | I |
| $\begin{aligned} & \frac{2}{6} \\ & 6 \\ & \frac{6}{2} \\ & \frac{6}{6} \end{aligned}$ |  |  |  | 䓂 |  |  | 管 | $\frac{4}{4}$ | ［ |
|  |  | 1 | $\stackrel{9}{9}$ | $\stackrel{8}{8}$ | 8 | 令 | ＋ | $\bigcirc$ | 8 |
|  | \％ivi | 8 |  | $\bigcirc$ | $\stackrel{n}{\sim}$ | N | m | $\stackrel{7}{7}$ | $\stackrel{4}{\sim}$ |
|  |  | $\bigcirc$ | $\underset{i}{p}$ | $\infty$ | $\begin{array}{\|r} \hline 8 \\ \hline 1 \\ \hline \end{array}$ | $\underset{\sim}{\mathrm{N}}$ | ¢ | $\stackrel{9}{7}$ | $\xrightarrow{8}$ |
|  |  | N | － |  |  |  | 18 |  |  |
|  |  | 2 | － | N | $\stackrel{\sim}{\sim}$ |  | $\cdots$ |  |  |
|  | 新気 | 7 | 옴 | 8 | 8 | ¢ |  |  |  |
|  | 㖪完 | $\bigcirc$ | － | N | M | $\checkmark$ | $\cdots$ | $\omega$ | N |
| 들 | ${ }^{5}$ | 1 | － | $\sim$ | 1 | I | ${ }_{6}^{69}$ | バざ | $\frac{8}{8}$ |
|  | $\frac{2}{3}$ | \％ | \％ | 9 | 0 | － | $\underline{\square}$ | $\stackrel{\square}{\square}$ | O |
|  |  | $\bigcirc$ | － | N | m | ＊ | $\sim$ | 0 | $\cdots$ |
|  | \％ig | $\begin{array}{\|c} \stackrel{8}{\sim} \\ \text { +1 } \\ \hline \end{array}$ | $1 \begin{aligned} & -1 \\ & +1 \end{aligned}$ | $\begin{gathered} N \\ i \\ \hline 1 \end{gathered}$ | $\begin{aligned} & m \\ & +1 \\ & \hline \end{aligned}$ | $\frac{\sum_{2}^{3}}{0}$ |  | $\begin{gathered} 6 \\ +1 \\ \hline \end{gathered}$ | $\stackrel{\text { N }}{\substack{4 \\ 4}}$ |
|  | 旁 | S | $\underline{9}$ | $\bigcirc$ | ¢ | $\bigcirc$ | $\bigcirc$ | \％ | $\stackrel{\square}{9}$ |
|  |  | S－ | － | $\stackrel{\square}{\square}$ | 앙 | ㅇ | O | 呂 | － |
|  | 脣这 | $\bigcirc$ | $\cdots$ | N | m | － | in | $\bigcirc$ | $n$ |
|  |  | $\left\lvert\, \begin{aligned} & x \\ & \text { 品 } \end{aligned}\right.$ | $\begin{array}{\|l\|} \hline \text { 誉 } \\ \text { 品 } \end{array}$ | 邑 |  |  | 営 | $\mid$ | $\frac{\stackrel{4}{4}}{\frac{\text { 흑 }}{2}}$ |



| $\begin{aligned} & \text { KLYSTRON } \\ & \text { WIRED } \\ & \text { LEADS } \end{aligned}$ |  | CROSSED FIELD DEVICES |  |  | STEREO PICK-UP LEADS |  |  | SEMI-CON-DUCTOR DEVICES |  | TRANSFORMERS |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  | ${ }_{\text {dot }}^{\text {diod }}$ |  |  |  |  |  |  |
| tracer | Elubent | ${ }_{\text {mignas }}$ | vtmo |  | ${ }^{3} \mathrm{~m}$, | ${ }^{4}$ mite | wire | ber | Sut. | A.F | 1-F" | Power | ${ }_{\text {center }}^{\text {Cen }}$ | colors |
| none |  | Body or other grounded elements |  |  | $\begin{array}{\|c} \text { Return } \\ \text { girid } \\ \text { gid } \end{array}$ |  | $\begin{array}{\|c\|c\|c\|c\|c\|} \hline \text { Retarn } \\ \text { gnod. } \end{array}$ | 0 | $\begin{gathered} \text { Not } \\ \text { Apot } \\ \text { cold } \end{gathered}$ |  | $\begin{aligned} & \text { Gr(d } \\ & \text { (or diode) } \\ & \text { return. } \end{aligned}$ |  |  | BLACK |
| none ${ }^{\text {a }}$ | Hester | Heaters or filament of.grnd. |  |  |  |  |  | 1 | A |  $\|$(ialue may be used it <br> petarity isn it important) |  | Filament windins \#\#2 | $\begin{array}{\|l\|l\|} \hline \text { Brown } \\ \text { and } \\ \text { adellow } \\ \text { stripepe. } \end{array}$ | Brown |
| none |  | Anode | Anode | cetay | $\underbrace{\substack{\text { night }}}_{\text {kight }}$ |  |  | 2 | 8 |  | " $\mathrm{C}^{\text {" }}$ 1 lad | H.v.plate winding | $\begin{array}{\|l\|l\|} \hline \text { Mad dand } \\ \text { and } \\ \text { stripe. } \end{array}$ | RED |
| $\begin{aligned} & \text { nane' } \\ & \text { green } \\ & \text { blue } \\ & \text { sray } \\ & \text { black } \\ & \text { white } \end{aligned}$ |  | - | - | Sole |  |  |  | 3 | c |  |  |  |  | ORANGE |
| none |  |  |  |  |  |  |  | 4 | D |  |  | $\begin{aligned} & \text { fecelfifier filament } \\ & \text { winding } \end{aligned}$ |  | YELOW |
| ${ }_{\substack{\text { nones } \\ \text { biack }}}$ | ${ }_{\text {cridid }}^{\text {Grid }}$ | - | Iniector | Grid |  |  | $\underbrace{\text { am }}_{\substack{\text { Right } \\ \text { law }}}$ | 5 | E |  |  | Fillment winding $\# 1$ | $\begin{array}{\|c\|c\|c\|c\|c\|c\|c\|c\|c\|c\|c\|c\|c\|l\|l\|l\|l\|l\|l\|l\|} \hline \text { stripe. } \end{array}$ | GREEN |
| ${ }_{\substack{\text { none } \\ \text { biack }}}$ | ginfld | - | - | $\begin{aligned} & \text { accel- } 1 \text { en } \end{aligned}$ |  | ${ }_{\substack{\text { left } \\ \text { low }}}$ | ${ }^{\text {Leth }}$ | 6 | F | Prito (finksn) leana of | Plate tead |  |  | BLUE |



EIA AND MILITARY DESIGNATIONS OF TEMPERATURE CHARACTERISTICS AND TOLERANCES FOR CERAMIC DIELECTRIC CAPACITORS

General Application and High-K Capacitors
EIA


Example: X 7 R means a max. cap. change of $\pm 15 \%$ over the temperature range of $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$.

## Military



Example: BX means a max. cap. change of $\pm 15 \%$ with no applied voitage or $-25 \%+15 \%$ with applied voltage over the ternperature range of $-55^{\circ} \mathrm{C} 10+125^{\circ} \mathrm{C}$.

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## Temperature Stable and Temperature Compensating Capacitors

## EIA



Example: characteristic $\operatorname{COC}$ is $0 \pm 30 \mathrm{pmm} /{ }^{\circ} \mathrm{C}$. For many years these capacitors were known by the trade designation NPO , which stood for Negative-Positive Zero.
Exceptions: $\$ 2 \mathrm{~L}=$ any temp. coeff. between +100 and $-750 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$
U2M $=$ any temp. coeff. between +150 and $-1500 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$
$S 3 \mathrm{~N}=$ any temp. coeff. between -1000 and $-5200 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$

## Military



Example: characteristic CG is $0 \pm 30 \mathrm{ppm} /{ }^{\circ} \mathrm{C}(\mathrm{NPO})$.
Capacitance Tolerance Codes
$\left.\begin{array}{|ccc|ccc|}\hline \begin{array}{c}\text { EIA and } \\ \text { Military }\end{array} & \text { Tolerance } & \text { Sprague } & \text { EIA and } \\ \text { Military }\end{array}\right]$

Copytight \& 1975, 5progut Electric Company, North Adamb, Mass.

Knowing the isotope half-life, its original activity at some particular time, it is an easy matter, using the chart, to determine the residual activity at some subsequent time.

FOR EXAMPLE: A sample of radioactive iodine- 131 has an activity of $10 \mu \mathrm{C}$, find the remaining strength 20 days later.

ANSWER: From an appropriate source determine the half-life of the isotope. For radioactive iodine-131, the half-life is 8.1 days.

Calculate how many "half-lives" there are corresponding to the time interval in question, that is, divide the time interval by the half-life: in this case 20/8.1 $=2.47$.

Enter this value on the horizontal axis of the chart and read the "fraction remaining" on the vertical axis as shown by the broken lines. In the case under consideration the value is 0.177 .

Multiply this value by the original activity thus giving a final value of $1.77 \mu \mathrm{C}$.


| Color |  |  | Spectral |  | Application |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Type | Fluorescence | Phosphorescence | Range $\boldsymbol{A}^{\circ}$ | Persistence |  |
| P1 | Yellow-Green | Yellow.Green | 4900-5800 | Medium | Oscillography |
| P2 | Yellow-Green | Yellow-Green | 4400-6100 | Medium | Oscillography |
| P3 | Yellow-Orange | Yellow-Orange | 5040-7000 | Medium | No longer in general use |
| P4 | White | White | 4100-6900 | Medium short | Television |
| P5 | Blue | Blue | 3500-5600 | Medium short | Photographic |
| P6 | White | White | 4160-6950 | Shorl | No longer in general use |
| P7 | White | Yellow-Green | 3900-6500 | One, medium short; One, long | Radar and osclliography |
| P10 | Dark trace: color absorption charac type of illuminatio | depends upon cteristics and on | 4000-5500 | Very long | Radar |
| P11 | Blue | Elue | 4000-5500 | Medium short | Oscillographic recording |
| P12 | Orange | Orange | 5450-6800 | Long | Hadar |
| P13 | Ped-Orange | Red-Orange |  | Medium | No longer in general use |
| P14 | Purple-Blue | Yellow-Orange | 3900-7100 | One, medium shor, One, medium | Radar |
| P15 | Green | Green | 3700-6050 | Visible, short; Ultraviolet, very short | Flying spol scanning systems; photograpnic |
| P16 | Blue-Purple and near UV | Blue.Purple and near UV | 3450-4450 | Very shont | Flying spot scanning systems: photographic |
| P17 | Yellow-White to Blue-White | Yellow | 3800-6400 | One, short; One, long | Radar |
| P18 | White | White | 3260-7040 | Medium to medium short | Television |
| P19 | Orange | Orange | 5450-6750 | Long | Radar |
| P20 | Yellow-Green | Yellow-Green | 4850-6700 | Medium to medium short | Radar |
| P21 | Red-Orange | Red-Orange | 5540-6500 | Medium | Radar |
| P 22 | Tri-color |  | 4000-7200 | Medium short | Color Television |
| P23 | White | White | 4100-7200 | Mediurn to medium short | Television |
| P24 | Green | Green | 4300-6300 | Shorl | Flying spot scanning sysiems |
| P25 | Orange | Orange | 5300.7100 | Medium | Radar |
| P26 | Orange | Orange | 5450-6650 | Very long | Radar |
| P27 | Red-Orange | Red-Orange | 5820-7200 | Medium | Color television monitor service |
| P28 | Yellow-Green | Yellow-Green | 4650-6350 | Long | Padar |
| P29 | Two-color phosp posed of a linear strips of P2 and | hor screen comarray of alternate P25 phosphors |  |  | Radar |
| P31 | Green | Green | 4150-6000 | Medium short | Oscillography |
| P32 | Purple-Blue | Yellow-Green | 3800-6550 | Long | Radar |
| P33 | Orange | Orange | 5450-6850 | Very long | Radar |
| P34 | Blue-Green | Yellow-Green | 3900-6800 | Very long | Radar and oscillography |
| P35 | Blue-White | Blue-White | 4350-6480 | Medium short | Photographic |

Important operating paramelers are listed for various crystal cuts. The impedance of a crystal is close to zero at the resonant frequency ( $f_{s}$ ) and rises to a peak at the antiresonant frequency ( $f_{g}$ ). The practical parallel resonant operating frequency ranges between $f_{s}$ and $f_{g}$ and may include these two limiting values. The operating frequency is expressed as

$$
f_{p}=f_{s} \sqrt{1+\frac{C_{1}}{C_{0}}}
$$

The steep slope of the curve and the corresponding large differential between the impedances at $f_{s}$ and $f_{\rho}$ indicale that the $Q$ of the crystal is high. Also, the frequency separation between $f_{s}$ and $f_{p}$ is determined by the capacitance ratio $C_{0} / C_{1}$. For example, the $45^{\circ}$ cut is a favorite choice in crystal filters because of its low $C_{0} / C_{1}$ ratio. Thus a larger filter bandwidth is achieved with fewer crystals.


The orientation of the better known crystal cuts shows the difference among the types.


Equivalent circuit of a crystal includes the capacitances contributed by the wire leads and the holder in $\mathrm{C}_{0}$. ratio of $C_{0}$ and $C_{1}$ indicates the frequency separation between the resonant and antiresonant frequencies of the crystal.


The impedance of a crystal is near zero at the series resonant frequency, $f$, and reaches its peak at the antiresonant frequency, $F_{A^{\prime}}$ Steep slope between these two frequencies indicates a high $Q$.


Temperature characteristics of four popular crystal cuts show the extremely stable behavior of the GT cut. Its frequency change is about 1 part per million over a $100^{\circ} \mathrm{C}$ range.

| Cut | Desigualion | Wode of wibration | Frequency range in kHz | $C_{0} / C_{1}$ | max. <br> drive <br> level | Remarks |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Duplex $5^{50 x}$ | J | Length, | $0.800 \cdot 10$ | 190-250 | 0.20 | Used in frequency and oscitlator applications. Zerotemperature coellicient occurs al appooximately toom femperature; theretore the crystal is limited to oven operation and to rigid temperaluse-control conditions. |
| $X Y$ | Cuslom. made | Lenglh, with | 3.50 | 600.900 | 0.1 | Suited for oven control applications, especially in its optimum Itequency cange. |
| NT | N | Length, | 4150 | 800-1500 | 0.1 | Preferred in low-frequency oscillatars and tillets. It operates over large temerature ranges. Stability of $\pm 5$ ppm can be oblained over $\pm 5^{\circ} \mathrm{C}$, if owencontrolled in the liequeacy range. Rugged, if properly mounted, <br> Can obtain frequency stability within $\pm 0.0025 \%$ over the normal room-lemperalure range, without tenperature conirol. |
| $+5^{\circ} \mathrm{X}$ | H | Flexure | 5-140 | 225 | 0.1 | A relatively large frequency deviativn over temperature range restricts filler applications to controlled enviconments. Low temperature coetficient and large ratio of stored mechanical enegy to electrical energy are the characteristic features. <br> Used in wideband lifters, below the range of practical size E plates, and in transistor oscillators, where LC circuits ate not stable eandigh, of where there is a space problem. <br> Disadvantages: Fabrication difficulties. The ciystal must be made in the loem of a long, thin bar to fit in a special holder, to avoid jumping between modes. |
| BT | B | Thickness | 1-75 | - | - | Thicker crystal possible al higher frequencies. Disadvantages: Too thick fow low fiequency. Also, difficelt to fabricate and has zero-temperalue coefficient over only a very small temperature ange. Not as active as the AT. |
| $-18.1 / 2^{\circ} \mathrm{X}$ | F | Extensiona | $50-250$ | 200 | - | Used principally in filters where low lemperature coefficient is sactificed tor Ireedom Irom certain spurious responses. Suitable for multi-electrodes. |
| $+5^{\circ} \mathrm{X}$ | E | Extensional | 50-250 | $130-160$ | 2.0 | Mosily applicable in low-frequency fillers, because of low $\mathrm{C}_{0} / \mathrm{C}_{\mathrm{j}}$ and good lemperature coelficient. |
| DT | 0 | Face shear | 80-500 | 450 | 2.0 | Suitable for oven ano non-oven applications. Its low capacily talio permits many useful filter applitations. Used as calibrator crystal and time base for frequenty counlers, Also used in FM and TV transmitters. <br> Disadvantage: Does not petioce well over 500 kHz . |


| Cut | Designation | Mode of vibration | Frequancy range in kHz | $C_{0} / C_{1}$ | Max. dive level | Remaks |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MT | M | Extensional | 50-250 | 250 | 2.0 | Its low temperature coefficient makes it useful for oscillater control and for filters where low $\mathrm{C}_{0} / \mathrm{C}_{1}$ ratio is required along with low inductance and good temperature coefficient. However, this crystal is seldom used, because gone conpact units have replaced it. |
| GT | G | Extensionai | 85-400 | 375 | 0.1 | Has the greatest stability yet altained within a cut. Does not vary wore than I part per million over a range of $100^{\circ} \mathrm{C}$. <br> Offers a low temperature crefficient over a wide frequency range, by coupling any desired mode with anotber of nearly equal amptilade at a frequency equal to 0.86 times ils natural trequency. <br> Used in Irequency standands asd when stability withoul temperature control or low impedance is essential. <br> Disadvantages: Most expensive of all types, because of painstaking lahor required to obtais exact orientation in dimension. |
| CT | C | Fate shear | 300-1100 | $351-400$ | 2.0 | Provides a zero temperalare coefficient in the shear mode for low frequencies. <br> Widely used in low-frepuency oscillators and filters and does not require conslant temperature control ower normal operating conditions. Useful in filters betause of lew $\mathrm{C}_{6} / \mathrm{C}_{1}$ ratio. Pgoular in oscillalors betause of its low series resistance, especially abowe 490 kHz . <br> Disadvantages: Large face dimensions make it difficult to fabricate fox the very low frequencies. |
| X | Custommade | Extensional | 350-20,000 | - | - | Mechanitally stable and an economic type of cut. Disadvantages: Large teaperature coefficient, with the lendency to jump frose one mode to another. |
| SL | Custommade | Face shear, coupled to flexure | 300-800 | 450 | - | Electrical characleristics similar to DT, but it is larger, has better Q and uniforaity of characteristics above 33 lll kHz . Its vaious characteristics make it desirable for some filter applicalions. |
| $Y$ | Y | Thickness, shear | 500-20,000 | - | - | Most active. Ratio of stored nechanical to electrical energy is large. is strong mechanically. Disadvantages: Large temperature coefficient and poor frequency spectrum. |
| AT | A | Thickness | 550-20,000 <br> fundamental <br> 10,000-60,000 <br> (3rd overtone) <br> 100,000 <br> (5th overtone) | 10-100,000 | 1.08.0 | Excellenl temperalure and frequency characteristics. Its overtones are used in cases where the Ifequency struuld nut change with escillator reactance variations. <br> Designs provide suitable capabilities for satisfying 70-A0\% ol all crystal tequirements. Preferied for high-rrequency oscillatox-cantrol wherever wide variation of temperature is encountered. Because of small size, it can be readity mounted to meet stringent vibralion specitications. <br> Disadvantage: Difficult to fabricate for optimum operation without coapling between moxjes. |

The AN nomenclature designation is assigned to:

1. Complete sets of equipment and major components of military design.
2. Groups of articles of commercial or military design which are grouped for a military purpose.
3. Major articles of military design which are not part of, or used with, a set.
4. Commercial articles where nomenclature facilitates identification and/or procedures.

As applied to complete sets, the nomenclature consists of the two letters AN followed by a slash and three indicator letters which indicate installation, type of equipment, and purpose. The number that may follow the letters indicates model number, and a subsequent letter refers to modification.

FOR EXAMPLE: AN/APN-10B airborne-radar-navigational aid 10th model-second modification
As applied to components, the AN nomenclature consists of one or two designator letters substituted for AN.
FOR EXAMPLE: An indicator model 42 for use with APQ-13 is designated as ID-42 /APQ-13. Modifications are indicated by letters, for example, ID-42B /APQ-13
Component Indicator Letters


HC-Cerystal holder
HO-Air conditioning apparatus
10-Indicating device
IL-insulator
$1 M$ - Intensity measuring device
IP-Indicator, cathode-ray tube
$J$-Junction device
$K Y$-Keying device
LC-Toal, line construction
LS-Loudspeaker
M-Mierophone
MO - Modulator
ME-Meter, portable
MK -Maintenance kit or equip ment
ML-Meterological device
MT Mounting
MX Miscellaneous
O Oscillator
OA -Operating assembly
OS-Oscilloscope, test
PO-Prime driver
PF-Fitting, pole
PG - Pigeon article
$\mathrm{PH}-$ Photographic article
PP-_Power supply
PT Plotting equipment
PU-Power equipment
R-Radio and radar receiver
AD Recorder and reproducer
RE-Relay assembly
RF-Radio frequency component
RG--Cable and transmission line, bulk r.f.

RL-Reel assembly
RP-Rope and twine
RR-Reflector
RT-Receiver and transmitter
S-Shetter
SA - Switching device
SB - Switchboard
SO-Generator, signal
SM-Simulator
SN-Synchronizer
ST--5map
$T$ - Radio and radar transmitter
TA - Telephone apparatus
TD - Timing device
TF - Transformer
TC Positioning device
TH - Telegraph apparatus
TK-Tool kit or equipment
TL-Tool
TN. Tuning unit
TS-Test equipment
TT - Teletypewriter and tac. simile apparatus
TV-Tester, tube
$U$-Connecter, audio and power
UG-Connector, r.f.
$V$-Vehicle
VS Signaling equipment, visual
WD --Cable, two conductor
WF - Cable, two conductor
WM - Cable, multiple conductor
WS-Cable, single-conductor
WT Cable, three conductor
ZM Impedance measuring device

|  | tir terier <br> Detigned incrallation Cloctat: |  | 2f better <br> Troe of Equipmontry |  | $3 d$ ferter Pufpore | Modar Na . | Madifi. cation terrer |  | Aiceellemanows Identificraion |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A | Airborne linstalled and operated in aircraft!. | A | Invisible light, heat radiatian. | A | Auxiliary assemblies inot complete operating sets used with, or part ot, two or more sets or sets seriest. | $\begin{aligned} & 1 \\ & 2 \\ & 3 \\ & 4 \end{aligned}$ | $\begin{aligned} & A \\ & B \\ & C \\ & D \end{aligned}$ | $\left.\begin{array}{l} x \\ y \\ z \end{array}\right\}$ | Changes in voltage, phase. or frequancy. Trainuing. |
| B | Underwater mobile, submarine. | B | Pigeon. | 8 | Bombing. | etc. | etc. | (v) | Variabte grouping. |
| C | Air transportable tinactivated, do not usel. | C | Carrier | C | Communications \{receiving and transmittingl. |  |  |  |  |
| 0 | Pilotless Carrier. | 0 | Radiac. | D | Direction finder, reconnaissance, andfor surveillance. |  |  |  |  |
|  |  | E | Nupac. | E | Ejection and/or release. |  |  |  |  |
| F | Fixed. | F | Plotographic. |  |  |  |  |  |  |
| G | Ground, general ground use tinclude two or more groundtype installations). | G | Telegraph or seletype. | G | Fire-control or searchlight directing. |  |  |  |  |
|  |  |  |  | H | Fecording and/ar reproducing tgraphic meteorologien! sad spund). |  |  |  |  |
|  |  | 1 | Interphone and public address. |  |  |  |  |  |  |
|  |  | J | Etectromechanical or ineftiat wise covered. |  |  |  |  |  |  |
| K | Amphibious. | K | Telemelering. | K | Comouting. |  |  |  |  |
|  |  | L | Countermessurts. | 1 | Searetalight control \||nact. vated, use Gl. |  |  |  |  |
| M | Graund, modile lingialed as operating unit in a vehiste which has no function othor than trensporting the equip. ment!. | $n$ | Mertarological. | M | Maltatenance and test assam. bties fincluding toolsh. |  |  |  |  |
|  |  | N | Sound in air, | N | Nawigational alds tincluding altimeters, buacons, compasses, racons. detith sounding, approach and landing). |  |  |  |  |
| P | Pack or portable lanimal or manl. | P | Fiadan. | F | Feproducing linactivated, do not use). |  |  |  |  |
|  |  | 0 | Sonar and underwater sound. | 0 | Special. or combination ot purposes. |  |  |  |  |
|  |  | A | Asaio. | R | Recaiving, passive detecting. |  |  |  |  |
| 5 | Wato surface craft. | 5 | Special types, magnetic, etc., or combinations of types. | S | Detecting and/or range and bearing, search. |  |  |  |  |
| T | Ground, transportable. | T | Teteplone twires. | T | Transmitting. |  |  |  |  |
| U | General urility fincludes two or more general instaliation elasses, aitborne, shipboard, and pround). |  |  |  |  |  |  |  |  |
| V | Ground, vehieular tinstalled in vehicle designed for functions other than carrying electronic equipment, etc., such as tanks]. | $v$ | Visuat and visible tight. |  |  |  |  |  |  |
| W | Water surface and under. water. | W | Armament (peculiar to arms. ment, not atherwise covered f. Facsimile or television. Date processing. | $W$ $\times$ | Automatic flight or remote control. <br> Identilication and recognition |  |  |  |  |

## MAGNETIC FIELD STRENGTH NOMOGRAM

This nomogram solves for the magnetic field strength, surrounding a power line, as a function of current in the line and the distance from it. Electronic equipment is susceptible to magnetic field interference, and this nomogram heips in determining the magnitude of the problem. For convenience the distance scale is calibraled in inches and centimeters.

FOR EXAMPLE: The magnetic field strength at a point 5 cm from a line that carries 100 A is 4.2 gauss.

## Derivation of the Field-Strength Equation

The field at point $P$ resulting from the current in segment $d l$ is given by

$$
d B=\mu_{0} \frac{1}{r^{2}} \cos \alpha d l
$$

If $d l$ is small, then

$$
\begin{aligned}
d i \cos \alpha & =r d \alpha \\
r & =R / \cos \alpha
\end{aligned}
$$

and

$$
\therefore d B=\mu_{0} \frac{1}{R} \cos \alpha d \alpha
$$

If the line is very long with respect to $R$,

$$
B=\int_{-\pi / 2}^{\pi / 2} \quad \mu_{0} \frac{1}{R} \cos \alpha d \alpha=\mu_{0} \frac{21}{R}
$$

If $B$ is in gauss, $I$ in amperes, and $R$ in centimeters, $\mu_{0}$ is equal to 0.1 .

$B * \mu_{n} \frac{2 I}{R}$
(inches) (contimeters)

INTERNATIONAL TIME MAP

This map shows the number of hours to add or subtract from Eastem Standard Time to determine the tirne anywhere on earth.


This chart is used to determine the \% change over a certain temperature range when the $\mathrm{ppm} /{ }^{\circ} \mathrm{C}$ characteristic is known or to determine the desired $\mathrm{ppm} /{ }^{\circ} \mathrm{C}$ for a maximum change over a given temperature range.

FOR EXAMPLE: 1. What will be the change in capacitance of a capacitor with a TC of 750 ppm when used over a $60^{\circ}$ temperature range? Answer: $4.5 \%$
2. What is the required stability in $\mathrm{ppm} /{ }^{\circ} \mathrm{C}$ of an oscillator that should not change in frequency by more than $1 \%$ when used between 10 to $90^{\circ} \mathrm{C}$ (i.e., temp. change $=80^{\circ} \mathrm{C}$ )? Answer: $125 \mathrm{ppm} / /^{\circ} \mathrm{C}$

(Reprinted courtesy TRW Capacitor DivIsion, Ogaliala, Nebraska.)

## Troposphere, Stratosphere and lonosphere



WIND DESIGNATIONS

Designation
Calm
Light air Light breeze Gentle breaze Moderate breeze Fresh breeze Strong breeze

Wind Speed (mph)
Less than 1
1 to 3
4 to 7
8 to 12
13 to 18
19 to 24
25 to 31

Designation
Moderate gale
Fresh gale
Strong gale
Whole gale
Storm
Hurricane

Wind Speed (mph)
32 to 38
39 to 46
47 to 54
55 to 63
64 to 72
Above 72

LIGHTNING AND THUNDERSTORM ACTIVITY FOR VARIOUS SECTIONS OF THE U.S.
Based on U.S. Weather Bureau data, this map shows the number of lightning storms occurring over a 20 -year period.


## WNDCHILL CHART

This chart shows the "windchill" and state of comfort under varying conditions of temperature and wind velocity.


WND MAP OF THE U.S.
This map shows the annual wind extremes in miles /hour, 30 feet above ground, 50 year mean recurrence interval.



THE TRIBOELECTRIC (OR ELECTROSTATIC) SERIES
The table below is so arranged that any material becomes positively charged (that is, it gives up electrons) when rubbed with any material bwer on the list. The farther apart the materials are on the list, the higher the charge will be. Surface conditions and variations in characteristics of some materials may alter some positions slightly.

|  | Positive polarity ( + ) |
| :--- | :--- |
|  | Asbestos |
| Aabbit's fur |  |
| Glass |  |
| Mica |  |
| Nylon |  |
| Wool |  |
| Cat's fur |  |
| Silk |  |
| Paper |  |
| Cotton |  |
| Wood |  |
| Lucite |  |
|  | Sealing wax |
| Amber |  |
| Polystyene |  |
| Polyethylene |  |
| Rubber balloon |  |
| Sulphur |  |
| Celluliold |  |
| Hard rubber |  |
| Vinylite |  |
| Saran wrap |  |
|  | Negative polarity ( - ) |

FOR EXAMPLE: A rubber balloon rubbed with nylon will produce a negative charge on the balloon and leave the nylon positively charged.

## CORROSION

Galvanic corrosion occurs when two dissimilar metals are in contact, in a liquid capable of carrying an electric current. Under these conditions the least noble metal (the anode) corrodes, while the more noble metal (the cathode) is not attacked.

In general, galvanic corrosion may be avoided by uniformity in the types of metals used. If uniformity is not practical, then metals should be used that are as close as possible to each other in the galvanic table, which lists metals in order of increasing nobility.

Stainless steel is "active" when chemicals present do not allow the formation of an oxide film on the surface of the metal. The treatment of stainless steel in a passivating solution accelerates the formation of the oxide film, thus making it "passive" and thereby increasing its resistance to galvanic corrosion.

Table 1. Listings of base-ta-noble metal sequence, activity teries, and gatvanic series. Base metols at the top of the list function as the anode when used with metals lower in the series imore nable), and are subject to corrosion. The activity series, with hydeogen gas as the arbitrory reference, indicate the relative ineetness of reactivity of metala. The reoctivg elements are above hydrogen while the inert olements are below. The galvanic sasies, the most used series in considering the electronics of corrosion, indicata vottoge roadings recorded between the indicoted metal and a silver/silver-chloride reference electrade white immersed in a relotively unpollutad sea-water electrolytu.


| Material and Major Aoplication Considerations | Common Avaitsble Forms | Representariva Tradionames and Suppliars |
| :---: | :---: | :---: |
| Acetals <br> Good etoctrical properties at most frequencies, which are little changed in humid environments to $125^{\circ} \mathrm{C}$. Outstanding mechanical strength, stiffness, tough. ness, and dimensiana! stability. | Extrusions, infection moldings, stock shapes. | Deitin (DuPont); Celcon (Celanesse Corp. |
| Acrylics <br> Excellent risistance to arcing and elsciricel tracking. Exceltont clarity and resistance to outdoor wiathering. | Castings, elktrutions, injection moldings, thermaformed perts, tock shapes, film, fiber, | Lucite \{OuPont); Plexiglas (Rehm and Haas Co. 1 |
| Cellulasics <br> Good elecuical properties and toughnesi, Used more tor general-purpose applications then for uitimate in shy eletrical requirement. Seversl types available. | Blow moldingt, extrusions, injection moldiags, thermoformed perts, film, fiber. stock thapes. | Tanite (Esstman Chemicat Col); <br> Ethocal-EC LDow Chemical Coli; <br> Forticel-CAP (Celanese Corp.) |
| Chlorinated Polyelhers <br> Good efectrically, but most outstanding properties ara corrosion resistance and onysicat and thermal stabilicy. | Extrusions, injectian moldings, stock shapet, film. | Penton \Herculas Powder Co. ${ }^{\text {d }}$ |
| Flyprocarbons <br> TFE: Electrically one of the mast outstanding thermoplastic materials, Very low electrical losats: very high electricil resitivity. Usetul from $=300^{\circ}$ to over $500^{\circ} \mathrm{F}$. Excellent high frequency dielectic. Has excellent combination of mechanical and electrical proparties but is relatively weak in cold llow propertes. Nearly inen chemically, as are most iluorocerbons. Very low coefficiern of friction, Nonflymmable. | Compression noldings. stock shapes, 1idrn. | Teflon TFE (OuPont); Halon TFE〔Allied Chemical Corp.\ |
| FEP: Sinnitar to TFE, expepi usalul temperature timited to about $400^{\circ} \mathrm{F}$ Egsier to mold than TFE. <br> CTFE: Excellent electrical properties and relatively good mechanical properties. Stiffer than TFE and FEP, but does have some cold flow. Uselut to about $400^{\circ} \mathrm{F}$ | Extrusions, injection moldings, Ramlinates, tilm. <br> Extrusions, ispatatic moldinģs, injection moldings. filsn. stock shapes. | Teflon FEP (Dupont) <br> Kel.F 13H Co. 1 ; Plaskon CTFE (Allied Chemical Corp. ${ }^{\text {d }}$ |
| PVF $_{2}$ One of the easiest of the fluorocarbons to process. Sitter and more resistant to cold fiow than TFE. Goed electricatly. Useful to sbout $300^{\circ} \mathrm{F}$. Maior electrical apptication is wite jacketing. | Extrusions, injection mold. ings, laminates, film. | Kynar PPennsaly Chemicals Corp. |
| Nylons <br> Convantional: Goad general-purpose electrical properies Easily processed Goocimtihancal strength and abrision resistame and tow coeffeient of friction. Commonly used types of arion are nuton 6. aylon $6 / 5$ and nylon $6 / 10$. Some have limited use in electeical applications because of moisturaabsoration properties. Nylon $6 / 10$ is best hare. | Exursions, injection moldings. isminares, rotational moldings, stock shepes, film. fiber. | Zytel iDuPont); Plagkon (Altied Chemical Co.); Bakelita Union Corbide Corp.) |
| High-Temperatup: Has excellent combingtion of thermal endurance (to $200^{\circ} \mathrm{C}$ ) and olectrical peoperties. Exhibuls relatively low dielectric constant, bigh volume reststivily, and good diefectric stengoth. Has high tensile strengith and wear fesistancs. | Fiber, sheet, tepe, peper, febric. | Nomax (OuPent) |
| Polysulfonm |  |  |
| Good combination of thermal endurance ito over $300^{\circ} \mathrm{FJ}$ and dislectric properties. Rolatively low dialectric comstant and dissipation factor, and high volume resistivity. Electrical proparties are maintained at $90 \%$ of initial values stor one vear at $300^{\circ} \mathrm{F}$. Good dimensionm stability and high ereep resistance. Flame eesistent. and good chemical resistance. | Extrusions, injection moldings, thermolormed parts, stock shappes. R Pidm, sheet. | Polysultome U Union Carbide Coro.l |



Polyathylanes, Polypropyienes, Palyallomers Exceliant electrical properties, especialiy low electrical losses. Tough and chemically resistant, but weak to varying degrees in creep and tharmat resistance. Thermal stability generally increases with density classes of polyechylene. Polypropylenes are genarally simiter to polyethylenes, but offer about $50^{\circ} \mathrm{F}$ higher hast resistance. Polyallomers are electricelly similar to polyerhylene and polypropylane but have batter stress-crack resistance and surface hardnass. Crossilinked protyethylenes provide im. prowed thermel enderance.

Polyimides and Polyamide imides
Among the highest-temperature thermoplastics ovailable, having usetul operating temperatures to about $700^{\circ} \mathrm{F}$ or higher. Excellent electrical properties. good rigidity, and excellent thermal stabitity.

Polyphenyiona Oxides (PPO
Excellent alectrical properties, especiatly lass prop. arties to above $350^{\circ} \mathrm{F}$, and over a wide froquency range. Good mechanleal strength and toughness. A lower-cost grade, Noryh, has simitiar proparties to PPO , but with a $75^{\circ}$ to $100^{\circ} \mathrm{F}$ reduction in heat resistance,

## Polysiyranas

Gurural-Putposa: Exceitent eiectrical proparties, especially loss properties. Conventional polystyrene is temperature-limited, but high-temperature modifications such as Roxalite or Polypenco crosslinked polystyrene are widely used, especially for high. frequency applicetions.
ABS: Good general electrical properties but not oulstanding for any spetific plactric epplication. Extremely tough, with high impact resistance. Can be formulated over a wide range of herdhess and toughness properties. Special gredes availabte for plated surfaces.
Vinyts
Good low cost, general-purpose tharmoplastic matesials, but electrical properties are nol outstanding. Propertias are greatly influanced by olasticizers. Many variations available, Including liexibie and rigid types. Flexible vinyla, emecially PVC, are widely used for wira ingulation.
Common Avaliable forms
Fitm coatings.

Extrusions, injection mold-
ings, thermeformed parts, ings, thermoformed parts, stock shepes. film.

Filins and tapts.

Blow moldingr, extrusions, injection molding, thermoformad parts, stock thapes, film, fiber, foam.

Films, coatings, molded and machined parts, resin: solutions.

Extrusions, injection moldings, thermoformed parts. stock thapes, film.

Blow moldings, extrusions, injection moldings, ratationgl moldings. thermoformed parts, foam.

Extrusions, injection moldIngs, themoformed parts. leminates, stock shapes, foam.

Blow moldingi, extrusions, injection maldings, cotational motdings, film.
sheet.

Representative Tradenames and Suppliers

Parylune \{Union Carbide Corp.)

Lexan (G. E. Co.); Merlon (Mohay Chemical Co.l

Mylar [DuPont); Scotchpar ${ }^{\text {(3M }}$ Coli; Calanar CColanese Corp.

Atainon Polyeahylene (DuPont): Petrothene Poivethylene fUSi Chemical Co.l: Grex H. D. Polyethylene (Allied Chemical Corp.): Hi-Fax H. D. Polyethylene, Pro. Fax Polypropytene (Hercules Pow dar Co.): Tenite Palyathylene, Polypropylens, and Polyallomer (Eastman Chemical Co.)

Vespel parts and mapes, Xapton film, and PyreM.L. resin iDu. Pontl; Al tamocol: Skyband tMonsanto Co. 1

PPO and Noryl \{G. E. Co.)

Styran (Dow Chemical Co.l: Lus. trex (Monsanto Ca.l; Rexotite (American Enka Corp.): Polypenco Q-200.5 (Polymer Corp.)

Morbon Cycolac EBorg-Warnar Corp.l; Lustran (Monsanto Co.k; Abson (Goodrich Chemical Co.)

Diamond PVC tDiannond Alkali Co.J: Plipvic \{Goodyear Chemical Co.J; Saran IDow Chernicat Co.)

THERMOSETTIAE PLASTICS FOR ELECTRICAL APPLICATIONS

| Marerial and Mojor Application Considerations | Common Available Forms | Aegreventative Tradenamas and Suppliers |
| :---: | :---: | :---: |
| Alkyds <br> Expellant dielectric strength, ore resistance, and dry insulation resistence. Low dialectric constant and dissipatian factor. Good dimensional stability. Essily molded. | Compression and transfer moldings. | Plaskon (Allied Chemical Corp.): Glaskyd (Amorican Cyanamid Co.) |
| Aminos (Mmbamint and U.4e) <br> Good peneral electrical properties. but not outthending excepi for glass-filted malamines whose hardness and arc resistance make tham useful for molded connectors. | Comprestion and transier moldings, oxtrusions. laminates. | Plaskon (Allied Chamical Corp.): Resimene (Monamic Col): Cymal melamint. Beetle uras famarican Cyanamid Co .1 |
| Dinily\| Phthelates (Allylics) <br> Unsurpassed amona thermosets in ratention of electrical properties in high-humidity onvironments. Alco, thay have among the highest volume and surface resistivities in thormosets. Low dissipation fector and heat resistance to $400^{\circ} \mathrm{F}$ or higher. Exeallont dimensional stability. Easily molded. | Compression, injection, and transfer moidings; extresions: Iaminates. | Dapon (FMC Corp.); Oibll (Allied Chamical Corp. |
| Epoxim <br> Good electricat properties, fow shrinkaga, axcellent dimassional stebllity, and good to exedilent adhesion. Easy to compound, using nonpressure pro+ cesses, for a varisty of end propertias. Useful over a wide rande of environments. | Castings; compression. injection, and transifer moldings; extrusions; laminates; matehwdie moddings: tilament windipgs foam. | Epon (Shall Chemical Col: EplRez tJorwer-Dabney Col; D.E.R. (Dow Chomical Co,\}; Araldite (Cibr Products Co.): ERL (Unlon Corbide Corp.): Scotcheast (3M Co. |
| Phenolen <br> Good gended olecirical propertios, laading to wide use for peneral-purpose molded parts. Not outstanding in any spesific electric property, but some formulations heve axcellent thermal stability above $300^{0} F$. | Castings; compression, injection, and transfer moldings; extrusions; laminates; matched-die moldings; srock shapes; form. | Bakelite (Unian Carbida Corp.l; Durez (Hooker Chemicat CoIp.) |
| Polymesters <br> Very low dissipation factor. Low-cost and extremety tasy to compound using nompressenre processes. Like epoxies, they can be formulsted for either foom temperature or mevdiod temperature use. Not equivalent to epoxies in envirommental resistance. | Compression, injection, and transter moldings: extrusions; laminates; matched die moldings: filument windings stoek shapts. | Selectran Pittshurgh Plate Gless Col) Laminac (Amarican Cyanamid Co.); Paraplex (Rohm \& Haos Co. 1 |
| Siliconet (rigid) <br> Ekcellons etectrical properties, eqpecially low dialectric constani and dissipation factor, which change litthe to $400^{\circ} \mathrm{F}$. | Castings, compression and urensior moldings. laminates. | DC Resins (Dow Corning Corp.) |

## SIGNIFICANCE OF PROPERTIES OF ELECTRICAL INSULATING MATERALS



## Significance of Vafues

The higher the value, the better the in. sulator. Dielectric strength of a materiat (per mil of thickness) usually increases considersbly with decresse in insulation thickness. Materials suppliers can provides curves of dielectric strength vs thick ness for their insulating materials.

## Resistance and Resistivity

Resistance of an insulating material, like that of a conductor, is the resistance offered by the conducting path to passage of electrical current. Resistance is expressed in ohms. Insulating materials are very poor conductors, offering high resistance. For insulating materials, the term volume resistivity is more commonly applied. Volume resistivity is the electrical resistance between opposite faces of a unit cube for a given material and at a given temperature. The relationship between resistance and resistivity is expressed by the equation $\rho=R A / /$ where $\rho=$ volume resistivity in ohro-cm, $R=$ resistance in ohms between faces; $A=$ area of the faces, and $/=$ distance between faces of the piece on which measurement is made. This is not resistance per unit volume, which would be ohm/cm ${ }^{3}$-ahihough this term is somatimes erroneously used. Other ierms are sometimes used to describe a specific application or condition. One such iterm is surface resistiyity, which is the reslstance between two opposite edges of a surface film $1 \mathbf{c m}$ square. Since the length and width of the path ore the same, the centimeter terms cancel. Thus, units of surface resistivity are aciually ohms. However, 10 avoid confusion with usual resistance values, surface resistivity is normally given In ohms/sa. Another broadly used term is insulation resistance, which, again, is a measurement of ohmic resistance for a given condition, rather than a standardized resistivity test. For both surface resistivity and insulation resistanct, standardized comparative tests are normally used. Such tasts can provide data such as effects of humidity on a given insulating matarlal conflguration.

## Dlotectric Constant

Tha dielectric constant of an insularing material is the ratio of the capa. citance of a capacitor containing that particular material to the capacitance of the same olectrode system with air replacing the insulation as the dielectric medium. The dielectric sonstant is also sometimes defined as the property of an insulation which determines the electrostatic energy stored within the solid material. The dielettric constani of most commercial insulating materials varies from about 2 to 10 , air having the value 1 .

## Power Factor and Dissipation Factor

Power factor is the ratio of the power dissipated (watts) in an insulating materlal to the product of the effective voltage and cutrent lvolt-ampece inpu:) and is a measure of the relative dielectric loss in the insulation when the system acts as eapacitor. Power factor is nondimensional and is a commonly used measure of insulation quality. it is of particular interest at high livels of frequency and power in such opolitations as microwave bquip. ment, transformers, and other inductive devices.
Dlsaipasion factor is the rangent of the dielectric loss angle. Hence, the term tan defta (tangent of the angle) is also sometimes used. For the low values ordinarily encountered in insulation, dissipation factor is practically the equivalent of power factor, and the terms are used interchangeably

## Arc Resistance

Arc resistance is a measure of an electrical breakdown condition along an insulating surface, caused by the formation of a conductive path on the surface. It is a common ASTM measurement, especialty usod with plastic materials because of the variations among plastics in the extent to which a surface breakdown occurs. Arc resistance is measured as the time, in seconds, required for breakdown along the surface of the material being measured, Surface breakdown farcing or electrical tracking along the surface) is also affected by surface cleanliness and dryness.

The migher the value, the better for a good insulating material. The resistance value for a given material depends upon a number of factors. It varies inversely with temperature, and is affected by humidity, moisture content of the test part. leval of the applied voltage, and time during which the voltage is applied. When tests are made on a piece that has been subjected to moist or humid conditions, it is important that measurements be made at controlled time intervals during or fter the test condition has been applied, since dry-out and resistence increase occur ropidly. Comparing or interpreting data is diffieult unless the test period is controlled and defined.

Low values are best for high.frequency or power applications, to minimize electrical power losses. Higher values are best for capacitance applications. For most insulating materials, dielectric constant increases with temperature, especially above a critical temperature region which is unique for ach material. Dielectric constant values are also affected fusually to a lesser degreel by fraquency. This variation is also unique for each material.

Low values are farorable, indicating a more efficient systern, with lower power losses.

The bigher the value, the better. Higher values indicate greater resistance to break. down along the surface due to arcing or tracking conditions.

To convert from Fahrenheit to Celsius＊－locate temperature（ ${ }^{\circ} \mathrm{F}$ ）in center column and read ${ }^{\circ} \mathrm{C}$ in left column． To convert from Celsius＊to Fahrenheit－locate temperature $\left({ }^{\circ} \mathrm{C}\right)$ in center column and read ${ }^{\circ} \mathrm{F}$ in right column．

| －459．4 | To | －70 | －69 Ta 0 | 7 | To | 69 | 70 |  | 839 | 140 | To | 290 | 300 | To | 000 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $c$ |  |  | $C \quad F$ | $c$ |  | $F$ | $C$ |  |  | C |  | $F$ | 6 |  | $F$ |
| －273 | －459．4 |  | $-56.1-69-92.2$ | －17．2 | 1 | 33.8 | 21.1 | 70 | 158.0 | 60.0 | 140 | 284.0 | 149 | 300 | 572 |
| －268 | －450 |  | －55．5－68－90．4 | －16．7 | 2 | 35.6 | 21.7 | 71 | 159．8 | 60.6 | 141 | 285.8 | 154 | 310 | 590 |
| －262 | －440 |  | －55．0－67－88．6 | －16．1 | 3 | 37.4 | 22.2 | 72 | 161，6 | 61.1 | 142 | 287.6 | 160 | 320 | 60 |
| －257 | －430 |  | －54．4－66－86．8 | －15．6 | 4 | 39.2 | 22.8 | 73 | 163.4 | 61.7 | 143 | 289.4 | 166 | 330 | 626 |
| －251 | －420 |  | －53．9－65－85．0 | $-15.0$ | 5 | 41.0 | 23.3 | 74 | 165.2 | 62.2 | 144 | 291.2 | 171 | 340 | 544 |
| －246 | －410 |  | －53．3－64－83．2 | －14，4 | 6 | 42.8 | 23.9 | 5 | 167.0 | 62.8 | 145 | 293.0 | 177 | 350 | 62 |
| －240 | －400 |  | $-52.8-63-81.4$ | －13．9 | 7 | 44，6 | 24.4 | 76 | 168．8 | 63.3 | 146 | 294.8 | 182 | 360 | 880 |
|  |  |  | －52．2－62－79．6 | －13．3 | 日 | 45.4 | 25.0 | 77 | 170.6 | 63.9 | 147 | 296．6 | 188 | 370 | 98 |
|  |  |  | －51．7－61－77．8 | －12．日 | 9 | $4 \mathrm{~B}, 2$ | 25.6 | 78 | 172.4 | 6 O .4 | 148 | 298． 4 | 193 | $33^{3}$ | 716 |
|  |  |  | $-51.1-60-76.0$ |  |  |  | 26.1 | 79 | 174.2 | 65.0 | 149 | 300.2 | 199 | 390 | 34 |
| －234 | －39 |  | －50．5－59－74．2 | －12．2 | 10 | 50.0 | 26.7 | 80 | 176．0 | 65.6 | 150 | 302.0 | 204 | 400 | 52 |
| －229 | －380 |  | －50．0－58－72．4 | －11．7 | 11 | 51.8 | 27.2 | 足 | 177．18 | 66.1 | 151 | 303．9 | 210 | 410 | 70 |
| －223 | －370 |  | －49．5－5．7－70．6 | － 11.1 | 12 | 53.6 | 27.8 | 82 | 179.6 | 66.7 | 152 | 105．6 | 216 | 420 | 88 |
| －218 | －360 |  | $-48.9-56-58.8$ | －10．6 | 13 | 55.4 | 28.3 | 83 | 181.4 | 67.2 | 153 | 307.4 | 221 | 430 | 806 |
| －212 | －350 |  | －48．4－55－67．0 | －10．0 | 14 | 57.2 | 28.9 | 84 | 183.2 | 67.8 | 154 | 309.2 | 227 | 440 | 824 |
| －207 | －340 |  | －47．8－54－65．2 | 9.44 | 15 | 59.0 | 29.4 | 85 | 185.0 | 68.3 | 155 | 311.0 | 232 | 450 | 42 |
| －201 | －330 |  | －47．3－53－63．4 | 8.69 | 15 | 60.8 | 30.0 | B6 | 186.3 | 68.9 | 156 | 312.9 | 238 | 450 | 60 |
| －196 | －329 |  | －46．7－52－61．6 | 8.33 | 17 | 62.6 | 30.6 | 37 | 188.6 | 69.4 | 157 | 314.6 | 243 | 470 | 78 |
| －190 | －310 |  | －46．2－51－59．8 | －7．78 | 18 | 64.4 | 31.1 | 39 | 190.4 | 70.0 | 158 | 316.4 | 249 | 480 | 996 |
| －184 | －300 |  | －45．6－50－58．0 | － 7.22 | 19 | 66.2 | 31.7 | 89 | 192.2 | 70，6 | 159 | 318.2 | 2.54 | 49 | 14 |
| －179 | － 290 |  | －45．0－49－56．2 | 6. | 20 | 68.0 | 32.2 | 90 | 194.0 | 71.1 | 160 | 320.0 | 260 | 500 | 32 |
| －173 | －280 |  | －44．4－48－54．4 | －6．11 | 21 | 69.8 | 32.8 | 91 | 195．0 | 71.7 | 161 | 321.0 | 266 | 510 | 50 |
| －169 | －279 | －4593 | －43．9－47－52．6 | 5.56 | 22 | 71.5 | 33.3 | 92 | 197.0 | 72.2 | 162 | 323.0 | 271 | 520 | 68 |
| －168 | －270 | －454 | －43．3－46－50．8 | 5.00 | 23 | 73.4 | 33.9 | 93 | 199.4 | 72.8 | 163 | 325.4 | 277 | 530 | 966 |
| －162 | －260 | －435 | － $42.8-45-49.0$ | 4.44 | 24 | 75.2 | 34.4 | 94 | 201.2 | 73.3 | 104 | 327.2 | $2 \mathrm{B2}$ | 540 | 1004 |
| －157 | －250 | －418 | －42．2－44－47．2 | － 3.89 | 25 | 77.0 | 35.0 | 95 | 203.0 | 73.9 | 165 | 329.0 | 288 | 550 | 1022 |
| －151 | －240 | －400 | $-41.7-43-45.4$ | － 3.33 | 26 | 78.8 | 35.6 | 95 | 204.8 | 74.4 | 166 | 330.8 | 293 | 560 | 1040 |
| －146 | －230 | －382 | $-41.1-42-43.6$ | 2.78 | 27 | B0．t | 36.1 | 97 | 206．6 | 5.0 | 167 | 332.6 | 299 | 570 | 058 |
| －140 | －220 | $-364$ | －40．6－41－41．8 | － 2,2 | 23 | B2．4 | 36.7 | 98 | 208.4 | 75.6 | 169 | 334.4 | 304 | 580 | 1076 |
| －134 | $-210$ | $-346$ | －40．0－40－40．0 | $-1.67$ | 29 | B4． 2 | 37.2 | 99 | 210.2 | 76.1 | 169 | 336.2 | 310 | 590 | 94 |
| －129 | －200 | －329 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| －123 |  |  | －39．4－31日－38． | ＝ | 30 | 0 | 37 | 100 | 21 | 78 | 170 | 338.0 | 316 | 0 | 2 |
| －118 | －1 | －212 | －39．8－38－39．4 | $=0.5$ | 31 | 87.8 | 73， | 109 | 213.8 | 77 | 171 | 338， | 321 | 610 | 10 |
| －112 | － 770 | －274 | －78．3－37－34．6 | ， | 32 | 89.6 | 39.9 | 102 | 215.6 | 77.8 | 172 | 341，0 | 327 | 620 | 149 |
| －107 | －1 | －256 | －37．8－36－32．8 | 0.50 | 33 | 91．4 | 39.4 | 103 | 217.4 | 75.3 | 173 | 143.4 | 332 | 630 | 166 |
| －101 | －150 | －2J8 | －37．2－36－31．0 | 1.11 | 34 | 93.7 | 40.0 | 104 | 219.2 | 70．9 | 174 | 346.2 | 399 | 640 | 1184 |
| － 86. | －140 | －220 | －36．6－34－29，2 | 1.6 | 34 | 95.0 | 40， 8 | 105 | 221.0 | 78， 4 | 175 | 347.0 | 343 | 650 | 1292 |
| － 90. | －130 |  | －36，1－33－27．4 | 2.2 | 18 | 96．］ | 41.1 | 106 | 222.1 | 60 | 176 | 348， 8 | 741 | 680 | 1220 |
| － 84 | －120 | －1 | － $38.5=32-25.6$ | 2.7 | 37 | 98.6 | 41，7 | 107 | 224．0 | 8 CD | 177 | 350，6 | 354 | 670 | 1238 |
| － 78 | 110 |  | － $36.0-31-25.8$ | 3.3 | 51 | 100.4 | 42.2 | 108 | 226.4 | 81.1 | 178 | 352．4 | 350 | 680 | 1286 |
| － 73 | 100 | －148 | －34．4－30－22．0 | 3.8 | 38 | 102.2 | 42．8 | 109 | 228.2 | 81.7 | 178 | 354，2 | 2＊${ }^{1}$ | 850 | 1274 |
| － 72 | － 99 | － 14 | － $3.3 .5 \times 28-20.2$ |  | 40 | 104.0 | 43 | 110 | 230.0 | 82 | 180 | 358.0 | 379 | 700 | 1292 |
| － 72.2 | － 88 | －144．4 | －33．3－28－18．4 | 5.0 | 41 |  | 43 | 111 | 231.8 | 82 | 181 | 357.8 | 37 | 710 | 1390 |
| － 71 | 87 | －142． | －32，8－27－16．6 | 5.5 | 42 | 107.6 | 44，4 | 112 | 233.6 | 83.3 | 182 | 359，6 | 382 | 720 | 378 |
| － 71. | －96 | －140．0 | $-32.2-26-14.8$ | 6.1 | 43 | 109.4 | 45.0 | 113 | 235.4 | 83. | 183 | 351.4 | 388 | 730 | 1346 |
| － 70 | － 8 | －139．0 | $-31,7=25=11.0$ | 5.5 | 44 | \＄11．2 | 45， | 114 | 237.2 | 84.4 | 184 | 353.2 | 303 | 740 | 1354 |
| －70， | － 94 | －137． 2 | －31．1－24－11．2 | 7.2 | 48 | 113.0 | 45.1 | 118 | 2390 | 86.0 | 185 | 365.0 | 398 | 750 | 1382 |
| － 8 白 | － 93 | －135．4 | － 30.5 － $23-9.4$ | 7.7 | 48 | 114.8 | 48，7 | 116 | 240.1 | 85.6 | 185 | 365， 3 | 404 | 750 | 1400 |
| － 88 | － 92 | － 13 | $-30,0-72-7.8$ | 8.3 | 47 | 116.6 | 47.2 | 117 | 242.6 | 88.1 | 187 | 388．6 | 410 | 770 | 1419 |
| － 68 | － 91 | $-131.8$ | $-28.8-21$－ 5.8 | 8.8 | 49 | 118.4 | 47，8 | 118 | 244，4 | 時， 7 | 1 䬶 | 370．4 | 413 | 780 | 1438 |
| －自 | －90 | －130．0 | －28．8－20－4．6 | 9.4 | 49 | 120.2 |  | 119 | 248.2 | 97.2 | 180 | 372.2 | 4 | 780 | 34 |
| － 6 | －88 | － 128.2 | $-28.3-18-2.2$ | 10.0 | 50 | 122. | 48. | 120 | 248.0 | 67 | 170 | 174．0 | 427 | 800 |  |
| － 68. | －88 | －126． | $-27,7-18=0.4$ | 10.9 | 51 | 123．6 | 49.4 | 121 | 249．8 | 88.3 | 191 | 375.8 | 437 | 810 | － |
| － 68. | － 87 | －124．6 | －27，2－17 1．4 | 11.1 | 52 | 125.6 | 60.0 | 127 | 2515 | 89.8 | 182 | 377.8 | 438 | 920 | 1509 |
| － 65. | － 86 | －122．8 | －25．5－16 3.2 | 11.7 | 13 | 127.4 | 30.6 | 123 | 257.4 | 89.4 | 193 | 379.4 | 443 | 830 | 132\％ |
| － 65. | －85 | －121．0 | －26．1－1区 $\quad 3.0$ | 12.2 | 54 | 179.2 | B1．1 | 124 | 268.2 | 00.0 | 194 | 381.2 | 449 | 840 | 1544 |
| － 64. | －84 | －119．2 | －25．5－14 6.8 | 12.8 | 55 | 131.0 | 51.7 | 125 | 257.0 | 90.8 | 195 | 383.0 | 454 | 850 | 1562 |
| －63． | －83 | －117．4 | －25．0－13 $\quad 8.6$ | 13.3 | 56 | 132.8 | 52.2 | 126 | 258.8 | 91.1 | 196 | 384.9 | 450 | 880 | 1580 |
| － 63. | －B2 | －116．6 | －24．4－12 10.4 | 13.9 | 67 | 134.6 | 52.8 | 127 | 260.6 | 91.7 | 197 | 386.6 | 960 | 870 | 1598 |
| － 62. | －B1 | － 113.8 | $\begin{array}{lll}-23.9-11 & 12.2\end{array}$ | 14.4 | 58 | 136.4 | 53.3 | 128 | 262.4 | 92.2 | 198 | 388.4 | A71 | 880 | 1616 |
| － 82. | － 80 | －112．0 | －23．3－10 14．0 | 15.0 | E9 | 138.2 | 53. | 129 | 264.2 | 92. | 199 | 390.2 | 47 | 890 | 163 |
| － 61. | － 79 | －110．2 | －22．6－9 15．8 | 15.6 | 60 | 140.0 | 51．4 | 130 | 266．0 | 93.3 | 200 | 792 | 482 | 900 | 1652 |
| －6t． | －78 | －108．4 | $\begin{array}{ll}-22.2-8 & 17.5\end{array}$ | 16.1 | 61 | 141.8 | 55.0 | 131 | 267.8 | 98.9 | 210 | 410 | 488 | 910 | 1670 |
| － 60. | －77 | － 106.6 | －21．7－7 19.4 | 16.7 | 62 | 143.6 | 55.6 | 132 | 269.6 | 100 | 212 | 413 | 493 | 920 | 698 |
| － 60.0 | －76 | －104． B | $-21.1-6 \quad 21.2$ | 17.2 | 67 | 145.4 | 56.1 | 133 | 271.4 | 104 | 220 | 428 | 499 | 930 | 1706 |
| － 59. | －75 | －103．0 | －20．6－5 23.0 | 17.8 | 64 | 147.2 | 56.7 | 134 | 273.2 | 110 | 230 | 495 | 504 | 940 | 172 |
| － 58.9 | －74 | －101．2 | －20．0－ 424.6 | 18.3 | 65 | 149.0 | 57.2 | 135 | 275.0 | 116 | 240 | 464 | 510 | 950 | 174 |
| － 58. | 4－73 | － 99.4 | －19．5－3 26.6 | 18.9 | 66 | 150.8 | 57.8 | 136 | 276.8 | 121 | 250 | 482 | 516 | 960 | 177 |
| － 57. | －72 | － 97.6 | －18．9－2 28.4 | 19.4 | 67 | 152.6 | 58.3 | 137 | 278.6 | 127 | 260 | 509 | 521 | 970 | 1778 |
| － 57. | 1－71 | －\＄5，${ }^{\text {a }}$ | －18．4－1 30.2 | 20.0 | 詚 | 154.4 | 58.9 | 138 | 280.4 | 132 | 270 | 518 | 527 | 980 | 776 |
| － 56. | － 70 | － 94.0 | －17．日 032.0 | 20.6 | 69 | 156.2 | 59.4 | 139 | 282.2 | 138 | 280 | 536 | 532 | 990 | 1814 |


| Interpolation Factors |  | Interpolation Factors |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $C$ | $F$ | $C$ | $F$ |  |  |
| 0.56 | 1 | 1.8 | 3.33 | 6 | 10.8 |
| 1.11 | $\mathbf{2}$ | 3.6 | 3.89 | 7 | 12.6 |
| 1.67 | 3 | 5.4 | 4.44 | 8 | 14.4 |
| 2.22 | 4 | 7.2 | 5.00 | 9 | 16.2 |
| 2.78 | 5 | 9.0 | 5.56 | 10 | 18.0 |

*The lerm Centigrade was officially changed to Celsius by International agreement in 1948. The Celsius scale uses the triple phase point of water, at $0^{\circ}$ Centigrade, in place of the ice point as a reference, but for all practical purposes ithe two terms are interchangeable.

| $\begin{aligned} & \text { §y } \\ & \text { S. } \end{aligned}$ | Temperature Conversion |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Cetsius | Fahrenhoir | Ketvis | Aeaumur | Rankine |
| Cels. | - | $\left(\frac{9}{5} c\right)+32$ | $C+273.96$ | $\frac{4}{5} \mathrm{C}$ | $1.8(\mathrm{C}+273.16)$ |
| Fahr. | $\frac{5}{9}(F-32)$ | - | $\left[\frac{5}{9}(F-32)\right]+273.16$ | $\frac{4}{9}(F-32)$ | F + 459.7 |
| Kelvin | K-273.16 | $\left[\frac{9}{5}(\mathrm{~K}-273.16)\right]+32$ | - | $\frac{4}{5}(\mathrm{~K}-273.16)$ | K $\times 1.8$ |
| Reau. | $\mathrm{Re} \times \frac{5}{4}$ | $\left(\frac{9}{4} \mathrm{Re}\right)+32$ | $\left(\frac{5}{4} R e\right)+273.16$ | - | $\left(\frac{9}{4} \mathrm{Re}\right)+491.7$ |
| Rank. | $\frac{\mathrm{Ra}}{1.8}-273.16$ | Ra-459.7 | $\frac{\mathrm{Ra}}{1.8}$ | $\frac{4}{9}(R a-491.7)$ | - |

Five major temperature scales are in use at present. They are: Fahrenheit, Celsius, Kelvin (Absolute), Rankine, and Reaumur. The interrelationship among the scales is shown here.

RELATIVE HUMIDITY TABLES

RELATIVE HUMIDITY TABLES

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[^3]
## TEMPERATURE-HUMIDITY INDEX

The United States Weather Bureau developed the formula for temperature-humidity index. It is based on temperature and relative humidity.

$$
\mathrm{THI}=15+0.4\left(T_{\text {diy bult }}+T_{\text {wet bulb }}\right)
$$

where temperatures are in degrees Fahrenheit. It has been determined that when the THI reaches 72, some people are uncomfortable; when it reaches 76 most everyone is uncomfortable.

Actually it is the combination of both high temperature and high humidity which causes discomfort. Lowering either one will increase comfort. On the other hand, lower temperature plus low humidity can cause discomfort on the cool side. Thus, in the wintertime, when the humidity in heated buildings is low, a higher temperature is needed for comfort than is required during other seasons when the humidity is higher.

FOR EXAMPLE: At a dry-bulb temperature of $75^{\circ} \mathrm{F}$ and a relative humidity of $60 \%$, the THI is 71 .


Commonly used terms to describe the color of heat are related to the approximate range of temperature.

| Incipient red heat | $500-550$ | Yellow heat | $1050-1150$ |
| :--- | :--- | :--- | ---: |
| Dark red heat | $650-750$ | Incipient white heat | $1250-1350$ |
| Bright red heat | $800-900$ | White heat | Above 1450 |
| Orange-red heat | $900-1000$ |  |  |

## THERMAL SPECTRUM



| AWt gat 5 Gauge | $\begin{aligned} & \text { Dian. } \\ & \text { ater in } \\ & \text { witis } \end{aligned}$ | Crozt 5atron |  | $\begin{aligned} & 0 \mathrm{HmH} \\ & 1000 \mathrm{~F} \\ & +200^{\circ} \mathrm{C} \\ & 168^{\circ} \mathrm{Ci} \end{aligned}$ | $1000 \mathrm{Ft}$ | Fi/LO | $\begin{aligned} & \text { ft/Ohm } \\ & 8 t 20^{\circ} \mathrm{C} \\ & \left.160^{\circ} \mathrm{F}\right) \end{aligned}$ | Onma/t b <br> ar $20^{\circ} \mathrm{C}$ <br> $\left(68^{\circ} \mathrm{F}\right)$ | $\begin{aligned} & 40.0 \mathrm{hm} \\ & =120^{\circ} \mathrm{C} \\ & t=68^{\circ} \mathrm{Ft} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Cincular Mis, | Squart trachers |  |  |  |  |  |  |
| 0000 | 460.0 | 211,600 | 0.1662 | 0.04901 | 640.5 | 1.561 | 20,400 | 0.00007652 | 13.070 |
| 000 | 409.6 | 167.800 | 0.1318 | 0.08180 | 507.9 | 1.968 | 16,180 | 0.0601217 | 8,219 |
| 00 | 364.8 | 133,900 | 0.1045 | 0.07793 | 4028 | 2482 | 12,830 | 0.0001935 | 5.163 |
| 0 | 324.9 | 105,500 | 0.08289 | 0.09827 | 319.5 | 3130 | 10.180 | 0.0003076 | 3.251 |
| 1 | 28.9 .3 | 83,690 | 0.06573 | 0.1239 | 253.3 | 3.947 | 8.070 | 0.0004891 | 2.044 |
| 2 | 257.6 | 66,370 | 0.05213 | 0.1563 | 200.9 | 4.977 | 6.400 | 00007778 | 1.286 |
| 3 | 229.4 | 52,640 | 0.04134 | 0.1970 | 159.3 | 6.276 | 5,075 | 0001237 | 8085 |
| 4 | 204.3 | 41,740 | 0.03278 | 0.2485 | 126.4 | 7.914 | 4,025 | 0.001966 | 508.5 |
| 5 | 181,9 | 33.100 | 0.02600 | 0.3133 | 100.7 | 9980 | 3.192 | 0003127 | 319.8 |
| 6 | 162.0 | 26.250 | 0.02082 | 0.3951 | 79.46 | 12.58 | 2,531 | 0.004972 | 201.1 |
| 7 | 1443 | 20.820 | 0.01635 | 0,4982 | 63.02 | 1587 | 2,007 | 0.007905 | 126.5 |
| 8 | 128.5 | 16.510 | 0.01297 | 0.6282 | 49.98 | 2001 | 1,592 | 0.01257 | 79.55 |
| 9 | 114.4 | 13.090 | 0.01028 | 0.7921 | 39.63 | 25.23 | 1,262 | 001999 | 50.03 |
| 10 | 101, ${ }^{\text {1 }}$ | 10,380 | 0.008155 | 0.9989 | 31.43 | 31.42 | 1,001 | 003178 | 3147 |
| 11 | 90.74 | 8,234 | 0.006467 | 1.260 | 24.92 | 40.12 | 794 | 0.05053 | 1979 |
| 12 | 80.81 | 5.530 | 0.005129 | 1.588 | 19.77 | 50.59 | 629 | 0.08035 | 12.45 |
| 13 | 71.95 | 5.178 | 0.004067 | 2.003 | 1568 | 63.80 | 499.3 | 01278 | 7827 |
| 14 | 64.08 | 4.107 | 0.003225 | 2.525 | -12.43 | 80.44 | 396.0 | 02032 | 4922 |
| 15 | 57.07 | 3,257 | 0.002558 | 3.184 | 9.858 | 101.4 | 314.0 | 03230 | 3096 |
| 16 | 50.82 | 2.583 | 0.002028 | 4.016 | 7.818 | 127 g | 249.0 | 05136 | 1947 |
| 17 | 45.26 | 2,048 | 0.001609 | 5.064 | 6200 | 161.3 | 197.5 | 0.8167 | 1224 |
| 18 | 40.30 | 1.624 | 0.001276 | 6.385 | 4917 | 2034 | 156.6 | 1299 | 07700 |
| 19 | 35.89 | 1.298 | 0.001012 | 8051 | 3899 | 256.5 | 124.2 | 2065 | 4843 |
| 20 | 31.96 | 1.022 | 0.0008023 | 10.15 | 3.092 | 3234 | 98.50 | 3.283 | 3046 |
| 21 | 28.46 | 8101 | 0.0006363 | 12.80 | 2452 | 4078 | 78.11 | 5.221 | 1915 |
| 22 | 25.35 | 642.4 | 00005046 | 16.14 | 1945 | 5142 | 61.95 | 8.301 | 1205 |
| 23 | 22.57 | 509.5 | 00004002 | 2036 | 1542 | 6484 | 49.13 | 13.20 | 07576 |
| 24 | 20.10 | 404.0 | 0.0003173 | 25.67 | 1223 | B17 7 | 38.96 | 2099 | 04765 |
| 25 | 17.90 | 120.4 | 0.0002517 | 32.37 | 0.9699 | 1.0310 | 30.90 | 33.37 | 02997 |
| 26 | 15.94 | 254. 1 | 00001996 | 40.81 | 07692 | 1.300 | 24.50 | 53.06 | 01885 |
| 27 | 14.20 | 201.5 | $0.00015 \mathrm{B3}$ | 5147 | 06100 | 1.639 | 19.43 | 84.37 | 01185 |
| 28 | 12,64 | 159.8 | 0.0001255 | 6490 | 0.4837 | 2.067 | 1541 | 1342 | 007454 |
| 29 | 1126 | 1267 | 0.00009953 | 81.83 | 0.3836 | 2.607 | 12.22 | 2133 | 004688 |
| 30 | 10.03 | 100.5 | 0.00007894 | 103.2 | 0.3042 | 3.287 | 9.691 | 3392 | 002948 |
| 31 | 8.928 | 7970 | 0.00606260 | 1301 | 02413 | 4. 145 | 7.685 | 5393 | 001854 |
| 32 | 7950 | 6321 | 0.00004964 | 1641 | 01913 | 5.227 | 6.095 | 8576 6 | 001166 |
| 33 | 7080 | 50.13 | 0.00003937 | 206.9 | 01517 | 6.594 | 4.833 | 1.364 | 0007333 |
| 34 | 6305 | 39.75 | 0.00003122 | 2609 | 01203 | 8,310 | 3.833 | 2.168 | 0004652 |
| 35 | 5615 | 31.52 | 000002476 | 329.0 | 0.09542 | 10,480 | 3.040 | 3.448 | 0002901 |
| 36 | 5000 | 2500 | 000001964 | 4148 | 003568 | 13.210 | 2.411 | 5,482 | 0001824 |
| 37 | 4.453 | 19.83 | 0.00001557 | 5231 | 0.06001 | 16.664 | 1.912 | 8.117 | 0001147 |
| 38 | 3.965 | 15.72 | 0.00001235 | 5596 | 0.04759 | 21.010 | 1.516 | 13.460 | 00007215 |
| 39 | 3.531 | 1247 | 0000009793 | 8318 | 0.03774 | 26,500 | 1.202 | 22,040 | 00004538 |
| 40 | 3.145 | 9888 | 0000007766 | 10490 | 002993 | 33.410 | 0.9534 | 35,040 | 00002854 |

Temperature coefficient of resistance: The resistance of a conductor at temperature $t$ in degrees Celsius is given by

$$
R_{1}=R_{20}\left[1+a_{20}(t-20)\right]
$$

where $R_{20}$ is the resistance at $20^{\circ} \mathrm{C}$ and $\mathrm{a}_{20}$ is the temperature coelficient of resistance at $20^{\circ} \mathrm{C}$. For copper, $\mathrm{a}_{20}$ $=0.00393$. That is, the resistance of a copper conductor increases approximately $0.4 \%$ per degree celsius rise in temperature.

| Insulation <br> Material | Breakdown <br> Votage | R. F. <br> Losses | Operating <br> Temp. fol | Weasher <br> Resistance | Flex- <br> diniry | Suggested <br> Use |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Standard PVC | High | Medium | -20 to +80 | Good | Fair | General purpose |
| Premium PVC | High | Medium | -55 to +105 | Good | Fair | General purpose |
| Polyethylene | High | Low | -60 to +80 | Good | Good | R. f. cables |
| Natural rubber | High | High | -40 to +70 | Poor | Good | Light duty |
| Neoprene | Low | High | -30 to +90 | Good | Good | Rough service |
| Waxed cotton | Low | High |  | Poor | Good | Experimenting |
| Teflon | High | Low | -70 to +260 | Good | Fair | High temperature |

## WIRE STRANDING CHART

A stranded conductor is made up of a number of smaller wire strands. This chart shows the size of each strand, when the number of strands in the finished wire size is known. Also, the number of strands for each given strand size may be determined for a finished wire gauge size.


Temperature Classifications
Definitions of Insulating Materials (IEEE)

| Clas5 | Definition |  |
| :---: | :---: | :---: |
| 0 | Materials or combinations of materials such as cotton, silk, and paper wilhout impreg. nation. Other malerials or combinations of materials may be included in this class if by experience or accepted tesis they can be shown to be capable of operation at | 90 C |
| A | Materials or combinations of materials such as cotton, silk, and paper when suitably impregnated or coated or when immersed in a dielectric liquid such as oil. Other materials or combinations of materials may be included in this class if by experience or accepted tests they can be shown to be capable of operation at | 105C |
| B | Materials or combinations of materials such as mica, glass fiber, asbestos, etc., with suitable bonding substances. Other materials or combinations of materiais, not necessarily inorgenic, may be included in this class if by experience or accepted tests they can be shown to be capable of operation at | 130 C |
| F | Materials or combinations of materials such as mica, glass fiber, asbestos, etc., with suitable bending substances. Other materials or combinations of materials, not necessarily inorganic, may be includad in this class if by experience or accepted tests they can be shown to be capable of operation at | 155C |
| H | Materials or combinations of materials such as silicone elastomer, mice, glass fiber, asbestos, etc., with suitable bonding substances suchas eppropriale silicone resins. Other materials or combinations of materials may be included in this class if by experience or accepted tests they can be shown to be capable of operation at | 180 C |
| 220C | Materials or combinations of materials which by experience or accepted tests can be shown to be capable of operation at | 220 C |
| Over <br> 220C <br> (class <br> C) | Insulation that consists entirely of mica, porcelain, glass, quartz, and similar inorganic materials. Other materials or combinations of materials may be included in this class if by experience or accepted tests they can be shown to be capable of operation at temperatures over | 220 C |

## NOTES:

1. Insulation is considered to be "impregnaled" when a suitable substance provides a bond between components of the structure and also a degree of filling and surface coverage sufficient to give adequate performance under the extremes of temperature, surface contamination (moisture, dirt, atc.), and mechanical stress expected in service. The impregnant must not flow or deteriorate enough at operating temperature so as to seriously affect performance in service.
2. The electrical and mechanical properties of the insulation must not be impaired by the prolonged application of the limiting insulation temperature permitted for the specific insulation class. The word "impaired" is here used in the sense of causing any change which could disquality the insulating material for continuously performing its intended function whether creepage spacing, mechanical suppori, or dielectric barrier action.
3. In the above definitions the words "accepted tests" are intended to refer to recognized Test Procedures established for the thermal evaluation of materials by themselves or in simple combinations. Experience or lest data, used in classifying insulating materials are distinct from the experience or test data derived for the use of materials in complete insulation systems. The thermal endurance of complete systems may be determined by Test Procedures specified by the responsible Technical Committees. A material that is classified as suitable for a given temperature may be found suitable for a different temperatura, either higher or lower, by an insulation system Test Procedure. For example, it has been found that some materials suitable for operation at one temperature in air may be suitable for a higher temperature when used in a system operated in an inert gas atmosphere.
4. It is imporiant to recognize that other characteristics, in addition to thermal endurance, such as mechanical strength, moisture resistance and corona endurance, are required in varying degrees in different applications for the successful use of insulating materials.

This nomogram can be used to determine:

1. The minimum wire size for any given load current and voltage drop;
2. the mV drop /foot for any given wire size and load current;
3. the maximum recommended* current for any given size wire.

FOR EXAMPLE: 1. With a permissible voltage drop of $5 \mathrm{mV} / \mathrm{t}_{\mathrm{r}}$ the minimum wire size in a 3-A circuit is \#12 AWG.
2. At 300 mA the voitage drop across \#22 AWG wire is $4.5 \mathrm{mV} / \mathrm{ft}$.
3. The maximum recommended current for \#18 AWG wire is 3.5 A. (This is found by connecting point A on the IR drop scale with the wire gauge scale, and reading the intersect point on the Current scale).

|  |
| :---: |

FUSING CURRENTS OF WIRES
This table gives the fusing currents in amperes for five commonly used types of wires. The current $/ \mathrm{in}$ amperes at which a wire will melt can be calculated from $l=K d^{3 / 2}$ where $d$ is the wire diameter in inches and $K$ is a constant that depends on the metal concerned. A wide variety of factors influence the rate of heat loss, and these figures must be considered approximations.


SUGGESTED AMPACITIES FOR APPLIANCE WIRING MATERIAL-ALL TYPES OF INSULATION

| Copper Temperature |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Size AWG | $\begin{array}{r} 90 \mathrm{C} \\ \text { Amper } \end{array}$ | ${ }^{105 \mathrm{C}} \mathrm{C}$ | $125 \mathrm{C}$ <br> tor | 200 C | $250 C$ |  |
| 30 | 3 | 3 | 3 | 4 | 4 | CURAENT RATING FOR DIFFERENT CONDUCTOR MATERIALS MAY BE CALCULATED BY MULTIPLYING |
| 28 | 4 | 4 | 5 | 6 | 6 |  |
| 26 | 5 | 5 | 6 | 7 | 8 |  |
| 24 | 7 | 7 | 8 | 10 | 11 | THE APPROPRIIATE COPPER CONDUCTOR RATING BY |
| 22 | 9 | 10 | 11 | 13 | 14 | THE FOLLOWING FACTORS: |
| 20 | 12 | 13 | 14 | 17 | 19 | Nickel - clad copper 0.87 |
| 18 | 25 | 20 | 22 | 26 | 29 | Nickel 0.43 |
| 16 | 27 | 28 | 30 | 36 | 38 | Note: The ultimate temperature an appliance wire reaches is |
| Correction Factors For Various Air Temperatures |  |  |  |  |  | inislors, motors elc) wilhin th |
| 30 C | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | current lowing in the wire itself. The ratings, therefore, |
| 40 | 0.91 | 0.93 | 0.95 | 0.97 | 0.98 | should only be used as a guide. In no case should the |
| 50 | 0.82 | 0.95 | 0.89 | 0.94 | 0.95 | wire be used in a manner that will cause it to exceed its |
| 60 | 0.71 | 0.77 | 0.83 | 0.91 | 0.93 | maximum lemperature rating. |
| 70 | 0.58 | 0.68 | 0.76 | 0.87 | 0.91 |  |
| 80 | 0.41 | 0.57 | 0.69 | 0.84 | 0.87 |  |
| 90 | ... | 0.44 | 0.61 | 0.80 | 0.83 |  |
| 100 | $\ldots$ | 0.25 | 0.51 | 0.77 | 0.80 |  |
| 125 | ... | . . . | ... | 0.66 | 0.69 |  |
| 150 |  | $\ldots$ | $\ldots$ | 0.54 | 0.56 |  |
| 200 | ... | . . | .. | $\ldots$ | 0.43 |  |

## AUDO LINE TABLE

This chart shows the maximum length of line that can be used between an amplifier and speaker(s) that would assure that the power loss does not exceed 15\% in low-impedance circuits, and $5 \%$ in high-impedance circuits.

When several speaker lines are brought separately to an amplifier, calculations must be made for each line independently.

FOR EXAMPLE: Four $\mathbf{1 6 - 0 h m}$ speakers are connected in parallel to the $\mathbf{4}$-ohm tap for periect impedance match. Line losses are cakulated for each line on the basis of the 16 -ohm impedance rather than the combined 4-ohm impedance.

Maximum Length of Line for 15\% Power Loss-Low Impedance Lines

| Wire Size <br> $(B$ and S) | 4 ohms | Load Impedance <br> 8 ohms | 16 ohms |
| :---: | ---: | :---: | :---: |
| 14 | 125 ft | 250 ft | 450 ft |
| 16 | 75 ft | 150 ft | 300 ft |
| 18 | 50 ft | 100 ft | 200 ft |
| 20 | 25 ft | 50 ft | 100 ft |

Maximum Length of Line for 5\%.Power Loss-High Impedance Lines

| Wire Size <br> $(B$ and $S$ | 100 ohms | Land impordance <br> 250 ohms | 500 ohms |
| :---: | :---: | :---: | :---: |
| 14 | 1000 ft | 2500 ft | 5000 ft |
| 16 | 750 ft | 1500 ft | 3000 ft |
| 18 | 400 ft | 1000 ft | 2000.5 ft |
| 20 | 250 ft | 750 ft | 1500 ft |

## SPARK-GAP BREAKDOWN VOLTAGES

The curves are for a voltage that is continuous or at a frequency low enough to permit complete deionization between cycles, between needle points, or clean, smooth, spherical surfaces (electrodes ungrounded) in dust-free clean air. Temperature is $25^{\circ} \mathrm{C}$ and pressure is 760 mm ( 29.9 in .) of mercury. Peak kilovolts shown in the graph should be multiplied by the factors given in the table for other almospheric conditions.

An approximate rule for unilorn fields at all frequencies up to at least 300 MHz is that the voltage breakdown gradient of air is 30 peak kV/cm or 75 peakkV/in. at sea level ( 760 mmof mercury) and normal temperature ( $25^{\circ}$ G). The breakdown voltage is approximately equal to pressure and inversely proportional to absolute ( ${ }^{\circ}$ Kelvin) temperature.


Spark-gap breakdown voltages.
Table of Multiplying Factors

| Pressure |  |  |  |  |  |  |  |  |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (in. | $(m m m$ |  |  |  |  |  |  |  |
| $\mathrm{Hg})$ | Hg ) | -40 | -20 | $o$ | 20 | 40 | 60 |  |
| 5 | 127 | 0.26 | 0.24 | 0.23 | 0.21 | 0.20 | 0.19 |  |
| 10 | 254 | 0.47 | 0.44 | 0.42 | 0.39 | 0.37 | 0.34 |  |
| 15 | 381 | 0.68 | 0.64 | 0.60 | 0.56 | 0.53 | 0.50 |  |
| 20 | 508 | 0.87 | 0.82 | 0.77 | 0.72 | 0.68 | 0.64 |  |
| 25 | 635 | 1.07 | 0.99 | 0.93 | 0.87 | 0.82 | 0.77 |  |
| 30 | 762 | 1.25 | 1.17 | 1.10 | 1.03 | 0.97 | 0.91 |  |
| 35 | 889 | 1.43 | 1.34 | 1.26 | 1.19 | 1.12 | 1.05 |  |
| 40 | 1016 | 1.61 | 1.53 | 1.42 | 1.33 | 1.25 | 1.17 |  |
| 45 | 1143 | 1.79 | 1.68 | 1.58 | 1.49 | 1.40 | 1.31 |  |
| 50 | 1270 | 1.96 | 1.84 | 1.73 | 1.63 | 1.53 | 1.44 |  |
| 55 | 1397 | 2.13 | 2.01 | 1.89 | 1.78 | 1.67 | 1.57 |  |
| 60 | 1524 | 2.30 | 2.17 | 2.04 | 1.92 | 1.80 | 1.69 |  |

The family trees show the various types of serial and parallel printers and how they relate.


The American Standard Code tor information Interchange (ASCil code) is used extensively in computer data transmission. The ASCII Code produced by most computer keyboards is shown here.

| BIT NUMEERS |  |  |  |  |  |  |  | ${ }^{\circ}{ }_{0}$ | $0_{1}$ | ${ }^{0}{ }_{0}$ | $0_{1}^{0}$ | ${ }^{1} 0_{0}$ | ${ }^{1} 0$ | $1_{0}$ | ${ }^{1}{ }_{1}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\xrightarrow{ }$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $\left\|\begin{array}{l} b_{7} \\ b \end{array}\right\|$ | $\left[\begin{array}{c} b_{6} \\ \vdots \end{array}\right.$ | $\begin{array}{\|c\|c} b_{5} & b_{4} \\ \vdots & b \end{array}$ | $4$ |  |  |  |  | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
|  |  | 0 | 0 | 0 |  | 0 | 0 | NUL | DLE | SP | 0 | ( ${ }^{\text {a }}$ | P | , | $p$ |
|  |  | $\bigcirc$ | 0 | 0 | - | 1 | 1 | SOH | OC1 | $!$ | 1 | A | Q | a | q |
|  |  | $\bigcirc$ | 0 | 1 |  | 0 | 2 | STX | DC2 | " | 2 | B | R | b | $r$ |
|  |  | 0 | 0 | 1 | 1 | 1 | 3 | ETX | DC3 | \# | 3 | C | S | c | s |
|  |  | 0 | 1 | 0 | 0 | 0 | 4 | EOT | DC4 | \$ | 4 | 0 | T | d | $t$ |
|  |  | 0 | 1 | 0 | 0 | 1 | 5 | ENQ | NAK | \% | 5 | E | U | e | $u$ |
|  |  | 0 | 1 | 1 |  | 0 | 6 | ACK | SYN | 8 | 6 | F | V | $\dagger$ | v |
|  |  | 0 | 1 | 1 |  | 1 | 7 | BEL | ETB | , | 7 | G | W | 9 | w |
|  |  | 1 | 0 | 0 | 0 | 0 | 8 | BS | CAN | 1 | 8 | H | X | $h$ | $\times$ |
|  |  | 1 | 0 | 0 | 0 | 1 | 9 | HT | EM | $)$ | 9 | 1 | $Y$ | $i$ | $y$ |
|  |  | 1 | $\bigcirc$ | 1 | 1 | 0 | 10 | LF | sub | - | : | $J$ | $Z$ | j | 2 |
|  |  | 1 | $\bigcirc$ | 1 | 1 | 1 | 11 | VT | ESC | + | ; | K | [ | k | 1 |
|  |  | 1 | 1 | 0 | 0 | 0 | 12 | FF | FS | 1 | $<$ | L | 1 | $\downarrow$ | 1 |
|  |  | 1 | 1 | 0 | 0 | 1 | 13 | CR | GS | - | $=$ | M | ] | m | \} |
|  |  | 1 | 1 | 1 | 1 | 0 | 14 | So | RS | - | $>$ | N | $\wedge$ | n | $\sim$ |
|  |  | $t$ | 1 | 1 | 1 | 1 | 15 | 51 | US | 1 | ? | 0 | - | 0 | DEL |


| NUL | Null, of all zeros | DC1 | Device control 1 |
| :--- | :--- | :--- | :--- |
| SOH | Star of heading | DC2 | Device control 2 |
| STX | Start of texi | DC3 | Device control 3 |
| ETX | End of text | DC4 | Device control 4 |
| EOT | End of transmission | NAK | Negative acknowledge |
| ENO | Enquiry | SYN | Synchronous idle |
| ACK | Acknowledge | ETB | End of transmission block |
| BEL | Eell, or alarm | CAN | Cancel |
| ES | Backspace | EM | End of medium |
| HT | Horizontal tabulation | SUB | Substitute |
| LF | Line feed | ESC | Escape |
| VT | Vertical tabulation | FS | Fike separator |
| FF | Forn feed | GS | Group separator |
| CA | Cariage retum | RS | Record separator |
| SO | Shit out | US | Unit separator |
| SI | Shit in | SP | Space |
| DLE | Data link escape | OEL | Delete |

## BAUDOT CODE

The Baudot Code is a 5 -bit code suitable for punched paper tape and standard teletypewriter operation. In addition to the five bits per character, each character is preceded by a start bit, which is a space, followed by a stop blt, which is a mark, approximately $11 / 2$ times longer than the regular data mark.


## GRAPHIC SYMBOLS FOR ELECTRONIC DIAGRAMS

## Semiconductors



## TRANSISTORS


pho ithasistar

multiple-amituer non transistor

non Varlington transistor

*
ngn Schotiky transistor

unajunction transistor \{UTT) with $n$-type base


00
unciunction transistor (USTFI with p-type base


00
programable unijunction tansistor (PUT). also SCR with n-type gale


## Optoelectronic Devices

FIELDEEFECT TRANSISTORS [FETS\}

three-terminal depletion-type insulated-gate (IGFET)

thres-terminal depletion-type IGFET, subsuate tued to soutce

four-termimal depletion-type IGFET

four-terminal enhancement-iype IGFET


Sive-terminat duat gate depletion-type IGFET

five-terminal dual gate enhancernent-type IGFET

diodes
light-emitting diode (LED)

photodiode

apo bidirectional photodiode fphote:duo-diode)

pnp bidirectional photodiade (pholo-duo diodol

anp two-segmem photodiode, with common cathode

psp four-quadrant phatodiode, wath common cathode


TRANSISTORS
nfan phototransisior. ho base commection

npn phototransistor, with base conncction


OPTICALLY COUPLED ISOLATORS
with photodiode output

with phototuansistor outpat, no base connection

with phototransistor output,
and base connection

with photo Darlington output, no base

with photo-Darlington output, and base

with phatodiode and ampliliertransistor output

with NAND-gate-ghotadetector output



## Contacts, Switches, and Relays



Transmission Path


Microwave Circuits


CONVERSION TABLE FOR BASIC PHYSICAL UNITS

|  | CGs-ESU | Multiply by to get cos-EMU |  | Multiply by to eet Rationalized MKS |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1. Length | Centimeter | 1 | Centimeter | $10^{-\frac{2}{2}}$ | Meter |
| 2. Mass | Gram | 1 | Gram | $10^{-3}$ | Kilogram |
| 3. Force | Dyne | 1 | Dyne | $10^{-5}$ | Newton, Dyne-five |
| 4. Energy, Work | Erg | 1 | Erg | $10^{-7}$ | Joule |
| 5. Power | Erg/second | 1 | Erg/second | $10^{-7}$ | Watt |
| 6. Electric Charge | Statcoulomb | $3.335 \times 10^{-17}$ | Abcoulomb | 10 | Coulomb |
| 7. Linear Charge Density | Statcoulomb/cm. | $3.335 \times 10^{-11}$ | Abcoulomb/cm. | $10^{4}$ | Coulomb/m. |
| 8. Surface Charge Density | Statcoulomb/ $\mathrm{cm}^{2}$ | $3.335 \times 10^{-11}$ | Abcoulomb/cm. ${ }^{2}$ | $10^{5}$ | Coulomb/m, ${ }^{2}$ |
| 9. Volumb Charge Density | Statcoulomb/ $\mathrm{cm}^{\text {a }}$. | $3.335 \times 10^{-11}$ | Abcoulomb/cm. ${ }^{3}$ | $10^{7}$ | Coulomb/m. ${ }^{\text {a }}$ |
| 10. Electric Flux | Statcoulomb | $3.335 \times 10^{-11}$ | Abcoulomb | 10 | Coulomb |
| 11. Displacement, Electric Flux Density | Statcoulomb/cm. ${ }^{\text {a }}$ | $3.335 \times 10^{-11}$ | Abcoulomb/cm. ${ }^{2}$ | $10^{5}$ | Coulomb/m. ${ }^{2}$ |
| 12. Polarization | Statcoulomb/cm. ${ }^{2}$ | $3.335 \times 10^{-11}$ | Abcoulomb/cm. ${ }^{2}$ | $10^{5}$ | Coulomb/m, ${ }^{2}$ |
| 13. Electric Dipole Moment | Statcoulomb-cm. | $3.335 \times 10^{-11}$ | Abcoulomb-cm. | $10^{-1}$ | Coulomb-m. |
| 14. Potential | Statvalt | $2.998 \times 10^{10}$ | Abvolt | $10^{-8}$ | Volt |
| 15. Electric Field Intensity | Statvolt/ $\mathrm{cm}_{\text {\% }}$ | $2.998 \times 10^{16}$ | Abvolt/cm. | $10^{-1}$ | Volt/m. |
| 16. Current | Statampers | $3.335 \times 10^{-11}$ | Abampere | 10 | Ampere |
| 17. Surface Current Density | Statampere/cm, | $3.335 \times 10^{-17}$ | Abampere/cm. | $20^{3}$ | Ampere/m. |
| 18. Volume Current Density | Statampere/cm. ${ }^{2}$ | $3.335 \times 10^{-11}$ | Abampere/cm. ${ }^{2}$ | $10^{3}$ | Ampere/m. ${ }^{2}$ |
| 19. Resistance | Statohm | $8.988 \times 10^{20}$ | Abohm | $10^{-9}$ | Ohm |
| 20. Resistivity | Statohm-cm, | $8.988 \times 10^{20}$ | Abohm-cm. | $10^{-11}$ | Ohm-m. |
| 21. Conductance | Statmho | $1.113 \times 10^{-21}$ | Abmho | $10^{4}$ | Mho |
| 22. Conductivity | Statmho/cm. | $1.113 \times 10^{-21}$ | Abmhe/cm. | $10^{11}$ | Mho/m. |
| 23. Capacity | Statfarad, Cm. | $1.113 \times 10^{-27}$ | Abfarad | $10^{9}$ | Farad |
| 24. Elastance | Statdaraf | $8.988 \times 10^{10}$ | Abdaraf | $10^{-9}$ | Daraf |
| 25. Dielectric Constant, Permittiviky | - | $1.113 \times 10^{-21}$ | - | . $7958 \times 10^{10}$ | Farad/m, |
| 26. Inductance | Stathenry | $8.988 \times 10^{20}$ | Abhenry (Centimeter) | $10^{-3}$ | Henry |
| 27. Permeability | - | $8.988 \times 10^{20}$ | Gauss/0ersted | $1.257 \times 10^{-4}$ | Henry/m. |
| 28. Reluctivity | - | $1.113 \times 10^{-21}$ | Oersted/Gauss | $10^{7}$ | - |
| 29. Magnetic Charge | - | $2.998 \times 10^{10}$ | Unit Pole | $1.257 \times 10^{-9}$ | Weber |
| 30. Magnetic Flux | - | $2.598 \times 10^{10}$ | Maxwell (Line) | $10^{-6}$ | Weber |
| 31. Magnetic Flux Density, Magnetic Induction | - | $2.998 \times 10^{10}$ | Gauss, Lines/cm ${ }^{2}$ | $10^{-4}$ | Weber/m. ${ }^{\text {P }}$ |
| 32. Magnetization | - | $2.998 \times 10^{10}$ | Pole/cm. ${ }^{2}$ | $1.277 \times 10^{-3}$ | Weber/m. ${ }^{2}$ |
| 33. Magnetic Dipole Moment | - | $2.998 \times 10^{10}$ | Pole-cm, | $1.257 \times 10^{-7}$ | Weber-m. |
| 34. Magnetic field Intensity, Magnet\|zing force | - | $3.335 \times 10^{-11}$ | Oersted (Gilberl/em.) (Gauss) | $.10^{2}$ | $\begin{gathered} \text { Praoersted } \\ \text { Ampere-turn/m. } \end{gathered}$ |
| 35. Magnetomotive Force | - | $3.335 \times 10^{-11}$ | Gilbert | $\begin{gathered} 10 \\ .7958 \\ \hline \end{gathered}$ | Pragílbert Ampere-turn |
| 36. Reluctance | - | $1.113 \times 10^{-21}$ | Gilbert/Maxwell (Oersted) | $\begin{gathered} 10^{\prime 0} \\ .7958 \times 10^{8} \\ \hline \end{gathered}$ | Pragllbert/Weber Ampere-turn/Weber |
| 37. Permeance | - | $8.988 \times 10^{20}$ | Maxwell/Gilbert | $1.257 \times 10^{-6}$ | Weber/Ampere-turn |

Practical System: /ncomplete system similar to MKS, but using centimeters and grams.
For all Systems: Temperature is in ${ }^{\circ} \mathrm{C}$. Time is in seconds.
For MKS System: Space Permittivity $8.854 \times 10^{-12} \mathrm{~F} / \mathrm{m}$. Space permeabifity $1.257 \times 10^{-5} \mathrm{H} / \mathrm{m}$.
Older or obsolete names are shown in parentheses.
To convert CGS-ESU to Rationalized MKS, multiply by both factors.

Radio-Phono


## Television


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## TORQUE-POWER-SPEED NOMOGRAM

This nomogram relates power, torque, and speed.
FOR EXAMPLE: 200 oz-in. at 500 rpm is 0.1 hp , which equals approximately 75 W . The nomogram is based on the formula:

$$
\text { Horsepower }=9.92 \times \text { torque } \times \text { speed } \times 10^{-7}
$$

where torque is in ounce-inches and speed in revolutions per minute.


Direct-Current Motors ${ }^{\text {a }}$
(Amperes at Full Load)

| $H P$ | $115 V$ | $230 V$ | $550 V$ |
| :---: | :---: | :---: | :---: |
| $1 / 2$ | 4.6 | 2.3 |  |
| $3 / 4$ | 6.6 | 3.3 | 1.4 |
| 1 | 8.6 | 4.3 | 1.8 |
|  |  |  |  |
| $1 \frac{1}{2}$ | 12.6 | 6.3 | 2.6 |
| 2 | 16.4 | 8.2 | 3.4 |
| 3 | 24 | 12 | 5.0 |
|  |  |  |  |
| 5 | 40 | 20 | 8.3 |
| $7 \frac{1}{2}$ | 58 | 29 | 12.0 |
| 10 | 76 | 38 | 16.0 |
|  |  |  |  |
| 15 | 112 | 56 | 23.0 |
| 20 | 148 | 74 | 31 |
| 25 | 184 | 92 | 38 |
|  |  |  |  |
| 30 | 220 | 110 | 46 |
| 40 | 292 | 146 | 61 |
| 50 | 360 | 180 | 75 |
|  |  |  |  |
| 60 | 430 | 215 | 90 |
| 75 | 536 | 268 | 111 |
| 100 |  | 355 | 148 |
|  |  |  |  |
| 125 |  | 443 | 184 |
| 150 |  | 534 | 220 |
| 200 |  | 712 | 295 |

Single-Phase, Alternating-Current Motors ${ }^{\text {b }}$ (Amperes at Full Load)

| $H P$ | 115 V | 230 V | 440 V |
| :---: | :---: | :---: | :---: |
| $1 / 6$ | 3.2 | 1.6 |  |
| $1 / 4$ | 4.6 | 2.3 |  |
| $1 / 2$ | 7.4 | 3.7 |  |
| $3 / 4$ | 10.2 | 5.1 |  |
| 1 | 13 | 6.5 |  |
|  |  |  |  |
| $1 \frac{1}{2}$ | 18.4 | 9.2 |  |
| 2 | 24 | 12 |  |
| 3 | 34 | 17 |  |
| 5 |  |  |  |
| $7 \frac{1}{2}$ | 80 | 28 |  |
| 10 | 100 | 50 | 21 |

For full-load currents of 208. and 200-V motors, increase corresponding $230 \cdot \mathrm{~V}$ motor full-load current by $10 \%$ and $15 \%$, respectively.
${ }^{3}$ These values for full-|oad current are average for all speeds.
bThese valubs of full-load current are for motars running at speeds usuat for belted motors and motors with normal torque characteristics. Motors built for especially low speeds or high torques may require more running current, in which case the name plate current rating should be used.

| Motor Type | Basic Characteristics | Performance Ranges | Application Areas |
| :---: | :---: | :---: | :---: |
|  | A simgie akernatine to miund-tifeld thunt. PM field plosimount atomatys. tiogar twitad - speed rela hivaringt in 3 all vell. <br>  Fasdity conliotited by frensinters of SCh's. | Output fion 16 it a tiatton of a hertepower. <br> Time constacts fle 63.5\% of ne-loud spend] to < 10 ase. <br>  <br> Whan ate matact materials, can belirth mith geth pewtis (horsejpower rincel) |  drive and contual apolications <br>  ablt for milmplackispace ast. <br>  Lervo malor |
|  | Mo commulalate mear of friction Unlimited lift. <br> Infinits etrelution. <br> Sacerm, ced-fim mation. <br>  <br> Availeth as moter alemanti \% folify houted. | Traxel ranate trpicalit la $120^{\circ}$. Torque fram a <br>  | Yery bigh-jecuracy posilioning of relocitp cantidi Dite I limilut dagle |
|  | Slow ripead, wifh ter ent. <br> Tasitiont low powion mut. <br>  <br> Tida ATmanic ringe. <br> laitet wyaber al coifs Ifot amcoth ogeration, |  Hoderate mechnical timat temalontr. Control to seconde of art. telatively teponsint. | for frect terpling to kayd. For whir medise ckeltiol Naterntitur to teand types |
|  <br>  | Similer to zwamanmant-reatact ac uniti. <br> Unam lorquet-1pers दharecteristics. <br> Sinmal neacetriat retation. <br>  <br> fast (tugeniv (<10 miter). | Ovtputs from < 1 W to tractional horsepower. Hige eflitiencies. <br>  | Computes paripherals where imodicontrol and lasi <br>  <br>  beverefik, fost alarting and ylopount |
|  | Brations and fuesed. <br> Wigh stepping rite dependual an ariver circuilry. <br> No loching teroue it rare menjisation <br> Poor inherent dampline. <br> (ow pown afficiency. <br> Can tilibit nesonence. <br> Ophratist apea lope <br> Whet dyawic nen $1:$ <br> (asily ceatrolita. <br>  | Sweral kundred to thovtrads of pps. Pomer oulpul up to a fim hundted watts. | Alfarnalive to tyachroneus motsor. <br> Uned is tontrol applications whare fory itspanu ISther than high power is ina priscipal raguirampat. <br> Intertestis well io shital cimputert. |
| sumal anclif: <br>  | Usas vertier mincipia io alve very mall steppint ingha, High tatapying tilat. <br> Hish coneing tragut with iwo inpul pow. <br> Elicioncr wivally wit iom. | Siepping ate fram <l00 pgs to nany L000's. Dependint ton driver thelionicy. Powar up to a lew hundied matta. Single stop lalit a formitliseconda. | Ufelul in numarical tonleod and otiublot application where control is dicital. <br> Frovider latt slemint and highoresolution triching. |
| INYEATER-DIIYEM AG | Oparater Itom ac, linit using a switching inwerte. <br> Sommenat was thicient than ac induction motori, oflerpist simeliar in performatca. <br> Singie-phase (capaction) or 2-phast vertions mest tommon. |  EHidencien from 70 lo 10 th in iarter madels. Sperdivg is 30,000 RMin and idifher. | Use merer ds is onty pomet assilatio. Fot priversal agplicalions wiwt ats suppliti viry widety, st in lontin applicathens. Use where brusbes mijet nef wisticiently reliable. is in wiry high jpeds or in severe envitsnmenti Yariable-trequanct wetsiment ured in acealeratiat high inerlial lates. |
|  |  <br>  <br>  <br> Lech of truytes fivet flablinty a ditticulh spofications |  <br>  <br> Sperde is 30.000 xPm . <br> EHxazacies to tot. <br> Votiges io IOC: \% Wof |  fite foficiency sud soalrol <br>  submangad. |
| 45 contiot | Bryintises. <br> 2-phise. <br> tem inamtic. <br> Squirual etite, <br>  <br> Facrapteat cerviketa fier mets $>20 \mathrm{w}$ <br>  <br>  <br> poor enviend capability |  (<1世 Io 5 ym ). <br>  <br> Time conslotit io me icis ef milisecoms. |  krew oulput pemer <br>  <br>  nolasbuty |
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| H0If: | $\begin{aligned} & \text { Yesuo } \\ & \text { ASDe } \end{aligned}$ |  <br>  | 3atin mainidican overfat copartis |


| Specific Applications | Comparisons with Other Motors | Selection and Application Factors |
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| Sopil anaperewe anfo had use in tompulec peripheals like lape Anves Mit cord benderz <br>  | Fasier reiponse than hete-fotion molors. Exctilent brush tite. Lowet slafling roltata. limeted onts br brush frittion Wuct max efficieni lhin steppor moters: | Rectimmended for fow cogring. iow starting roliadt, last response spplications. <br> Refor millt xp quictly. <br> Thermellirinsients and hart remotil car be imporlatil factori. <br> Lerte, ithozmormance anits can be aperime. <br>  4Wful |
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|  <br>  bil. |  <br>  Lest suitable for contros inat other \&ctypes. <br> Yery rong life with progerty defitnt』 inverter. | Impecter can bas sepasite of pachased with malox. <br> Hish fine-tifevit spolks. <br> [mil generation, wilh bulky fitter capacitics itquired for aupplession. <br> SCR inyerters prefected in hithur power uses, but transigise inveriars art tisier ta switch and more tolisible. <br> Power-supply capacitofa san im requirtd and muas wilhazand aupNo transients. |
|  <br> Sulable for pumgs when flyie in the aution does not sugoiferentry Setacte camation. <br>  |  costers. <br>  <br>  byes <br>  |  Woth peal tine tritants <br>  <br>  <br>  <br>  |
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|  <br>  trinimum speed modulation <br> U未iof in precision gyrodrives | Somewhat iess elficifnt than salient-pote synchrongus mathines of cilber weund-fiold of PM tonstruction. <br> Less huating than other types of synchranous inalals <br> Simpler than phas!-\|bth drives | Hish elficitancies important let compultr apaliczations <br> Low power istors lead to high inpul curreali. <br> Hither powte facters available in ling le: phase capacilm uestions. <br> Senblive to ingul harmonces. <br> Can meteleale high-inalia leads <br>  |
|  <br>  proportioced |  |  |

FAMILY TREE OF ELECTRIC MOTORS

Device
Average Rating (Watts)
Air Cleaner50
Air Conditioner (roorn) ..... 1,500
Blender ..... 390
Broiler ..... 1,450
Carving Knife ..... 100
Clock ..... 2
Clothes Dryer ..... 4,850
Coffee Maker ..... 900
Deep Fryer ..... 1,450
Dehumidifier ..... 250
Dishwasher ..... 1,200
Electric Blanket ..... 175
Fan:
attic ..... 370
turnace ..... 290
window ..... 200
Floor Polisher ..... 300
Freezer:
( $14 \mathrm{cu} . \mathrm{ft}$ ) ..... 340
(frostless - $15 \mathrm{cu} . \mathrm{It}$ ) ..... 440
Frying Pan ..... 1,200
Heater (portable) ..... 1,320
Heating Pad ..... 65
Hot Plate ..... 1,250
Humidífier ..... 175
Iron (Hand) ..... 1,000
Microwave Oven ..... 1,450
Mixer ..... 125
Oil Burner (stoker) ..... 265
Fadio ..... 70
Radio /Record Player ..... 100
Range with oven ..... 12,200
Refrigerator:
( $12 \mathrm{cu} . \mathrm{It}$ ) ..... 300
(frostless, $12 \mathrm{cu} . \mathrm{ft}$ ) ..... 390
Pefrigerator /Freezer: ( $14 \mathrm{cu} . \mathrm{fl}$ ) ..... 352
(frostless, $14 \mathrm{cu} . \mathrm{ft}$ ) ..... 600
Roaster ..... 1,300
Sandwich Grill ..... 1,150
Sewing Machine ..... 75
Television:
black and white:
tube type ..... 160
solid state ..... 55
color TV:
lube type ..... 300
solld state ..... 200
Toaster ..... 1,150
Trash Compaclor ..... 400
Vacuum Cleaner ..... 630
Watfle Iron ..... 1,100
Washing Machine: automatic ..... 500
nonautomatic ..... 280
Waste Disposer ..... 440
Water Heater: standard ..... 2,475
quick recovery ..... 4,475
Water Pump ..... 460

## NOMOGRAM RELATING AMPLITUDE, FREQUENLY, AND ACCELERATION OF A BODY WITH SIMPLE HARMONIC MOTION

This nomogram is based on the formula

$$
g=0.10225(d)(f)^{2}
$$

where
$g=$ acceleration in g-units
$f=$ frequency of vibration in cps
$d=$ amplitude of vibration (peak displacement each side of resting point) in inches
FOR EXAMPLE: A vibrating body with a displacement of 0.01 in . each side of center at 200 Hz , has an acceleration of 40 g 's.

NOTE: To find the acceleratlon in a rotating body resulting from centrifugal force, substitute radius of rotation for amplitude ( $d$ ), and revolutions per second for vibrations per second ( $f$ ), $g=32 \mathrm{H} / \mathrm{sec} / \mathrm{sec}$ in the MKS system of units.


This nomogram relates deceleration ( $G$ load), stopping distance, and drop height as an aid to designers and engineers who must deal with problems of shock caused by violent or sudden deceleration.

The equation used to plot the nomograph is $\log G=\log g+\log H-\log D$. Relating deceleration ( $G$ load), stopping distance, and drop height, it is based on the following relationships:

$$
\begin{aligned}
H & =g t^{2} / 2 \\
D & =G T^{\prime 2} / 2 \\
V_{t} & =g t \\
V_{i} & =G t^{\prime \prime}
\end{aligned}
$$

where:
$H=$ free-fall distance
$g=$ acceleration due to free fall
$t=$ free-fall time
$D=$ stopping or deflection distance
$G=G$ load due to impact shock
$t^{\prime}=$ deceleration time
$V=$ temminal velocity due to free fall at instant of impact
$V_{1}=$ Initlal deceleration velocity at instant of impact
Since at the moment of impact the terminal velocity $\left(V_{r}\right)$ caused by acceleration is equal to the initial velocity $\left(V_{i}\right)$, it follows that:

$$
g t=G t^{\prime}
$$

Combining the equations:

$$
H / D=\frac{g t^{2} / 2}{G t^{\prime} 2 / 2}=g t(t) / G t^{\prime}\left(t^{\prime}\right)
$$

Since $g t=G t^{\prime} H / D=t / t^{\prime}$. Also, since $G / g=t / t^{\prime}, H / D=G / g$. Transposing, $G=g(H / D)$ or $\log G=\log$ $g+\log H-\log D$. This equation is based on a constant or uniformly decelerating force. For linear deceleration the equation for load distance relationship is: $G=2 g H / D$.

Neither formula Includes the stopping distance as part of the distance traveled because its effect is negligible for small values of stopping distance (D).

FOR EXAMPLE: 1. Find the G load on a shock-mounted case that endures a 30 -in. drop height with a maximum mount deflection of 0.4 in . Assume a rigid case and unilorm deceleration in the mount.

ANSWER: Intersect impact shock $(G)$ scale with a line connecting the $30-\mathrm{in}$. drop height with 0.4 in . on the absorber deflection scale. Read answer off impact shock scele. In this example, it is $73 G$.
2. Find the impact shock on a piece of equipment that is dropped 20 in . on expanded rubber foam gasket. The foam is compressed a total of 0.1 in . and is assumed to have a linear deceleration characteristic.

ANSWER: Intersect the impact shock ( $G$ ) scale with a line connecting the $20-\mathrm{in}$. drop height with 0.1 in. on the absorber deflection scale. Since peak impact shock $(G)$ load due to linear deceleration is approximately twice as severe as that due to uniform deceleration, the value of 200 G obtained is multiplied by 2 for linear deflection. Answer is 400 G .


For a given power dissipation and air density, this nomogram solves for the air flow (cubic feet per minute) that is required to keep the temperature rise of an equipment at a specified value. At sea level ( 760 mm Hg ) , $0^{\circ} \mathrm{C}$, and an air density of $0.079 \mathrm{lb} / \mathrm{t}^{3}$, the temperature rise is approximately equal to $3,000 \mathrm{P} / \mathrm{Q}$, where $P$ is power dissipation in kilowatts and $Q$ is the air flow in cubic feet per minute.

To use the nomogram first determine the ambient temperature and altitude at which the equipment must operate and note from the graph the applicable air density for these conditions. On the nomogram align the permissible temperature rise with the equipment's power dissipation and note the intersect point on the turning scale. Align this point with the applicable air densily and read required air flow in cubic feet per minute on scale $B$.

FOR EXAMPLE: To operate an equipment wilh a power consumption of 500 W at sea level, an ambient temperature of $20^{\circ} \mathrm{C}$, and a permissible heat rise of $15^{\circ} \mathrm{C}$, requires an air flow of $50 \mathrm{ft}^{3} / \mathrm{min}$.


METALLIC ELEMENTS

\begin{tabular}{|c|c|c|c|c|c|c|}
\hline Name and Symbol \& Color \& Atomic Weight \& Specific Gravity or Density \& Specific Heat \& Meltingpoint ( \({ }^{\circ}\) Celsius) \& Coefficient of Linear Expansion \\
\hline Aluminmm . \(\quad\) N \& Timxnme \& 271 \& \({ }^{267}\) \& 0.2140 \& \({ }^{55}\) \& 0.0000231 \\
\hline  \&  \& 1202
750 \& \({ }_{5}^{671.685}\) \& \({ }^{0.00518}\) \& \({ }_{400}\) \& 0.00000105
0.00055 \\
\hline  \& Penemprory \& 1394 \& 3.8 \& O.08 \& Cso \& \\
\hline  \&  \& 80 \& \(\square^{192}\) \& 0.8820 \& 238 \& T00014 \\
\hline  \&  \&  \& 8.540-.607 \& -0.568 \& 590 \& -0,00027 \\
\hline Cotum \& anvermule \& 13, 12. \& 1.978 \&  \& 27 \& \(\overline{0} 000080\) \\
\hline Crapum \& Yerow \& \({ }^{140.2}\) \& \(7{ }^{1}\) \& - 01700 \& 100 \& - \\
\hline Critomum \({ }_{\text {cosan }}\) \& \& \({ }_{36} 80\) \&  \& 0.120
0.1078 \& 9,7,900 \& \(\bigcirc\) \\
\hline \(\cdots\) \& Crenshimhlt \& \& \& \& \& \\
\hline coseor as \& Fees \& 330 \& 492485 \& Q0082 \& 1.100 \& 0.0000185 \\
\hline  \& = \& 11680 \& = \& - \& \(=\) \& - \\
\hline Gatium \& Bumbumus \& \({ }_{695} 9\) \& 89 \& 90x \& 20 \& \\
\hline  \& Baynumit \& 127
1972 \& 939 \& 0074
00384 \& 1.006 \& \({ }^{0} 00000167\) \\
\hline Indum Mr \& Yhie \& 11188 \& 1722 \& 0 0570 \& \({ }_{2} 175\) \& 00000417 \\
\hline \({ }_{\text {lnom }}^{\text {mosem }}\) \& Sieet mete \& \begin{tabular}{l}
188 \\
\hline 59
\end{tabular} \& 2238
7 \& 0038
01140 \& 2, 2.550 \& \({ }^{0} 000000061{ }^{0}\) \\
\hline Cansorum - - - \& Gemy \& 1390

797 \&  \& ${ }^{0 \times 49}$ \& ${ }_{3}^{188}$ \& -000027 <br>
\hline  \& Resingrit \& ${ }_{702}$ \&  \& ${ }^{0 \times 314}$ \& ${ }_{100}^{328}$ \& 0000027 <br>
\hline  \& Sixemit \& 243
590 \& 1780 \& ${ }^{0} 02500$ \& - 6122 \& 0 0000ees <br>
\hline  \& Rlodestry \& 2000 \& 13 194 \& (1200 \& -40 \& -00008ta <br>
\hline  \& Serememat \& 960 \& ${ }^{86}$ \& 0.072 \& 2,450 \& - <br>
\hline Nosemernum \& - \& 307 \& 8.9 \& -raso \& 1,430 \& 0.000017 <br>
\hline Notaum no \& Slowigy \& 935
1909 \& $\begin{array}{r}121 \\ 22.3 \\ \hline\end{array}$ \& 0071 \& (1.850 \& -000000s <br>
\hline  \& Bush-mis \& 190\% \& 214 \& ${ }_{0}^{000510}$ \& i.s. \& ${ }^{0} 000000017$ <br>
\hline  \& - \& 1982 \& 215 \& 0.0024 \& 1,780 \& -0.0000060 <br>
\hline  \& Sinememisa \& 1405 \& ${ }_{83}$ \& $\underline{0} 1500$ \& 900 \& ${ }^{0} 0.000081$ <br>
\hline  \&  \& 225.9 \& 121 \& \& 2,000 \& 0.0000085 <br>
\hline fluburume \&  \& 95.5 \& 15 \& 0.0.800 \& ${ }^{2} \mathbf{3} 8.5$ \& $\square 000085$ <br>
\hline  \& 二 \& ${ }_{10}^{1017}$ \& 12281
7.7 \& ${ }_{0}^{0.0811}$ \& - \& $0.0 \times 0005$ <br>
\hline $\mathrm{Sa}_{\text {Scmanmm }}$ \& $\square$ \& 4.1 \& \& \& \& <br>
\hline Sinori...... $\mathrm{AO}_{0}$ \& Shireme \& ${ }_{207.9}$ \& ${ }_{\substack{104.10 .57 \\ 0.06}}$ \& 0.8000 \& ${ }_{98}^{962}$ \& ${ }^{0.00001192}$ <br>
\hline Stimmmen \& Stinemion \& \% 87.8 \& 258 \& 0.720 \& +00 \& - <br>
\hline  \& Eluch \& ¢ \& 160
825 \& 00365
0049 \& 2.910
462 \& 0.0000078 <br>
\hline Torsum \& こ \& +180 \& -18 \& \& \& $\bigcirc$ <br>
\hline  \&  \& ${ }^{2050}$ \& 118 \& 0.035
0.9776 \& 1.6998 \& 0.0000602 <br>
\hline Thwilumm ${ }_{\text {Tin }}^{\text {min }}$ \& Wrat \& 1190 \& $12 \times 3$ \& -0,350 \& 232 \& n <br>
\hline Thursom - \& Datay \& 481 \& 38 \& ${ }_{013}$ \& ${ }_{1,000}^{2}$ \& 0.000083 <br>
\hline  \&  \& 1640
2085 \& 19173
1830 \& 0, 0338 \& 3.000 \& <br>
\hline Venetwimm \& Minmor \& 51.1 \& 58 \& 0.128 \& 1,000 \& <br>
\hline Yowem. \& \& 890 \& 3s0 \& - \& \& <br>
\hline  \& Bunsume \& ${ }_{\text {cos }} \mathbf{5 6}$ \& 719 \& 0.0835 \& ${ }^{419}$ \& 0.000684 <br>
\hline
\end{tabular}

(Reprinted from Master Handbook of Electronic Tables \& Formulas by Marlin Cliftord, courlesy TAB BOOKS, Inc.)

## DENSITIES OF SOLIDS AND LIQUIDS IN CUBIC CENTIMETERS AND CUBIC FEET



## SOLDER ALLOYS

The term solder alloys covers a broad range of materials with greatest emphasis placed on compositions of tin and lead. The tin lead system of alloys has a general solidus temperature of $361^{\circ} \mathrm{F}$. The eutectic composition, the alloy with a single sharp melting point and no plastic range, is $63 \%$ tin, $37 \%$ lead. This alloy is in widest use in the electronic industry.

The specific tin lead alloy selected is determined by the nature of the joining operation and the degree to which a plastic or "mushy" solder state can be tolerated or is desirable. Tin lead alloys with a tin content from $20 \%$ up through and including $97.5 \%$ have the same $361^{\circ} \mathrm{F}$ solidus line. Alloys containing lower percentages of tin have an increased solidus temperature. This is also true of tin antimony, tin silver, and lead silver alloys. The higher solidus line permits operation of the soldered part in higher ambient temperatures. It also permits sequential or piggy-back soldering. Where two soldering connections are to be made in areas very close to each other, the first joint can be made with one of the high-temperature alloys. When the second joint is made with an alloy in the normal tin lead system, the first joint will not be disturbed.

|  |  |  |  | Temperature at which Soldar Becomes Piastic |  | Temperature of which Solder Becemes Liquid |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Percent Tin | percent bued | Percent Shluar | Percent Antimeny | ${ }^{\circ} \mathrm{C}$ | ${ }^{0} \boldsymbol{F}$ | ${ }^{\circ} \mathrm{C}$ | ${ }^{9} \mathrm{~F}$ |
| 0 | 100 |  |  |  |  | 327. | 621 |
| 5 | 95 |  |  | 300 | 572 | 315 | 509 |
| 10 | 90 |  |  | 287.6 | 514 | 300 | 572 |
| 15 | 85 |  |  | 223 | 433 | 200 | 554 |
| 20 | 60 |  |  | 189 | 361 | 280 | 538 |
| 25 | 75 |  |  | 183 | 319 | 287 | 613 |
| 30 | 70 |  |  | 183. | 361 | 255 | 491 |
| 35 | 65 |  |  | 183 | 361 | 245 | 473 |
| 40 | 60 |  |  | 183 | 361 | 235 | 455 |
| 45 | 55 |  |  | 183 | 361 | 223 | 433 |
| 50 | 50 |  |  | 183 | 361 | 212 | 414 |
| 55 | 45 |  |  | 183 | 361 | 200 | 392 |
| 80 | 40 |  |  | 183 | 361 | 189 | 372 |
| 83 | 37 |  |  | eutectio | alloy ${ }^{4}$ | ${ }^{186}$ | 381 |
| 65 | 35 |  |  | 183 | 361 | 188 | 367 |
| 70 | 30 |  |  | 183 | 361 | 191 | 378 |
| 75 | 25 |  |  | 183 | 361 | 195 | 393 |
| 80 | 20 |  |  | 183 | 361 | 201 | 384 |
| 45 | 15 |  |  | 183 | 361 | 207 | 404 |
| 90 | 10 |  |  | 189 | 361 | 214 | 417 |
| 85 | 8 |  |  | 183 | 381 | 222 | 432 |
| 97,5 | 2.5 |  |  | 183 | 361 | 227 | 441 |
| 100 | 0 |  |  |  |  | 232 | 450 |
| 35 | 63 |  | 2 | 187 | 369 | 237 | 488 |
| 20 | 78.7 | 1.3 |  | 181 | 358 | 276 | 529 |
| 27 | 70 | 3 |  | 178 | 352 | 253 | 487 |
|  | 98 | 5 |  | 305 | 581 | 380 | 680 |

"A eutectic alloy is thet eompesitifen of two or more matale that has one sharp melting point and ne plagtic range.

The two graphs are used to determine the current-carrying capacity and sizes of etched copper conductors (tracks) for various temperature rises above ambient. To use the charts, enter the top chart from the left at the current value which is anticipated, to the point where it inlerrupts the applicable copper temperature-rise curve. Then, proceed vertically down to the second chart to the appropriate weight (the weight of one square foot of copper of a given thickness) slanted line, and proceed left to determine the minimum track width.

FOR EXAMPLE: To carry 10 amperes and not exceed a $20^{\circ} \mathrm{C}$ rise above ambient requires a 0.100 -inch wide conduct of 2-ounce copper track.

*Eased on $1 / 16$ inch boards. For thicker boards, derate by $15 \%$.

A consistent set of physical values has been adapted by the National Bureau of Standards. The values presented below are at least as accurate as any others available, and have the advantage of being self-consistent, thus preventing the necessity of having to make a choice between different answers derived in different ways.

## Fundamental Constants

Compiled by E. R. Cohen and B. N. Taylor under the auspices of the CODATA Task Group on Fundamental Constants. This set has been otficially adopted by CODATA and is taken from J. Phys. Chem. Ref. Data, Vol. 2, No. 4, p. 663 (1973) and CODATA Butletin No. 11 (December 1973).

| Quantity | Symboi | Numerical value * U | Uncert. (ppms) | $51+$ | $\stackrel{\text { Units }}{ } \rightarrow$ cre ; |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Speed of light in vacuum | c | 299792458(1.2) | 0.004 | $\mathrm{m} \cdot \mathrm{s}^{-1}$ | $10^{2} \mathrm{~cm} \cdot \mathrm{~s}^{-1}$ |
| Permeability of vacuum | $\mu_{0}$ | $\begin{aligned} & 4 \pi \\ & =12.5663706144 \end{aligned}$ |  | $\begin{aligned} & 10^{-9} \mathrm{H} \cdot \mathrm{~m}^{-1} \\ & 10^{-1} \mathrm{H} \cdot \mathrm{~m}^{-1} \end{aligned}$ |  |
| Permittivity of vacuum, $1 / \mu_{0} c^{2}$ | ${ }^{6}$ | 8.854187818 (71) | 0.008 | $10^{-11} \mathrm{~F} \cdot \mathrm{~m}^{-1}$ |  |
| Fine-structure constant, $\left[\mu_{0} c^{2 / 4} / 4\right]$ ( $e^{7 \hbar c)}$ | $\mathrm{a}^{\text {a }}$ | $\begin{gathered} 7.2973506(60) \\ 137.03604(11) \end{gathered}$ | $\begin{aligned} & 0.82 \\ & 0.82 \end{aligned}$ | $10^{-2}$ | $10^{-3}$ |
| Elementary charge | e | $\begin{aligned} & 1.6021892(46) \\ & 4.803242(14) \end{aligned}$ | $\begin{aligned} & 2.9 \\ & 2.9 \end{aligned}$ | ${ }^{10^{-19}} \mathrm{C}$ | $\begin{aligned} & 10^{-14} \text { ormu } \\ & 10^{-11} \text { esu } \end{aligned}$ |
| Planck constant | $\begin{aligned} & h \\ & \pi=h / 2 \pi \end{aligned}$ | $\begin{aligned} & 6.626176(36) \\ & 1.0545887(57) \end{aligned}$ | $\begin{aligned} & 5.4 \\ & 5.4 \end{aligned}$ | $\begin{aligned} & 10^{-24} \mathrm{~J} \cdot \mathrm{~s} \\ & 10^{-34} \mathrm{~J} \cdot \mathrm{~s} \end{aligned}$ | $\begin{aligned} & 1 \sigma^{-27} \text { erg's } \\ & 10^{-11} \text { erges } \end{aligned}$ |
| Avogadro constant | $\mathrm{N}_{\text {A }}$ | 6.022045 (31) | 5.1 | $10^{19} \mathrm{~mol}^{-1}$ | $10^{13} \mathrm{~mol}^{-3}$ |
| Atomic mass unit. $10^{-3} \mathrm{~kg} \cdot \mathrm{~mol}^{-1} \mathrm{~N}_{\mathrm{A}}{ }^{-1}$ | $u$ | 1.6605555(86) | 5.1 | $10^{-31} \mathrm{~kg}$ | $10^{-14} \mathrm{~g}$ |
| Electron rest mass | $m_{e}$ | $\begin{aligned} & 9.109534(47) \\ & 5.4858026(21) \end{aligned}$ | $\begin{aligned} & 5.1 \\ & 0.38 \end{aligned}$ | $\begin{aligned} & 10^{-31} \mathrm{~kg} \\ & 10^{-4} \mathrm{u} \end{aligned}$ | $\begin{aligned} & 10^{-14} \mathrm{~g} \\ & 10^{-4} \mathrm{u} \end{aligned}$ |
| Proton rest mass | $\pi_{r}$ | $\begin{aligned} & 1.6726485(86) \\ & 1.007276470(11) \end{aligned}$ | 5.2 | $10.15 \mathrm{~kg}$ | $\mathrm{u}^{10^{-14} \mathrm{E}}$ |
| Ratio of proton mass to electron mass | $m_{\mathrm{n}} / \mathrm{m}_{e}$ | 1836.15152(70) | 0.38 |  |  |
| Neutron rest mass | $\mathrm{ma}^{\prime}$ | $\begin{aligned} & 1.6749543(86) \\ & 1.008665012(37) \end{aligned}$ | $\begin{aligned} & 5.1 \\ & 0.037 \end{aligned}$ | $\begin{aligned} & 10^{-11} \mathrm{~kg} \\ & \mathrm{u} \end{aligned}$ | $\begin{aligned} & 10^{-14} \mathrm{E} \\ & \mathrm{O}^{2} \end{aligned}$ |
| Electron charge to mass ratio | $\mathrm{e} / \mathrm{m}_{6}$ | $\begin{aligned} & 1.7588047(49) \\ & 5.272764(15) \end{aligned}$ | $\begin{aligned} & 2.8 \\ & 2.8 \end{aligned}$ | $10^{11} \mathrm{Cl}^{\text {kg }}{ }^{-1}$ | $\begin{aligned} & 10^{\prime} \text { emu-g } g^{\prime} \\ & 10^{11} \text { osu- } \varepsilon^{\prime} \end{aligned}$ |
| Magnetic fiux quantum, $[c]^{-1}(h c / 20)$ | $\begin{aligned} & \Phi_{10} \\ & h / e \end{aligned}$ | $\begin{aligned} & 2.0678506(54) \\ & 4.135701(11) \\ & 1.3795215(36) \end{aligned}$ | $\begin{aligned} & 2.6 \\ & 2.6 \\ & 2.6 \end{aligned}$ | $\begin{aligned} & 10^{-16} \mathrm{~Wb} \\ & 10^{-15} \mathrm{~J} \cdot 5 \cdot \mathrm{C}^{-1} \end{aligned}$ | $\begin{aligned} & 10^{-1} \mathrm{G} \cdot \mathrm{~cm}^{\mathrm{t}} \\ & 10^{-1} \text { org's.emu } \\ & 10^{-17} \text { org } \cdot \mathrm{s} \cdot \mathrm{es} \mathrm{u}^{-1} \end{aligned}$ |
| Josephson frequencyvoltage ratio | 2e/h | 4.835939(13) | 2.6 | $10^{14} \mathrm{~Hz}, \mathrm{Y}^{-1}$ |  |
| Quantum of circulation | $\begin{aligned} & h / 2 m_{e} \\ & h / m_{e} \end{aligned}$ | $\begin{aligned} & 3.6369455(60) \\ & 7.273891(12) \end{aligned}$ | 1.6 | $10^{-1} \mathrm{~J} \cdot 3 \cdot \mathrm{~kg}^{-1}$ $10^{-4} \mathrm{j} \cdot 8 \cdot \mathrm{~kg}^{-1}$ | $\begin{aligned} & \text { org.s } \cdot \mathrm{g}^{-1} \\ & \text { erg } \cdot s \cdot \mathrm{~g}^{-1} \end{aligned}$ |
| Faraday constant, $\mathrm{NA}_{\boldsymbol{A}}{ }^{\text {a }}$ | $F$ | $\begin{aligned} & 9.649456(27) \\ & 2.8925342(82) \end{aligned}$ | $\begin{aligned} & 2.8 \\ & 2.8 \end{aligned}$ | $10^{4} \mathrm{C} \cdot \mathrm{mol}^{-1}$ | $10^{1}$ omu $\cdot \mathrm{mol}^{-3}$ <br> $10^{14}$ esu $\cdot \mathrm{mol}^{-1}$ |
| Rydberg constant, $\left[\mu_{0} c^{2} / 4 \pi\right]^{2}\left(m_{k} \mathrm{e}^{1 / 4 \pi} \pi^{7} c\right)$ | $R_{\text {天 }}$ | 1.097373177 (83) | 0.075 | $10^{\circ} \mathrm{m}^{-1}$ | $10^{1} \mathrm{~cm}^{-1}$ |
| Böhr radius, $\left[\mu_{0} c^{2} / 4 \pi\right]^{-1}\left(n^{2} / m_{r} e^{2}\right)=a_{a} / 4 \pi R_{\alpha}$ | $a_{0}$ | 5.2917706(44) | 0.82 | $10^{-11} \mathrm{~m}$ | $10^{-2} \mathrm{~cm}$ |
| Classical electron radius, $\left[\mu_{0} c^{2} / 4 \pi\right]\left(\mathrm{e}^{2} / m_{r} c^{2}\right)=s^{3} / 4_{\pi} R_{x}$ | $\mathrm{r}_{\mathrm{e}}=\boldsymbol{a} \mathrm{N}_{\mathrm{C}}$ | 2.8179380 (70) | 2.5 | $10^{-13} \mathrm{~m}$ | $10^{-13} \mathrm{~cm}$ |
| Thomson cross section. $(8 / 3) \pi r_{e}{ }^{2}$ | $\sigma_{\text {n }}$ | 0.6652448(33) | 4.9 | $10^{14} \mathrm{~m}^{2}$ | $10^{-24} \mathrm{~cm}^{2}$ |
| Free electron g-factor, or electron magnetic moment in Bohr magnetons | $g_{+} / 2=\mu_{*} / \mu_{B}$ | $1.0011596567(35)$ | ) 0.0035 |  |  |


| Quantity | Symbol | Numerical Valus - U | Uncert. (ppm) | SIt $\quad<$ Units $\rightarrow$ | css= $\ddagger$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Free muon 8 -factor, or muon magnetic moment in units of [c](eh/2m $m_{\mu}$ ) | $\mathrm{S}_{\mu} / 2$ | $1.00116616(31)$ | 0.31 |  |  |
| Bohr magneton, [c] (en/2m,c) | ${ }^{\text {日 }}$ | $9.274078(36)$ | 3.9 | $10^{-34} \mathrm{~J} \cdot \mathrm{~T}^{-1}$ | $10^{-11} \mathrm{erg} \cdot \mathrm{G}^{-1}$ |
| Electron magnetic moment | $\mu_{r}$ | $9.284832(36)$ | 3.9 | $10^{-14} \mathrm{~J} \cdot \mathrm{~T} \cdot 1$ | $10^{-11} \mathrm{erg} \cdot \mathrm{G}^{-1}$ |
| Gyromagnetic ratio of protons in $\mathrm{H}_{2} \mathrm{O}$ |  | $\begin{aligned} & 2.6751301(75) \\ & 4.257602(12) \end{aligned}$ | $\begin{aligned} & 2.8 \\ & 2.8 \end{aligned}$ | $\begin{aligned} & 10^{3} \mathrm{~s}^{-1 \cdot \mathrm{~T}^{-1}} \\ & 10^{\mathrm{r}} \mathrm{~Hz} \cdot \mathrm{~T}^{-1} \end{aligned}$ | $\begin{aligned} & 10^{4} \mathrm{~s}^{-1} \cdot \mathrm{G}^{-1} \\ & 10^{1} \mathrm{~Hz} \cdot \mathrm{G}^{-1} \end{aligned}$ |
| $\gamma_{\text {. }}$. corrected for diamagnetism of $\mathrm{H}_{2} \mathrm{O}$ | $\gamma_{r}$ $\gamma_{p} / 2 \pi$ | $\begin{aligned} & 2.6751987(75) \\ & 4.257711(12) \end{aligned}$ | $\begin{aligned} & 2.8 \\ & 2.8 \end{aligned}$ | $\begin{array}{ll} 10^{r} & \mathrm{~s}^{-1} \cdot \mathrm{~T}^{-1} \\ 10^{\mathrm{r}} \mathrm{~Hz} \cdot \mathrm{~T}^{-1} \end{array}$ | $\begin{aligned} & 10^{4} \mathrm{~s}^{-1} \cdot \mathrm{G}^{-1} \\ & 10^{3} \mathrm{~Hz} \cdot \mathrm{G}^{-1} \end{aligned}$ |
| Magnetic moment of protons in $\mathrm{H}_{2} \mathrm{O}$ in Eohr magnotons | $\mu^{\prime} / \mu_{11}$ | $2.52099322(10)$ | 0.066 | $10^{-2}$ | $10^{-1}$ |
| Proton magnetic moment in Bohr magnetons | $\mu_{\mathrm{s}} / \mu_{\mathrm{H}}$ | 1.521032209(16) | ) 0.011 | $0 \cdot 3$ | $10^{-1}$ |
| Ratio of electron and proton magnetic moments | $\mu, / \mu_{\nu}$ | 658.2106880(66) | 0.010 |  |  |
| Proton magnetic moment | $\mu$ | 1.4106171(55) | 3.9 | $10^{.46} \mathrm{~J} \cdot \mathrm{~T}^{-1}$ | $10^{311}$ erem. ${ }^{\text {a }}$ |
| Magnetic moment of protons in $\mathrm{H}_{2} \mathrm{O}$ in nuclear magnetons | $\mu^{\prime}, / \mu$ | 2.7927740(11) | 0.38 |  |  |
| $\mu_{\mathrm{s}}{ }^{\prime} / \mu_{\mathrm{s}}$ corrected for dlamagnetism of $\mathrm{H}_{2} \mathrm{O}$ | $\mu_{s} / \mu_{0}$ | 2.7928456(11) | 0.38 |  |  |
| Nuelear magneton. $[c](0 h / 2 m, c)$ | $\mu$ | $5.050824(20)$ | 3.9 | $10^{19} \mathrm{~J} \cdot \mathrm{~T} \cdot 1$ | $10^{14}$ org. ${ }^{1}$ |
| Ratio of muon and proton magnotic moments | $\mu_{\mu} / \mu_{\text {, }}$ | $3.1833402(72)$ | 2.3 |  |  |
| Muon magnetic moment | $\mu$ | 4.490474(18) | 3.9 | $10^{34} \mathrm{~J} \cdot \mathrm{~T} \cdot 1$ | $10^{-11}$ org. ${ }^{-1}$ |
| Ratio of muon mass to electron mass | $m_{\mu} / m$ 。 | $206.76865(47)$ | 2.3 |  |  |
| Muon rest mass | $m_{\mu}$ | $\begin{aligned} & 1.883566(11) \\ & 0.11342920(26) \end{aligned}$ | $\begin{aligned} & 5.6 \\ & 2.3 \end{aligned}$ | $\begin{aligned} & 10^{-23} \mathrm{~kg} \\ & \mathrm{u} \end{aligned}$ | ${ }_{4}^{10^{-26} g}$ |
| Compton wavelength of the alectron, $h / m_{8} c=w^{2} / 2 R_{n}$ | $\begin{aligned} & \lambda_{c} \\ & \lambda_{C}=\lambda_{C} / 2 \pi=a B_{n} \end{aligned}$ | $\begin{aligned} & 2.4263089(40) \\ & 3.8615905(64) \end{aligned}$ | $\begin{aligned} & 1.6 \\ & 1.6 \end{aligned}$ | $\begin{aligned} & 10^{-13} \mathrm{~m} \\ & 10^{-19} \mathrm{~m} \end{aligned}$ | $10^{-10} \mathrm{~cm}$ <br> $10^{-11} \mathrm{~cm}$ |
| Compton waverength of the proton, $h / m_{f} c$ | $\begin{aligned} & \lambda_{r . r} \\ & \lambda_{r, 0}=\lambda_{c, p} / 2 \pi \end{aligned}$ | $\begin{aligned} & 1.3214099(22) \\ & 2.1030892(36) \end{aligned}$ | $\begin{aligned} & 1.7 \\ & 1.7 \end{aligned}$ | $\begin{aligned} & 10^{-13} \mathrm{~m} \\ & 10^{-14} \mathrm{~m} \end{aligned}$ | $\begin{aligned} & 10^{-11} \mathrm{~cm} \\ & 10^{-11} \mathrm{~cm} \end{aligned}$ |
| Compton wavalength of the neutron, $h / m_{n}{ }^{6}$ | $\lambda_{c, n}^{\lambda_{c, n}}=\lambda_{c, n} / 2 \pi$ | $\begin{aligned} & 1.3195909(22) \\ & 2.2001941(35) \end{aligned}$ | $\begin{aligned} & 1.7 \\ & 1.7 \end{aligned}$ | $\begin{aligned} & 10^{-25} \mathrm{~m} \\ & 10^{-14} \mathrm{~m} \end{aligned}$ | $10^{-11} \mathrm{~cm}$ $10^{-14} \mathrm{~cm}$ |
| Molar volume of ideal gas at s.t.p. | $V_{n}$ | 22,41383(70) | 31 | $10^{-3} \mathrm{~m}^{2} \cdot \mathrm{~mol}^{-1}$ | $10^{3} \mathrm{~cm}^{1} \cdot \mathrm{~mol}^{-1}$ |
| Molar gas constant, $V_{11} P_{10} / T_{4}$ | $R$ | $8.31441(26)$ | 31 | J. $\mathrm{mol}^{-1}+\mathrm{K}^{-1}$ | $10^{1}$ erg.mol ${ }^{-1 . K^{-1}}$ |
| $\begin{aligned} & \left\{T_{0}=273.15 \mathrm{~K} i p_{\\|} \equiv 101325\right. \\ & \left.P_{a \in \mathbb{E}} \mathrm{latm}\right) \end{aligned}$ |  | 8.20568(26) | 31 | $10^{-5} \mathrm{~m}^{3} \cdot$ atm $\cdot \mathrm{mol}{ }^{-1} \cdot \mathrm{~K}^{-1}$ | $10 \mathrm{~cm} \cdot \frac{\mathrm{~atm}}{} \cdot \mathrm{~mol}^{-1} \cdot \mathrm{~K}^{-1}$ |
| Boltzmann constant, R/NA | k | 1,380662(44) | 32 | $10^{-23} 3 \cdot \mathrm{~K}^{-1}$ | $10^{-14}$ ergek ${ }^{-1}$ |
| Stefan-Boltzmann constant, $\pi^{2} k^{4} / 60 h^{3} c^{2}$ | 0 | $5.67032(71)$ | 125 | $10^{\circ 4} \mathrm{~W} \cdot \mathrm{~m}^{-3} \cdot \mathrm{~K}^{-4}$ | $10^{-5}$ - $\mathrm{rg}^{-1 / 4} \mathrm{~cm}^{-1} \cdot \mathrm{~K}-4$ |
| First radiation constant, $2 \pi h c^{2}$ | $\varepsilon_{1}$ | $3.741832(20)$ | 5.4 | $10^{16} \mathrm{~W} \cdot \mathrm{~m}^{\text {²}}$ | $10^{-4} \mathrm{erg} \cdot \mathrm{cm}^{2.5}{ }^{-1}$ |
| Second radiation constant, he/k | $c_{2}$ | $1.438786(45)$ | 31 | $10^{-9} \mathrm{~m} \cdot \mathrm{~K}$ | $\mathrm{cm} \cdot \mathrm{K}$ |
| Gravitational constant | G | 6.6720(41) | 615 | $10^{-11} \mathrm{~m}^{3} \cdot \mathrm{~s}^{-2} \cdot \mathrm{~kg}^{-1}$ | $10^{-8} \mathrm{~cm}^{3} \cdot \mathrm{~s}^{-8} \cdot \mathrm{~g}^{1}$ |
| Ratio, kx-unit to Angström, $\begin{aligned} & A=\lambda(A) / \lambda(k \times u): \\ & \lambda\left(C u K a_{1}\right) \equiv 1.537400 \mathrm{kxu} \end{aligned}$ | A | $1.0020772(54)$ | 5.3 |  |  |
| $\begin{aligned} & \text { Ratio, } A^{*} \text { to anngström, } \\ & A^{*}=\lambda(A) / \lambda\left(A^{*}\right) ; \\ & \lambda\left(W K a_{1}\right) \equiv 0.2090100 A^{*} \end{aligned}$ | $\mathrm{A}^{*}$ | $1.0000205(56)$ | 5.6 |  |  |

## ENERGY CONVERSION FACTORS AND EQUIVALENTS

| Quantity | Symbol | Numerical Value * | Units | Uncert (ppm) |
| :---: | :---: | :---: | :---: | :---: |
| 1 kilogram ( $\mathrm{kg} \cdot \mathrm{C}^{2}$ ) |  | $8.987551786(72)$ <br> 5.609545(16) | $\begin{aligned} & 10^{16} \mathrm{~J} \\ & 10^{29} \mathrm{MeV} \end{aligned}$ | $\begin{aligned} & 0.008 \\ & 2.9 \end{aligned}$ |
| 1 Alomic mass unit (u-c*) |  | $\begin{gathered} 1.4924418(77) \\ 931.5016(26) \end{gathered}$ | $\begin{aligned} & 10^{-10} \mathrm{~J} \\ & \mathrm{MeV} \end{aligned}$ | $\begin{aligned} & 5.1 \\ & 2.8 \end{aligned}$ |
| 1 Electron mass $\mathrm{mr}_{*} \cdot \mathrm{c}^{2}$ ) |  | $\begin{aligned} & 8.187241(42) \\ & 0.5110034(14) \end{aligned}$ | $\begin{aligned} & 10^{1+} \mathrm{J} \\ & \mathrm{MeV} \end{aligned}$ | $\begin{aligned} & 5.1 \\ & 2.8 \end{aligned}$ |
| 1 Muon mass ( $\mathrm{m}_{\mu} \mathrm{c}^{2}$ ) |  | $\begin{gathered} 1.6928648(96) \\ 105.65948(35) \end{gathered}$ | $\begin{aligned} & 10^{-61} \mathrm{~J} \\ & \mathrm{MeV} \end{aligned}$ | $\begin{aligned} & 5.6 \\ & 3.3 \end{aligned}$ |
| 1 Proton mass ( $m_{*}^{*} c^{2}$ ) |  | $\begin{gathered} 1.5033015(77) \\ 938.2796(27) \end{gathered}$ | $\begin{aligned} & 10.10 \mathrm{~J} \\ & \mathrm{MeV} \end{aligned}$ | $\begin{aligned} & 5.1 \\ & 2.8 \end{aligned}$ |
| I Neutron mass ( $\mathrm{m}_{5}{ }^{*} \mathrm{C}^{\mathbf{*}}$ ) |  | $\begin{gathered} 1.5053738(78) \\ 939.5731(27) \end{gathered}$ | $\begin{aligned} & 10^{-10} \mathrm{~J} \\ & \mathrm{MeV} \end{aligned}$ | $\begin{aligned} & 5.1 \\ & 2.8 \end{aligned}$ |
| 1 Electron volt |  | $1.6021892(46)$ | $\begin{aligned} & 10^{-19} \mathrm{~J} \\ & 10^{-12} \text { erg } \end{aligned}$ | $\begin{aligned} & 2.9 \\ & 2.9 \end{aligned}$ |
|  |  | $2.4179696(63)$ | $10^{14} \mathrm{~Hz}$ | 2.6 |
|  | $1 \mathrm{eV} / \mathrm{hc}$ | $8.065479(21)$ | $\begin{aligned} & 10^{5} \mathrm{~m}^{-1} \\ & 10^{3} \mathrm{~cm}^{-1} \end{aligned}$ | 2.6 2.6 |
|  | $1 \mathrm{eV} / \mathrm{k}$ | $1.160450(36)$ | $10^{4} \mathrm{~K}$ | 31 |
| Voltage wavelength conversion, bc |  | $\begin{aligned} & 1.996478(11) \\ & 1.2398520(32) \end{aligned}$ | $\begin{aligned} & 10^{2 \mathrm{j}} \mathrm{~J} \cdot \mathrm{~m} \\ & 10^{-5} \mathrm{eV} \cdot \mathrm{~m} \\ & 10^{-4} \mathrm{eV}^{\mathrm{V}} \cdot \mathrm{~cm} \end{aligned}$ | $\begin{aligned} & 5.4 \\ & 2.6 \\ & 2.6 \end{aligned}$ |
| Rydberg constant | $\mathrm{R}_{x} h \mathrm{c}$ | $2.179907(12)$ | $\begin{aligned} & 10^{-10} \mathrm{~J} \\ & 10^{-11} \mathrm{erg} \end{aligned}$ | $\begin{aligned} & 5.4 \\ & 5.4 \end{aligned}$ |
|  |  | $13.605804(36)$ | eV | 2.6 |
|  | $\mathrm{R}_{\mathrm{z}} \mathrm{c}$ | $3.28984200(25)$ | $10^{15} \mathrm{~Hz}$ | 0.075 |
|  | $R_{x} h \mathrm{c} / \mathrm{h}$ |  |  |  |
| Bohr magneton | $\mu_{\mathrm{H}}$ | $\begin{aligned} & 9.274078(36) \\ & 5.7893785(95) \end{aligned}$ | $\begin{aligned} & 10^{-7:} \mathrm{J} \cdot \mathrm{~T}^{-1} \\ & 10^{-3} \mathrm{eV} \cdot \mathrm{~T}^{-1} \end{aligned}$ | 3.9 1.6 |
|  | $\mu_{B} / h$ | $1.3996123(39)$ | $10^{10} \mathrm{~Hz} \cdot \mathrm{~T}^{-1}$ | $\begin{aligned} & 2.8 \\ & 18 \end{aligned}$ |
|  | $\mu_{H} /$ hc | 46.68604(13) | $\begin{aligned} & \mathrm{m}^{-1}, \mathrm{~T}^{-1} \\ & 10^{-2} \mathrm{~cm}^{-1}, \mathrm{~T}^{-1} \end{aligned}$ | $\begin{aligned} & 2.8 \\ & 2.8 \end{aligned}$ |
|  | $\mu_{n} / k$ | $0.671712(21)$ | K.T-1 | 31 |
| Nuclear tragneton | $\mu \mathrm{s}$, | $5.505824(20)$ | $10 \mathrm{NT} \mathrm{J.T-1}$ | 3.9 |
|  |  | $3.1524515(53)$ | $10^{-2} \mathrm{eV} \cdot \mathrm{T}^{-1}$ | 1.7 |
|  | \%/h | $7.622532(22)$ $2.5426030(72)$ | $10^{\circ} \mathrm{Hz} \cdot \mathrm{t}^{-1}$ $10^{-1} \mathrm{~m}^{-1 . t-1}$ | 2.8 2.8 |
|  | ¢V/re | $2.5426030(72)$ | $10^{-1} \mathrm{~cm}^{-1}, \mathrm{~T}^{-1}$ | 2.8 |
|  | $\mu, 7 k$ | $3.65826(12)$ | $10^{-}+\mathrm{K} \cdot \mathrm{T}^{-1}$ | 31 |

[^4]

 cecond factor, in parentheses. I5 the oxpression to bi uxed when all quantiliet ora expressed in egs units, with the electron charge in alectioatatic units. The first factor, in brechets, is to be ancluded only if all quantities are exprassed in SI units. Wo remind the rasder that with the exceplian of the suxiliary conslanta which have been taken to be exaci, the uncertnintioz of these constants are carralefed, and therefore the gensral law of erroe propagation muat be used in calcuiating additiongl quantifies requiring two or more of these constants.
$t$ Quentotiet given in $u$ and asm are for tise convenience of the resdar, thata uniti are not part of the International syifem of Units (SI).
$\ddagger$ In order to ovoid separate columns for "electromagnotic" ond "electrostatic" units, both are givin under the single meading "cgi Units."


| Spacing (in.) | XXXP | Material <br> Melamine | Tellon |
| :--- | :--- | :--- | :--- |
| $1 / 32$ | 1.05 | 1.25 | 0.33 |
| $1 / 116$ | 0.85 | 1.10 | 0.26 |
| $1 / 8$ | 0.72 | 0.90 | 0.22 |

## APPROXIMATE RESISTANCE OF CONDUCTORS (ohms/inch)

Based on $100 \%$ conductlvity of copper at $20^{\circ} \mathrm{C}$

$$
\begin{aligned}
& R=\frac{0.000503}{w} \text { for } 1 \text { ounce copper } \\
& R=\frac{0.000226}{w} \text { for } 2 \text { ounce copper } \\
& R=\frac{0.000135}{w} \text { for } 3 \text { ounce copper } \\
& w=\text { conductor width in inches }
\end{aligned}
$$

VELOCITY OF SOUND IN SOLIDS, GASES, ANO LIQUIDS


## RELAY CONTACT CODE

This is the letter code adapted by the American Standards Association and by the National Association of Relay Manufacturers to describe relay contacts.

Other standard contact symbols



| FORM | TERM | CONTACT CONFIGURAIION | FORM | TERM | CONTACT CONFIGURATION |
| :---: | :---: | :---: | :---: | :---: | :---: |
| A | make |  | J | make <br> MAKE <br> BREAK |  |
| B | BREAK |  | K | sp or center OFF |  |
| $C$ | BREAK MAKE (rionster) |  | l | greak hake ~AKE |  |
| D | MAKE BEFORE BREAK (continuily tronslet) | $\infty-\infty$ | U | dougle make CONTACT ON armature |  |
| E | break <br> MAKE-BEFORE <br> break |  | V | oOuble break CONTACTON aRMATURE |  |
| F | $\operatorname{MaKE}_{\text {MAKE }}$ |  | w | DOUble sreak double make CONTACT ON aRMATURE |  |
| G | BREAK BREAK |  |  | Double make |  |
| H | BREAK BREAK MAKE |  |  | DOUBLE BREAK | ST NC DB. |
| 1 | MAKE BREAK MAKE |  | 2 | DOUBLE BREAK double make |  |

## heat-Sink thermal resistance chart

Heat-sink thermal resistance can be determined with the accompanying chart. Values determined graphically are not as accurate as those found from thermal equations but are precise enough for most applications. To find thermal resistance, draw a vertical line from the scale for surface area to the scales for materials and read the corresponding thermal resistance. For example, a $3 / 16$-in-thick piece of horizontally mounted copper with a surface area of $15 \mathrm{in} .^{2}$ has a thernal resistance of approximately $4.1^{\circ} \mathrm{C} / \mathrm{W}$. And a $3 / 32$-in.-thick piece of vertically mounted copper with a surface area of 25 in. ${ }^{2}$ has a thermal resistance of approximately $3.1^{\circ} \mathrm{C} / \mathrm{W}$. Note that vertical heatsinks have lower thermal resistances than horizontal sinks because convection provides increased heat dissipation.


Following is an up-to-date guide to predominant electric voltages in foreign countries. In general, all references to 110 V apply to the range from 110 V to 160 V . References to 220 V apply to the range from 200 V to 260 V . Where $110 / 220 \mathrm{~V}$ is indicated, voltage varies within the couniry, depending on location.

| Aden | 220 V | Domlnica | 220 V |
| :---: | :---: | :---: | :---: |
| Aghanistan | 220 V | Dominican Rep. | 1101220 V |
| Algeria | $110 / 220 \mathrm{~V}$ | Ecuador | $110 / 220 \mathrm{~V}$ |
| Angola | 220 V | Egypt | $110 / 220 \mathrm{~V}$ |
| Anguills | 220 V | ElSalvador | 110 V |
| - Antlgua | $110 / 220 \mathrm{~V}$ | Ethiopia | 1101220 V |
| + Argentina | 220 V | $\ddagger \mathbf{F}\|\boldsymbol{j}\|$ | 220 V |
| Aruba | 110 V | Finland | 220 V |
| $\ddagger+$ Australia | 220 V | France | $110 / 220 \mathrm{~V}$ |
| - Austris | 220 V | French Guiana | $110 / 220 \mathrm{~V}$ |
| Azores | $110 / 220 \mathrm{~V}$ | Gabon | 220 V |
| Bahamas | 110/220V | Gambia | 220 V |
| Bahrain | 220 V | - Germany | $180 / 220 \mathrm{~V}$ |
| Bangladesh | 220 V | Ghama | 220 v |
| Barbados | $110 / 220 \mathrm{~V}$ | Gibralter | 220 v |
| Belglum | $110 / 220 \mathrm{~V}$ | -Great Britain | 220 V |
| Bermuda | 1101220 V | +Greece | $110 / 220 \mathrm{~V}$ |
| Bhulan | 220 V | Greenland | 220 V |
| Bolivia | 110/220V | -Grenada | 220 V |
| Bonalre | $110 / 220 \mathrm{~V}$ | Grenadines | 220 V |
| - Botswana | 220 V | - Guadeloupe | $110 / 220 \mathrm{~V}$ |
| + Brazil | $110 / 220 \mathrm{~V}$ | Guatemala | 1101220 V |
| Brit. Honduras | $110 / 220 \mathrm{~V}$ | Guines | 220 V |
| Brit. Virgin I . | $110 / 220 \mathrm{~V}$ | Guyana | $110 / 220 \mathrm{~V}$ |
| Buigaria | $110 / 220 \mathrm{~V}$ | Haiti | 110 I 220 V |
| Burma | 220 V | Honduras | 1101220 V |
| Burundi | 220 V | - Hong Kong | 220 V |
| Cambodia | $110 / 220 \mathrm{~V}$ | Hungary | 220 V |
| Cameroon | $110 / 220 \mathrm{~V}$ | Iceland | 220 V |
| Canada | 110 V | $t$ india | 220 V |
| Canal Zone | $110 / 220 \mathrm{~V}$ | indonesia | 1101220 V |
| Canary l . | $110 / 220 \mathrm{~V}$ | iran | 220 V |
| Cayman I . | 110 V | Ireq | 220 V |
| Cen. African Rep. | 220 V | - Iraland | 220 V |
| Chad | 220 V | Isle of Man | 220 V |
| - Channel I. (Brit) | 220 V | larsel | 220 V |
| ${ }^{+}$Chille | 220 V | Italy | $110 / 220 \mathrm{~V}$ |
| $\ddagger$ China | 220 V | Ivory Coast | 220 V |
| Colombia | 110 V | - Jamaica | $110 / 220 \mathrm{~V}$ |
| Coste Rica | $110 / 220 \mathrm{~V}$ | Japan | 110 V |
| Cuba | 110 V | Jordan | 220 V |
| Curacao | 110 V | - Kenye | 220 V |
| - Cyprus | 220 V | Korea | 110 V |
| Czechoslovakia | $110 / 220 \mathrm{~V}$ | Kuwalt | 220 V |
| Dahomey | 220 V | Lso | $110 / 220 \mathrm{~V}$ |
| Denmark | 220 V | Lebanon | $110 / 220 \mathrm{~V}$ |


| Lesotho | 220 V | Samoe | $110 / 220 \mathrm{~V}$ |
| :---: | :---: | :---: | :---: |
| Liberia | $110 / 220$ | St. Barthelemy | 220 V |
| Liby* | $110 / 220 \mathrm{~V}$ | St. Eustatlus | 110/220V |
| -Liechtenstein | 220 V | -St, Kilts | 220 V |
| Luxembourg | $110 / 220 \mathrm{~V}$ | -St. Lucia | 220 V |
| Macao | $110 / 220 \mathrm{~V}$ | St. Mastien | $110 / 220 \mathrm{~V}$ |
| + Madeira | 220 V | St. Vincent | 220 V |
| Majorca | 110 V | Saudi Arabia | $110 / 220 \mathrm{~V}$ |
| Malagasy Rep. | 220 V | - Scotland | 220 V |
| -Malawi | 220 V | Senegal | 110 V |
| - Malaysia | 220 V | Seychalles | 220 V |
| Mali | $110 / 220 \mathrm{~V}$ | Slerra Leone | 220 V |
| Malta | 220 V | -Singapore | $110 / 220 \mathrm{~V}$ |
| Martinique | $110 / 220 \mathrm{~V}$ | Somalia | $110 / 220 \mathrm{~V}$ |
| Mauritanis | 220 V | -South Alrica | 220 V |
| Mexico | $110 / 220 \mathrm{~V}$ | - Spaln | $110 / 220 \mathrm{~V}$ |
| Monaco | $110 / 220 \mathrm{~V}$ | SriLanke (Ceylon) | 220 V |
| Montserrat | 220 V | Sudan | 220 V |
| Morocco | $110 / 220 \mathrm{~V}$ | Surinam | 1101220 V |
| Mozambique | 220 V | Swaziland | 220 V |
| Nepal | 220 V | + Sweden | $110 / 220 \mathrm{~V}$ |
| - Netheriands | $110 / 220 \mathrm{~V}$ | -Switzerland | $110 / 220 \mathrm{~V}$ |
| Neth. Antilles | $110 / 220 \mathrm{~V}$ | Syria | $110 / 220 \mathrm{~V}$ |
| - Nevis | 220 V | Tahiti | 110 V |
| New Caledonia | 220 V | Talwan | 1101220 V |
| New Hebrides | 220 V | Tanzania | 220 V |
| $\ddagger$ New Zealand | 220 V | Thalland | 220 V |
| Nicaragua | 110 V | Tobago | 110 l 220 V |
| Niger | 220 V | Togo | $110 \mathrm{h220V}$ |
| - Nigeria | 220 V | Tonga | 220 V |
| - Northern lreland | 220 V | Trinidad | $110 / 220 \mathrm{~V}$ |
| Norway | 220 V | Tunisia | $110 / 220 \mathrm{~V}$ |
| Okinawa | 110 V | Turkey | $110 / 220 \mathrm{~V}$ |
| Oman | 220 V | Turksac Calcos 1. | 110 V |
| Paklstan | 220 V | Ugande | 220 V |
| Panama | 110 V | United Arab Emirates | 220 V |
| Papua New Guines | 220 V | Upper Volta | 220 V |
| *Paraguay | 220 V | Uruguay | 220 V |
| Peru | 220 V | USA | 110 V |
| Phillippines | $110 / 220 \mathrm{~V}$ | USSR | $110 / 220 \mathrm{~V}$ |
| Poland | 220 V | U.S. VIrginl. | 110 V |
| Portugal | 1101220 V | Veneruela | 110 V |
| Puerto Rico | 110 V | Vietnam | $110 / 220 \mathrm{~V}$ |
| Oatar | 220 V | -Wales | 220 V |
| - Rhodesla | 220 V | Yemen | 220 V |
| Romanis | 110 i 220 V | - Yugoslavia | 220 V |
| Pwande | 220 V | Zaire | 220 V |
| Saba | $110 / 220 \mathrm{~V}$ | Zambla | 220 V |

[^5](Reprinted from "Foreign Electricity is No Deep Dark Secret," courtesy of Franzus Company Inc.)


It is sometimes necessary to determine the $x$ and $y$ coordinates of a circle divided into an equal number of parts. The following table can be used directly, or it can serve as a crosscheck against answers obtained by normal trigonometric methods.

FOR EXAMPLE: A circle that has a radius of 5.0 cm and contains 4 holes spaced at $90^{\circ}$. Determine the distance between their centers. $A=1.4142 \mathrm{R}=1.4142(5.0)=7.07 \mathrm{~cm}$.


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[^0]:    

[^1]:    The computer programming required for the Chebyshev and elliptic filter design tabulations was prepared by Mike Barge under the direction of Ed Wetherhold. The tables are made available for publication through the courtesy of the Signal Analysis Center of Honeywell tnc., Annapolis, MD.

[^2]:    league Light year Light year
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[^3]:    
     vertically to find the relative humidity at the intersection of the horizontal column representing the dry－bulb reading． Tables are given for Celslus and Fahrenheit readings at sea level．

    FOR EXAMPLE：A dry－bulb reading of $88^{\circ} \mathrm{F}$ and a wet－bulb readirg of $80^{\circ} \mathrm{F}$（difference $8^{\circ} \mathrm{F}$ ）indicates a relative humidity of $70^{\circ}$ ．

[^4]:    * Note that the numbers in perentheses are the one atandard-deviation uncertaintien in the lest digits of the quoted value compuied on the

[^5]:    *Denotes countries in which plugs with 3 square pins are used (in whole or part)
    ¡Countries using de in certain areas
    \#Requires plug with angled blades -Countries with recessed outlets

